SITE PLAN REVIEW AGENDA

5/25/2022 - 9:00 A.M. Conference Room #4 315 E. Acequia Avenue

ITEM NO: 1 Resubmit
SITE PLAN NO: SPR20124
PROJECT TITLE: Forebay Farms

DESCRIPTION: Development of 35.07 +/- acres into Single Family residential Development (O-PA, R-1-5, R-M2)

APPLICANT: Norman Allinder

OWNER: FOREBAY FARMS LLC

APN: 101050041

LOCATION: 1410 S LOVERS LANE

ITEM NO: 2 Resubmit SITE PLAN NO: SPR22005

PROJECT TITLE: 125 S Crenshaw

DESCRIPTION: 41 Lot Single Family Subdivision (X)

APPLICANT: Bill Toor

OWNER: TOOR SANTOKH S & ARPINDER K (TRS)

APN: 085130002

LOCATION: 125 S CRENSHAW ST

ITEM NO: 3 Resubmit SITE PLAN NO: SPR22041

PROJECT TITLE: Visalia Plaza 39/Seefried

DESCRIPTION: New Construction of a 535,540 sf Industrial Building and Associated Improvements. (I)

APPLICANT: Bryan Frarey

OWNER: VALLEY GOLD PROPERTIES LLC

APN: 077111047 077111046

LOCATION: 2045 N PLAZA DR Visalia, C

ITEM NO: 4 Resubmit SITE PLAN NO: SPR22053

PROJECT TITLE: Adam & Eve Visalia

DESCRIPTION: Retail - Lingerie & Boutique Store

APPLICANT: LM Capital LLC

OWNER: CHEN FENG YU (TR)

APN: 096321009

LOCATION: 1312 S MOONEY BLVD

ITEM NO: 5 Resubmit SITE PLAN NO: SPR22072

PROJECT TITLE: GA Industrial Complex

DESCRIPTION: New 140800 SF Warehouse With Loading Docks. (I)

APPLICANT: Corwyn Oldfield

OWNER: AMERICAN INCORPORATED

APN: 081180003

LOCATION: On Goshen Ave 600ft West of Clancy St

SITE PLAN REVIEW AGENDA

5/25/2022 - 9:00 A.M. Conference Room #4 315 E. Acequia Avenue

ITEM NO: 6

SITE PLAN NO: SPR22085

PROJECT TITLE: Alejandra's and Jimmy John's

DESCRIPTION: Rebuild of Existing Restaurants and Retail Building. (D-MU)

APPLICANT: Dave Francy

OWNER: FRANEY FAMILY LIMITED PARTNERSHIP

APN: 094322004

LOCATION: 312 W MAIN ST

314 W MAIN ST 316 W MAIN ST

ITEM NO: 7

SITE PLAN NO: SPR22086

PROJECT TITLE: Larry & Penny Owsley

DESCRIPTION: Lot Split (R-1-5)

APPLICANT: Larry & Penny Owsley

OWNER: OWSLEY LARRY D & PENNY M

APN: 103330100

LOCATION: 3307 E HOUSTON AVE

ITEM NO: 8

SITE PLAN NO: SPR22087

PROJECT TITLE: Facial Xpressions Skin Care Salon

DESCRIPTION: Skin Care Salon and Retail

APPLICANT: Norma A Pena

OWNER: OLDENBOURG JOSEPH (TR) (OLDENBOURC

APN: 123240024

LOCATION: 400 W CALDWELL AVE UNI

ITEM NO: 9

SITE PLAN NO: SPR22088

PROJECT TITLE: Visalia/Kelsey St. Industrial

DESCRIPTION: Construction of 2 Warehouse/Distribution Buildings for a total of 2098 SF (X)

APPLICANT: Derek Meddings
OWNER: SE LAND LLC
APN: 081071013
081071020

081071020 081040001

LOCATION: 29811 RD 88 29709 RD 88

ITEM NO: 10

SITE PLAN NO: SPR22089
PROJECT TITLE: Super Serrano's

DESCRIPTION: Taco Truck (C-N)
APPLICANT: Susan Ocampo

OWNER: SINGH SUCHA

SITE PLAN REVIEW AGENDA

5/25/2022 - 9:00 A.M. Conference Room #4 315 E. Acequia Avenue

APN: 103152010

LOCATION: 3332 E MINERAL KING AVE

CITY OF VISALIA SITE PLAN REVIEW APPLICATION

- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -

| | - Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting - | | | | | | | |
|--|---|---------------------------------------|--|--|--|--|--|--|
| | Project/Business Name: Forebay Farms, LLC | Date: 09/27/2021 | | | | | | |
| | Project Description: Development of 35.07+/- acres of vacant land into 82 R-1- | 5 Single Family Residential units and | | | | | | |
| | 7 remained lots of mixed uses. | | | | | | | |
| ININI | Site Plan Review Resubmittal: Yes No If Resubmittal, Previous Site P | Plan Review Number: SPR 20-124 | | | | | | |
| | Property Owner: Forebay Farms, LLC | | | | | | | |
| SEINERAL PROJECT INFORMATION | Applicant(s) Name: Norman L. Allinder, AICP | | | | | | | |
| I L | Project Address/Location: 1410 S. Lovers Lane; South of Tulare Ave. | | | | | | | |
| N. L. | Assessor Parcel Number: <u>1 0 1 - 0 5 0 - 0 1 9</u> | | | | | | | |
| 5 | Parcel Size (Acreage or Square Feet): 35.07+/- Building or Suite S | Square Footage: N/A | | | | | | |
| | Are There Any Proposed Building Modifications: Yes No X | THIS AREA FOR CITY STAFF USE ONLY | | | | | | |
| | Estimated Cost of Modifications to Building: \$ N/A | Date Received: | | | | | | |
| | Describe All Proposed Building Modifications: N/A | SPR Agenda: Item No | | | | | | |
| | | Zone: SPR No20-124 | | | | | | |
| | | Historic District: Yes No | | | | | | |
| | | Flood Zone: X AE X/AE | | | | | | |
| | A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOM | MENDED FOR ALL SUBMITTALS | | | | | | |
| | Existing/Prior Building Use: | | | | | | | |
| | Proposed Building Use: | | | | | | | |
| | Proposed Hours of Operation: | | | | | | | |
| TO THE PARTY OF TH | Days of Week In Operation (Circle): Su M T W Th F Sa | | | | | | | |
| | Number of Employees Per Day: Existing Propose | ed | | | | | | |
| | Number of Customers Per Day (Estimated): Existing Propose | ed | | | | | | |
| | Predicted Peak Operating Hour: | | | | | | | |
| | Describe Any Truck Delivery Schedule & Operations: | | | | | | | |
| Si Filoria | | | | | | | | |
| | Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For | Operations, Customers, or Employees | | | | | | |
| | (Provide Separate Attachment if Necessary): | | | | | | | |
| | | | | | | | | |
| | Describe Any Special Events Planned for the Facility: | | | | | | | |
| | | | | | | | | |
| | Page 1 of 2 - Application continues on back of t | this name | | | | | | |

| | SITE PLAN MINIMUM REQUIREMENTS | | | | | | | |
|------------------------|---|--|--|--|--|--|--|--|
| ENTS | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies not accepted). | | | | | | | |
| SEME. | Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. | | | | | | | |
| SITE PLAN REQUIREMENTS | Site plan shall provide for and indicate all of the following: North arrow All existing & proposed site features All existing & proposed site features Refuse enclosures & containers Existing and proposed fencing at site Public improvements (curbs, sidewalks, utility poles, hydrants, street lights, etc.) Applicant Information (Final comments will be mailed to the name and address provided below) - Loading/unloading areas - Accessible path of travel from ADA stall - Accessible path of travel from ADA stall - Location and width of drive approaches to site - Tentative maps shall adhere to requirements of Visalia Municipal Code Section 16 | | | | | | | |
| JRE | Name: Norman L. Allinder, AICP Signature of Owner or Authorized Agent* | | | | | | | |
| VATL | Address: PO Box 2717 | | | | | | | |
| SIG | City, State, Zip Merced, CA 95344 Owner Date | | | | | | | |
| RED | Phone: 209-534-6252 | | | | | | | |
| REQUIRED SIGNATURE | Email: nallinder@yahoo.com Authorized Agent* Date | | | | | | | |
| æ | * If signed by an authorized agent , the "Agency Authorization" information below must be completed for this application to be considered acceptable. | | | | | | | |
| | AGENCY AUTHORIZATION | | | | | | | |
| | OWNER: | | | | | | | |
| | I, Lloyd Fagundes , declare as follows; I am the owner of certain real property bearing assessor's | | | | | | | |
| | parcel number (APN): | | | | | | | |
| | 101-050-019 | | | | | | | |
| | AGENT: | | | | | | | |
| | I designate Norman L. Allinder to act as my duly authorized agent for all purposes necessary to file | | | | | | | |
| FORM | an application for, and obtain a permit to _process a Tentative Subdivision Map | | | | | | | |
| Z | relative to the property mentioned herein. | | | | | | | |
| ZATIC | I declare under penalty of perjury the foregoing is true and correct. | | | | | | | |
| AGENCY AUTHORIZATIO | Executed this day of | | | | | | | |
| / AUT | | | | | | | | |
| ENC | OWNER Signatures AGENT | | | | | | | |
| AC | See Attached Letter of Agency | | | | | | | |
| | Signature of Owner Signature of Agent | | | | | | | |
| | PO Box 2717, Merced, CA 95344 Owner Mailing Address PO Box 2717, Merced, CA 95344 Agent Mailing Address | | | | | | | |
| | Agent Walling Address | | | | | | | |
| | 209-383-6046 209-534-6252 | | | | | | | |
| | Owner Phone Number Agent Phone Number | | | | | | | |
| | | | | | | | | |
| 1 | Page 2 of 2 | | | | | | | |

Forebay Farms

P.O. Box 2717 • Merced, CA 95344 Phone: (209) 383-6046 • Fax: (209) 383-6042

July 31, 2020

City of Visalia 315 E. Acequia Avenue Visalia, CA 93291

Subject: Letter of Agency - 1410 S. Lovers Lane APN - 101-050-019

Japunk

Forebay Farms designates Norman L. Allinder, AICP to act as duly authorized agent for all matters related to entitlement, engineering and development of property located east of S. Lovers Lane and north of E. Walnut Avenue in the City of Visalia, APN 101-050-019. Please feel free to contact me if you have any questions.

Sincerely,

Lloyd Fagundes Forebay Farms



430 Tenth Street Modesto, CA 95354 Tel.: 209.568.4477

Fax: 209.568.4478

April 21, 2022

Cristobal Carrillo

City of Visalia **Associate Planner** 315 E Acequia Avenue Visalia, CA 93291

Reference: Forebay Farms, Site Plan No. 2020-124-B

Mr. Carrillo,

Thank you for the letter dated October 13, 2021, providing plan review comments for the referenced project. Included herewith are revised plans as requested. Find following our written responses to all review comments in **bold italics**:

1. Project shall require a Tentative Subdivision Map (TSM).

Response: Tentative Subdivision Map (TSM) included with resubmittal.

2. Vehicle Miles Traveled Analysis shall be required with TSM submittal.

Response: Per results from the City of Visalia VMT online screening tool VMT analysis is not required (attached email 1).

- 3. Due to changes in the density of the project, the proposal will no longer require a Conditional Use Permit (CUP) for a Planned Residential Development.
 - Response:
- 4. A Phasing Plan shall be provided with the site Plan Review and TSM submittal.
 - Response: Phasing has been added to sheet 1 of the TSM.
- 5. Lot shall be designed with Visalia Municipal Code development standards, in particular 60 ft. widths for corner lots, 80 ft. widths for corner cul-de-sac lots (Lot No. 35), and 40 ft. widths on cul-de-sac interior lots (Lot No. 45).

Response: All corner lots meet the minimum design requirements of the Visalia Municipal Code.

| Lot Number | Lot Width | Location |
|------------|-----------|------------|
| 1 | 60' | Rear |
| 22 | 65' | Front/Rear |
| 23 | 65.56′ | Front |
| 34 | 60' | Front/Rear |
| 35 | 80' | Front/Rear |
| 47 | 60' | Front |
| 59 | 60' | Front/Rear |
| 66 | 60.14' | Rear |
| 67 | 60' | Front/Rear |
| 74 | 67.40 | Front |
| 75 | 69.61' | Rear |
| 82 | 60.′ | Rear |



- 6. Tribal consultation as required by AB 52 shall be conducted for the project. If requested during consultation, a cultural study and/or record searches with the Native American Heritage Commission and California Historical Resources Information System may be required.
 - Response: We understand that Tribal Consultation will occur. Our understanding is the City will perform this task (attached email 1).
- 7. The applicant shall label all outlots as "Remainder" lots. *Response: Outlot's have be labeled remainder lots.*
- 8. Note that all street names shall be reviewed and approved by City of Visalia Traffic Engineering staff.
 - Response: Street names have been updated to match adjacent street alignment names.
- 9. As much as possible the applicant shall identify all future uses for the Remainder lots.

 Response: Future uses have been identified to the best of our ability. Some future uses are assumed and not exactly known at this time.
- 10. The applicant shall provide additional detail on the proposed open space areas and outlots, including any potential block walls, infrastructure, and amenities to be placed onsite. Response: Remainder Lot Table has been updated to include detail on proposed open space. Remainders A, D, E, and F are proposed to be dedicated to the City of Visalia for use as open space. No block walls or infrastructure are proposed for these Remainder Lots. Remainder Lot G shall be dedicated to the City of Visalia as a future park. Water and sewer utilities will be stubbed to the Remainder Lot.
- 11. The inclusion of bike and pedestrian paths is encouraged.

 Response: No bike paths are proposed with this project. The only pedestrian paths that are proposed are the sidewalks within the public right of way.
- 12. The relocation of Parks/Recreation designated areas shall be approved by the Visalia Community Services Department prior to the discretionary review process for the TSM.

 Response: Please see attached email for park size. Location of park appears to match General Plan map location (attached email 2).
- 13. Project shall include the build-out of Vista Street as required by the Engineering Division.

 Response: The buildout of Vista Street has been included as part of the development. Vista Street will terminate with a cul-de-sac north of Packwood Creek, Vista Street will start at the knuckle south of Packwood Creek and continue to the southern boundary of the project.
- 14. Note that per Engineering Division, access from Lot H to South Lovers Lane may be restricted. A stub street may be necessary to the south. A full City Standard cul-de-sac/turnaround will be required at the terminus of Santa Anita Way. Furthermore, left turn access from Lovers Lane to Churchill Downs Way will be prohibited. Lastly, connectivity between South Lovers Lane and the proposed Packwood Trail will need to be addressed and discussed by the applicant and Engineering staff.
 - Response: Access to Remainder H shall be restricted along the frontage of Lovers Lane and will be noted on the Final Subdivision Map. The revised TSM has included a stub street (S. Vista St) to the southern boundary of the subdivision. The revised TSM includes a full designed cul-de-sac per City of Visalia Standards. The intersection of E. Harvard Ave and Lovers lane has been designed as a ¾ access with no left turn out of E. Harvard Ave onto Lovers Lane. Left turn into E. Harvard Ave from Lovers Lane is part of the proposed TSM. Connectivity with the proposed



Packwood Creek crosswalk and accessible curb ramp has been evaluated and adjustments have been made to the SM to avoid any conflict. The proposed mid-block curb ramp proposed with the City project shall be removed and replaced with an accessible return curb ramp as part of the development of this project and more specifically E. Harvard Avenue.

- 15. See Engineering Division comments.
 - 1) Local street design to comply with City stds. Ensure knuckles and cul-de-sacs are designed to standard radii.
 - Response: Local streets within the subdivision are designed to comply with City of Visalia P-1, cul-de-sac design complies with City of Visalia standard P-16, knuckle design complies with City of Visalia standard P-17. Dimensions have been added to the TSM for cul-de-sacs and knuckles.
 - 2) Comply with City local (60') and arterial (110') street standards.

 Response: Public rights of way shown on the TSM are designed to comply with City of Visalia standard P-1 and P-5.
 - 3) Show phasing of tentative map if desired. Submit tentative subdivision map, refer to City submittal requirements.
 - Response: Phasing has been added to the TSM.
 - 4) All lots along Lovers Lane will require access relinquishment along their west property line. Future development of the lots shall take access from local street circulation per City standards.
 - Response: All lots with frontage on Lovers Lane will have access relinquished by Final Subdivision Map.
 - 5) Refer to traffic Dept. comments for access restrictions and median break design. Further coordinate with Traffic Dept. is required to determine areas of improvement for access to project.
 - Response: Access has been modified per consultation from Diego Corvera.
 - 6) There is a current City project that will install a signalized pedestrian crossing for trail along creek. City project will impact proposed development design. Further coordinate with City project manager. Redesign accordingly.
 - Response: We have received plans for the Packwood Trail from Diego Corvera. The street has been modified to allow the proposed curb ramp to align with the crossing.
 - 7) Provide storm and sewer master plan design plan with development. The City is currently updating its master sewer and storm plans, proposed project will be subject to any changes implemented.
 - Response: The project will be designed in accordance with the adopted storm and sewer master plans.
 - 8) Lovers Lane is a 110' arterial, 55' to C/L and dedicate right-of-way accordingly. Project to improve Lovers Lane per Standards, including the creek frontage. Improvements to include, but not limited to, pavement, curb and gutter, 7' sidewalk, 5' landscape, parkway w/ street trees, street lighting, utility relocations and undergrounding, striping, signage, 30' radius curb returns, and median improvements.
 - Response: Dedication along Lovers Lane frontage is proposed for a 110' ultimate right of way. Frontage dedication matches previous dedication to the north. Returns have been revised to a 30' flowline radius.





Respectfully,

VVH CONSULTING ENGINEERS

Adam Reed Senior Designer

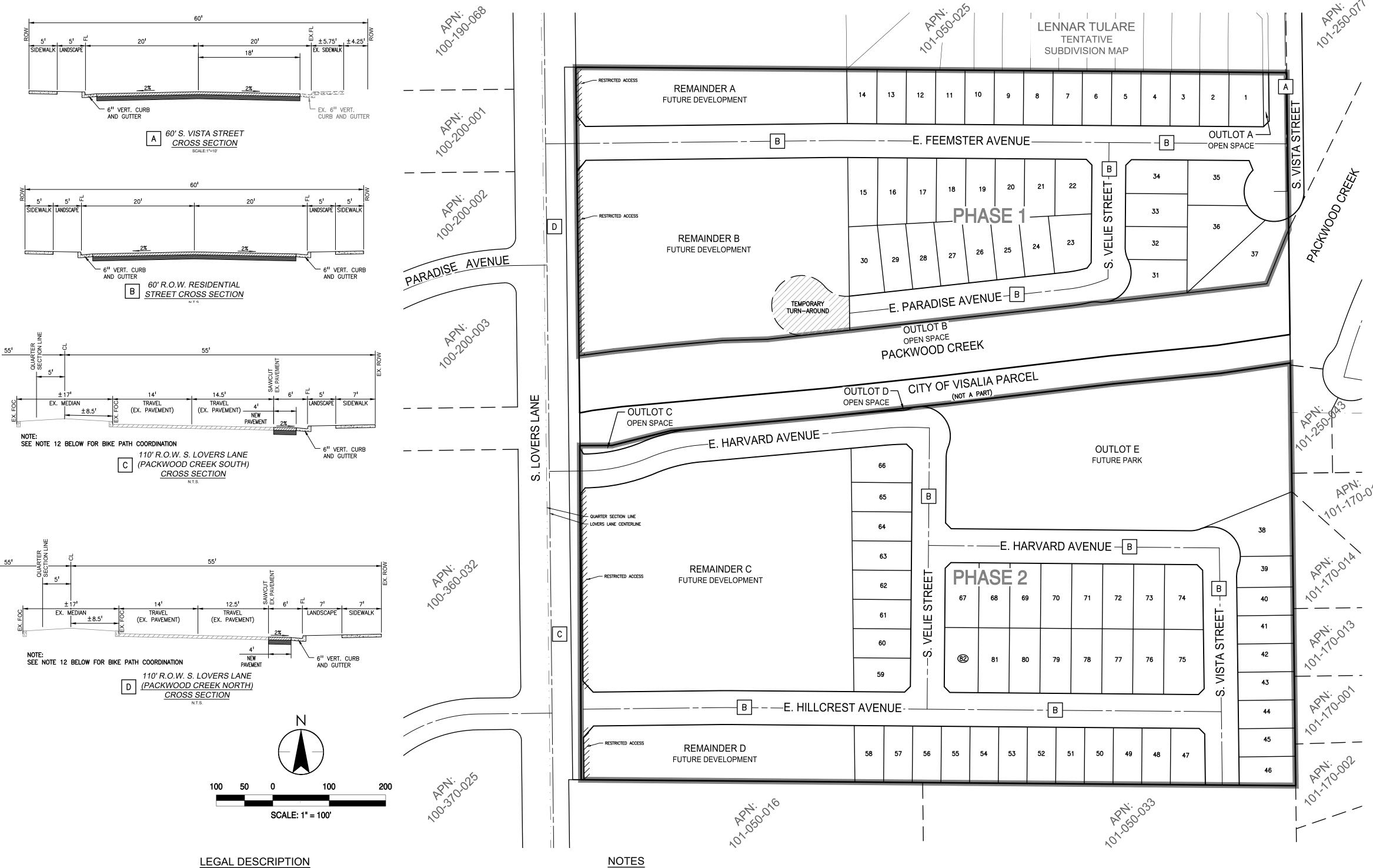
Tel.: (209) 568-4477 Fax: (209) 568-4478 areed@vvhce.com

c. File

rsp_letter_20211014.docx

TENTATIVE SUBDIVISION MAP VISALIA 35

A PORTION OF THE WEST 1/2 SECTION 34, T 18S, R 25E, CITY OF VISALIA, TULARE COUNTY, CALIFORNIA



THE LAND REFERRED TO HEREIN BELOW IS SITUATED IN THE CITY OF VISALIA, COUNTY OF TULARE, STATE OF

The Northwest Quarter of the Southwest Quarter; and the North half of the Southwest Quarter of the Southwest Quarter, all in Section 34, Township 18 South, Range 25 East, Mount Diablo Base and Meridian, in the City of Visalia, County of Tulare, State of California, according to the Official Plat thereof.

EXCEPTING therefrom a strip of land 2 rods off the West side of the Northwest Quarter of the Southwest Quarter and the North half of the Southwest Quarter of the Southwest Quarter of said Section 34.

ALSO EXCEPTING THEREFROM the North 720 feet of the Northwest Quarter of the Southwest Quarter of Section 34, Township 18 South, Range 25 East, Mount Diablo Base and Meridian, in the County of Tulare, State of California, according to the Official Plat of the Survey of said land on file in the Bureau of Land Management at the date of the issuance of the patent thereof.

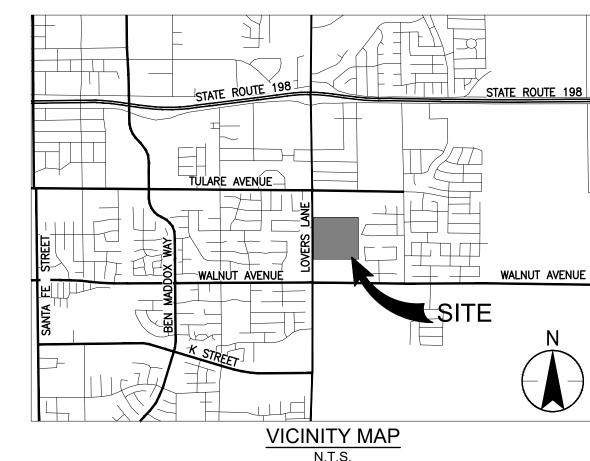
ALSO EXCEPTING THEREFROM the West 33 feet thereof.

ALSO EXCEPTING THEREFROM the West 60 feet of the North 720 feet of the Northwest Quarter of the Southwest Quarter of Section 34, Township 18 South, Range 25 East, Mount Diablo Base and Meridian, according to the Official Plat of the Survey of said land on file in the Bureau of Land Management at the date of the issuance of the patent thereof.

ALSO EXCEPTING THEREFROM that portion conveyed to the City of Visalia, a municipal corporation by Grant Deed recorded October 9, 2017, as Instrument No. 2017-62355, of Official Records.

- 1. THIS EXHIBIT IS FOR TENTATIVE MAP PURPOSES ONLY. ALL SITE CHARACTERISTICS SHALL BE VERIFIED PRIOR TO FINAL MAP.
- 2. A 10' PUBLIC UTILITY EASEMENT (P.U.E. OF PUE) WILL BE LOCATED ADJACENT TO AND PARALLEL WITH ALL PUBLIC RIGHT OF WAYS.
- 3. PURSUANT TO GOVERNMENT CODE SECTION 66456.1, THE SUBDIVIDER MAY FILE MULTIPLE FINAL MAPS BASED UPON THIS TENTATIVE SUBDIVISION MAP. THE FILING OF A FINAL MAP ON A PORTION OF THIS TENTATIVE SUBDIVISION MAP SHALL NOT INVALIDATE ANY PART OF THIS
- TENTATIVE SUBDIVISION MAP. 4. LOT NUMBERS ARE FOR IDENTIFICATION PURPOSES ONLY.
- 5. FIRE HYDRANTS AND ELECTROLIERS ARE TO BE DESIGNED AND LOCATED PER CITY OF VISALIA STANDARDS AND SPECIFICATIONS.
- 6. UTILITY SIZING, LOCATION, CONNECTION POINTS, STREET GRADES, PAD ELEVATIONS AND LOT DIMENSIONS ARE PRELIMINARY ONLY AND SUBJECT TO FINAL ENGINEERING DESIGN.
- 7. ALL UTILITIES WILL BE PLACED UNDERGROUND WITHIN THE PUBLIC RIGHT OF WAY OR PUBLIC UTILITY EASEMENTS. PUBLIC UTILITY EASEMENTS WILL BE PROVIDED AS REQUIRED BY THE CITY OF VISALIA AND UTILITY COMPANIES.
- 8. THE BOUNDARY INFORMATION IS BASED UPON A FIELD SURVEY PERFORMED BY VVH CONSULTING ENGINEERS.
- 9. FINAL LANDSCAPE AND IRRIGATION PLANS ARE TO BE SUBMITTED ALONG WITH FINAL IMPROVEMENT PLANS.
- 10. SUBDIVISION SIGNAGE PER CITY OF VISALIA REQUIREMENTS. 11. TOPOGRAPHICAL SURVEY PERFORMED BY VVH CONSULTING ENGINEERS ON 10-31-2019.

- 12. A CLASS 4 BIKE PATH IS TO BE CONSTRUCTED ALONG THE ENTIRE PROJECT FRONTAGE OF LOVERS LANE AND MAY BE PHASE BASED ON THE PROJECT PHASING SHOWN ON THIS TENTATIVE MAP AND/OR AS APPROVED BY THE CITY OF VISALIA. THE DEVELOPER SHALL COORDINATE WITH THE CITY OF VISALIA THE DESIGN OF THE CLASS 4 BIKE PATH DURING THE CIVIL IMPROVEMENT PORTION OF THE PROJECT.
- 13. THE INTERSECTION OF E. HARVARD AVENUE AND S. LOVERS LANE WILL BE DESIGNED TO BE COMPATIBLE WITH THE APPROVED PACKWOOD CREEK BIKE TRAIL AND PEDESTRIAN CROSSING. THE PROPOSED CURB RAMP TO BE CONSTRUCTED WITH THE PACKWOOD CRREK TRAIL AND PEDESTRIAN PROJECT MAY BE REMOVED AND RECONSTRUCTED WITH A RETURN CURB RAMP WITH BULB-OUT AS APPROVED BY THE CITY OF VISALIA DURING THE CIVIL IMPROVEMENT PORTION OF THE PROJECT.



TENTATIVE MAP INFORMATION

FOREBAY FARMS, LLC PO BOX 2717 MERCED, CA 95344 **DEVELOPER:** FOREBAY FARMS, LLC PO BOX 2717 MERCED, CA 95344 **ENGINEER: VVH CONSULTING ENGINEERS** 430 10TH STREET MODESTO, CA 95354 PH. 209.568.4477

CASEY BARKMAN: cbarkman@vvhce.com ASSESSORS PARCEL NUMBER: ±35.07 ACRES PARCEL SIZE: **EXISTING ZONING:**

O-PA PROFESSIONAL/ADMINISTRATIVE OFFICE R-M-2 MULTI-FAMILY RESIDENTIAL R-1-5 SINGLE-FAMILY RESIDENTIAL OS OPEN SPACE EXISTING GENERAL PLAN DES.: LOW DENSITY RESIDENTIAL

MEDIUM DENSITY RESIDENTIAL

OFFICE PARKS/RECREATION **EXISTING USE:** VACANT/UNDEVELOPED

PROPOSED LOT SIZE SQUARE FOOTAGE R-1-5 (LOW DENSITY RES.): 5,000 6,000

ZONING DENSITY R-1-5 (LOW DENSITY RES.) R-M-2 (MULTI-FAMILY RES.) 10.28 O-PA (OFFICE-PRO. ADMIN. **OPEN SPACE RIGHT OF WAY** TOTAL 35.07 35.07

REMAINDER TABLE FUTURE DEVELOPMENT 1.11 AC 3.58 AC FUTURE DEVELOPMENT 4.42 AC FUTURE DEVELOPMENT

1.09 AC FUTURE DEVELOPMENT 910 SF PARK STRIP (OPEN SPACE)

2.88 AC OPEN SPACE (DEDICATION TO THE CITY OF VISALIA) 1,558 SF OPEN SPACE (DEDICATION TO THE CITY OF VISALIA) 202 SF OPEN SPACE (DEDICATION TO THE CITY OF VISALIA) PARK (OPEN SPACE) 3.50 AC

OPEN SPACE TOTAL - 6.44 AC (18.36% NET)

CITY OF VISALIA SEWER: **CALIFORNIA WATER** WATER: CITY OF VISALIA STORM DRAIN: CITY OF VISALIA GARBAGE: ELECTRIC: SOUTHERN CALIFORNIA EDISON SOUTHERN CALIFORNIA GAS CABLE: XFINITY

TELEPHONE: FIRE PROTECTION: CITY OF VISALIA SCHOOL DISTRICT: VISALIA UNIFIED SCHOOL DISTRICT

06107C0934E EFFECTIVE DATE: 06-16-2009 PANEL: COMMUNITY: CITY OF VISALIA, 060409

X; 0.2% ANNUAL CHANCE OF FLOOD; 1% ANNUAL CHANCE ZONE: FLOOD WITH AVERAGE DEPTHS OF LESS THAN 1 FOOT

R-1-5 ZONING SETBACKS FRONT (EXTERIOR)

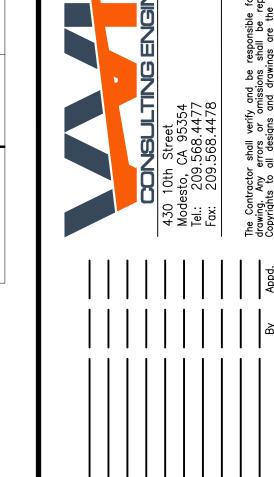
FLOOD ZONE

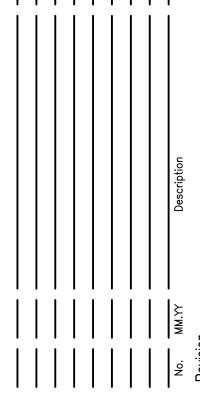
FRONT (EXTERIOR) CUL-DE-SAC/KNUCKLE

SIDE (INTERIOR) SIDE (EXTERIOR)

22' GARAGE 15' LIVING 20' GARAGE

15' LIVING SPACE





Engineer's Seal

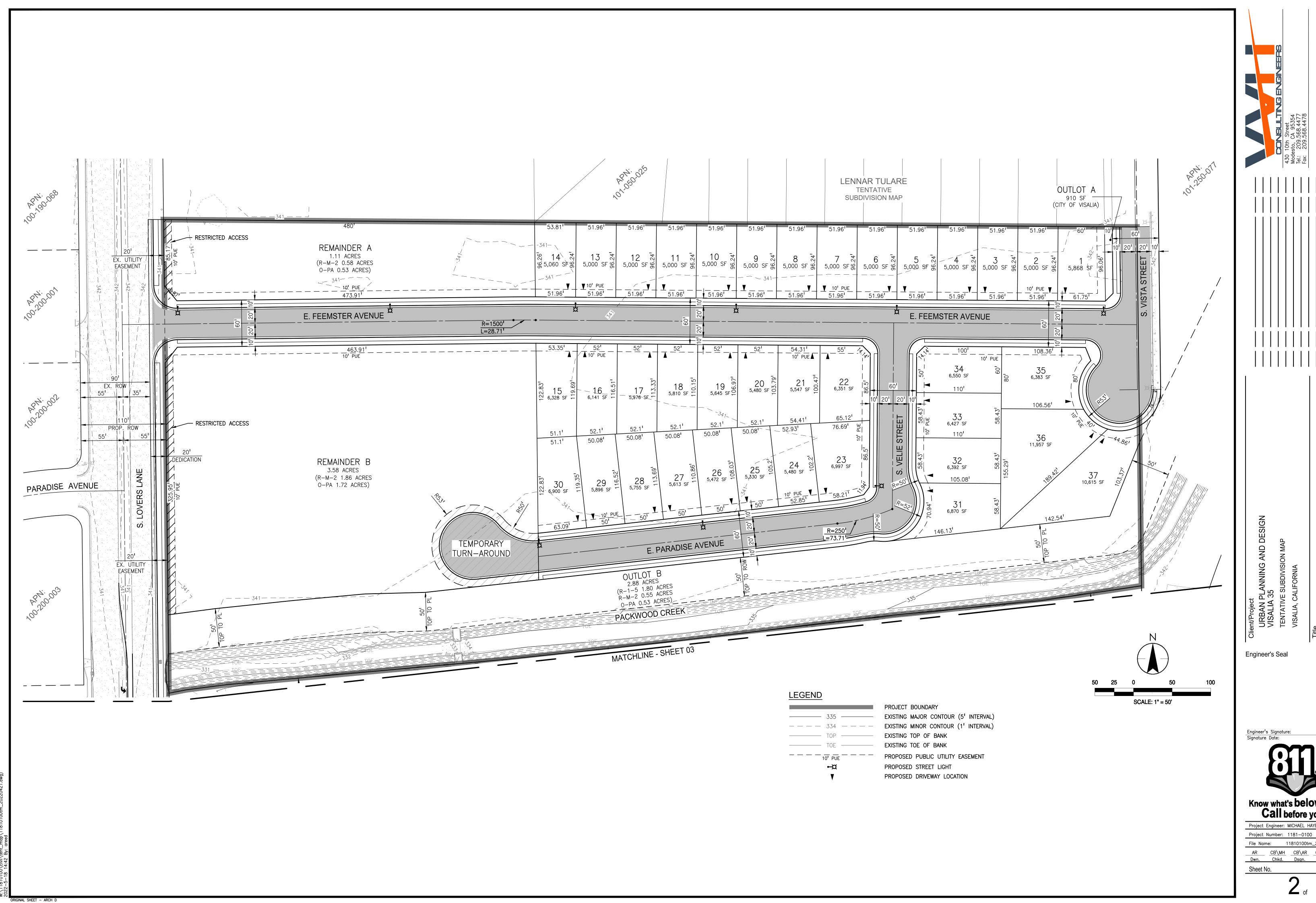


Call before you dig.

Project Engineer: MICHAEL HAYES Project Number: 1181-0100

AR ___CB\MH __CB\AR __09.30.21_ Sheet No.

File Name: 11810100tm_20220421.dwg





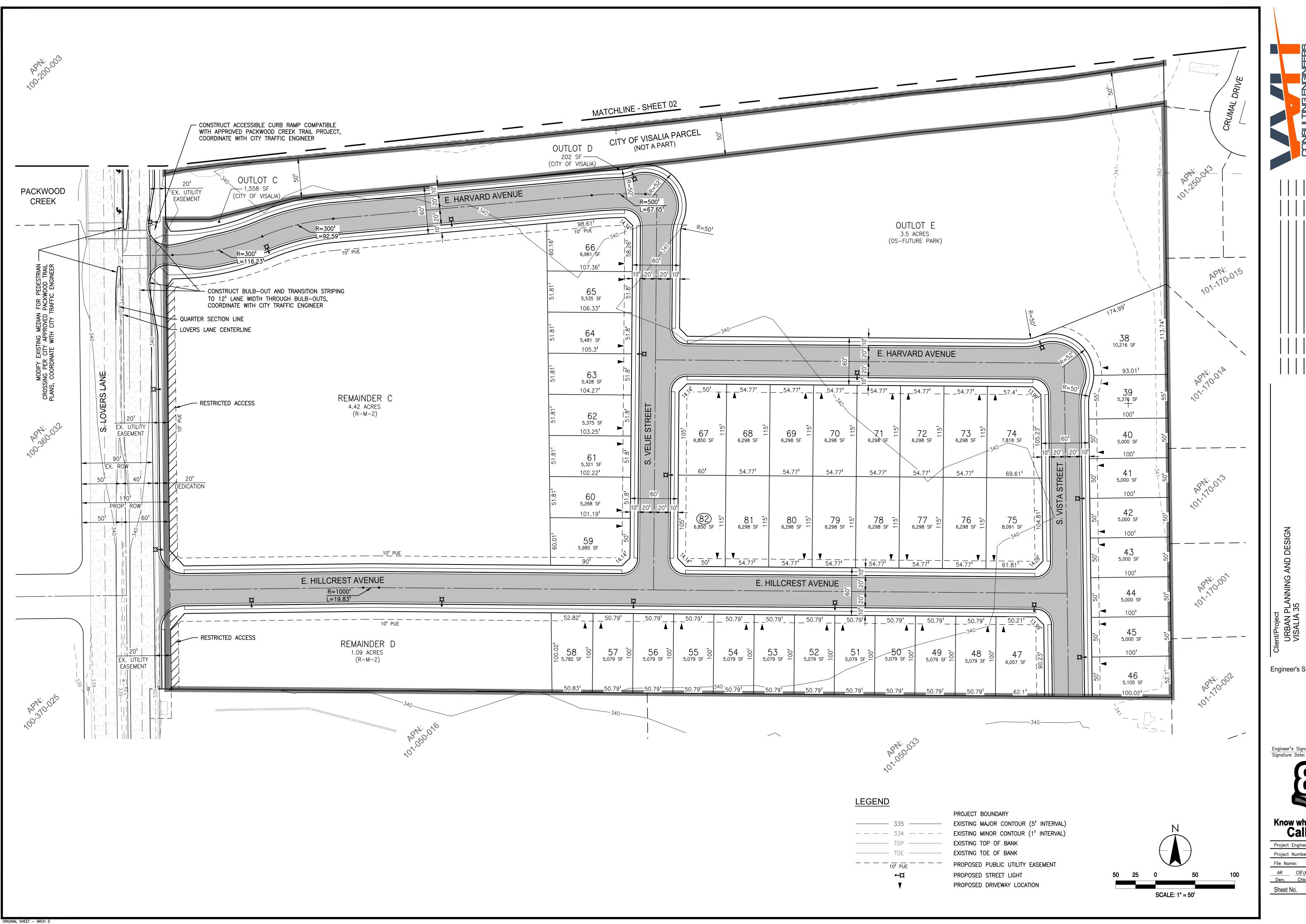
Know what's below.

Call before you dig.

Project Engineer: MICHAEL HAYES

File Name: 11810100tm_20220421.dwg
 AR
 CB\MH
 CB\AR
 09.30.21

 Dwn.
 Chkd.
 Dsgn.
 MM.DD.YY



Engineer's Seal



Know what's below.

Call before you dig.

Project Engineer: MICHAEL HAYES Project Number: 1181-0100

File Name: 11810100tm_20220421.dwg
 AR
 CB\MH
 CB\AR
 09.30.21

 Dwn.
 Chkd.
 Dsqn.
 MM.DD.YY

CITY OF VISALIA SITE PLAN REVIEW APPLICATION

- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -- Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting -Project/Business Name: Date: 5/19/2022 125 S. Crenshaw 34 Lot Single Family Subdivsion Project Description: GENERAL PROJECT INFORMATION Yes X No O If Resubmittal, Previous Site Plan Review Number: Site Plan Review Resubmittal: 22005 Property Owner: Applicant(s) Name: Bitta Toor Project Address/Location: 125 S. Chrenshaw St., Visalia, CA 93291 Assessor Parcel Number: 0 8 5 - 1 3 0 - 0 0 2 Parcel Size (Acreage or Square Feet): Building or Suite Square Footage: 6.77 Acres N/A Are There Any Proposed Building Modifications: Yes No (X) -- THIS AREA FOR CITY STAFF USE ONLY ---Estimated Cost of Modifications to Building: Date Received: Describe All Proposed Building Modifications: Vacant Lot SPR Agenda: Item No. Zone: _____ SPR No. 22-005 Yes () Historic District: X/AE Flood Zone: AE() - - A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS - -N/A Existing/Prior Building Use: N/A Proposed Building Use: N/A Proposed Hours of Operation: OPERATIONS & TRAFFIC INFORMATION Days of Week In Operation (Circle): Su M T W Th F Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existing Proposed N/A Predicted Peak Operating Hour: N/A Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees (Provide Separate Attachment if Necessary): N/A Describe Any Special Events Planned for the Facility:

Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS | | | | | | | |
|------------------------|--|--|--|--|--|--|--|--|
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies | | | | | | | |
| ENTS | not accepted). | | | | | | | |
| REM | ⇒ Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. | | | | | | | |
| EQUI | ⇒ Site plan shall provide for and indicate all of the following: | | | | | | | |
| SITE PLAN REQUIREMENTS | - North arrow - Existing & proposed structures - Loading/unloading areas | | | | | | | |
| E PL | All existing & proposed site features Adjacent street names Accessible path of travel from right of way Site dimensions, including building Refuse enclosures & containers Accessible path of travel from ADA stall | | | | | | | |
| SIT | - Existing and proposed fencing at site - Valley oak trees (show drip line) - Location and width of drive approaches to site | | | | | | | |
| | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements | | | | | | | |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 | | | | | | | |
| | Applicant Information (Final comments will be mailed to the name and address provided below) | | | | | | | |
| URE | Name: Bitta Toor Signature of Owner or Authorized Agent* | | | | | | | |
| NAT | Name: Bitta Toor Address: 27725 Rd 92 Signature of Owner or Authorized Agent* | | | | | | | |
| SIG C | City, State, Zip Visalia, CA 93277 Owner Date | | | | | | | |
| IREC | Phone: 559-690-9024 | | | | | | | |
| REQUIRED SIGNATURE | Email: bt5323@gmail.com Authorized Agent* Date | | | | | | | |
| | * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. | | | | | | | |
| | | | | | | | | |
| | AGENCY AUTHORIZATION | | | | | | | |
| | OWNER: | | | | | | | |
| | Santokh S. Toor & Arpinder K. Toor , declare as follows; I am the owner of certain real property bearing assessor's | | | | | | | |
| | parcel number (APN): | | | | | | | |
| | 085-130-002 | | | | | | | |
| | AGENT: | | | | | | | |
| | AME : AN AND THE STATE OF THE S | | | | | | | |
| Σ | I designate <u>AW Engineering - Allen Williams</u> , to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to Tentative Subdivision Map | | | | | | | |
| FORM | relative to the property mentioned herein. | | | | | | | |
| TION | I declare under penalty of perjury the foregoing is true and correct. | | | | | | | |
| RIZA | 11 | | | | | | | |
| THO | Executed this11day ofJanuary | | | | | | | |
| AGENCY AUTHORIZATION | Signatures Signatures | | | | | | | |
| SENC | OWNER AGENT | | | | | | | |
| A | BM M | | | | | | | |
| | Signature of Owner Signature of Agent | | | | | | | |
| | 27725 Road 92 | | | | | | | |
| | Owner Mailing Address Agent Mailing Address | | | | | | | |
| | Visalia, CA 93277 Visalia, CA 93292 | | | | | | | |
| | 559-690-9024 | | | | | | | |
| | Owner Profile Number | | | | | | | |
| | | | | | | | | |

Page 2 of 2

CITY OF VISALIA SITE PLAN REVIEW APPLICATION

- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.vlsalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -- Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting -5/19/22 Visalia Plaza 39/Seefried Project/Business Name: Date: New Construction of a 535,540 sf industrial building and Project Description: GENERAL PROJECT INFORMATION associated improvements. Yes No Site Plan Review Resubmittal: If Resubmittal, Previous Site Plan Review Number: SPR 22-041 Seefried Industrial Properties, Inc. Property Owner: Applicant(s) Name: Bryan Frarey Project Address/Location: Northeast corner of W. Goshen Ave. and Rd. Assessor Parcel Number: 0 7 7 _ 1 1 1 _ 0 4 6 and 0 7 7 - 1 1 1 - 0 4 7 Building or Suite Square Footage: 535,540 sf 39.25 acres Parcel Size (Acreage or Square Feet): Are There Any Proposed Building Modifications: Yes () No (X) --- THIS AREA FOR CITY STAFF USE ONLY ---Estimated Cost of Modifications to Building: Date Received: SPR Agenda: _____ Item No. ___ Describe All Proposed Building Modifications: Zone: SPR No. 22-041 Yes No Historic District. AE XIAE Flood Zone: - - A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS - -N/AExisting/Prior Building Use: General Light Industrial Proposed Building Use: Proposed Hours of Operation: 24 hours a day OPERATIONS & TRAFFIC INFORMATION Days of Week In Operation (Circle): Su M T W Th F Sa daily N/A842 (estimated with ITE) Existina Number of Employees Per Day: Proposed N/A0 Number of Customers Per Day (Estimated): Existing Proposed 7-8 AM and 4 - 5 PM Predicted Peak Operating Hour: N/A Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees (Provide Separate Attachment if Necessary): See attached TIA Scope of Work N/A Describe Any Special Events Planned for the Facility:

Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS |
|---------------------------|---|
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies |
| Ę | not accepted). |
| SITE PLAN REQUIREMENTS | Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. |
| ion. | Site plan shall provide for and indicate all of the following: |
| 3 | - North arrow - Existing & proposed structures - Loading/unloading areas |
| PLA | - All existing & proposed site features Adjacent street names Accessible path of travel from right of way - Site dimensions, including building Refuse enclosures & containers - Accessible path of travel from ADA stall |
| E | Site dimensions, including building Refuse enclosures & containers Accessible path of travel from ADA stall Existing and proposed fencing at site Valley oak trees (show drip line) Location and width of drive approaches to site |
| | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (Include ADA) of Visalla Municipal Code Section 16 |
| | Applicant Information (Final comments will be mailed to the name and address provided below) |
| 3 | Name: Bryan Frarey Signature of Owner or Authorized Agent* |
| FA | Address: 2201 E Camelback, Ste 222 Address: 9.19.7022 |
| SIG | City, State, Zip Phoenix, AZ 85016 |
| RED | Phone: 602.390.1928 |
| REQUIRED SIGNATURE | Email: bfrarey@seefriedproperties.com Authorized Agent* Date |
| - | * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | |
| | |
| | AGENCY AUTHORIZATION |
| | OWNER: |
| | |
| | OWNER: |
| | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's |
| | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's |
| | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): AGENT: |
| W. | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to |
| FORM | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file |
| ZATION FORM | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to |
| JORIZATION FORM | OWNER: I, |
| UTHORIZATION FORM | OWNER: I, |
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| AGENCY AUTHORIZATION FORM | OWNER: I, |
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Page 2 of 2



MEMORANDUM

To: Josh Dan / Planning Division Tel: 559-713-4003

City of Visalia

Date: May 19, 2022

Subject: Visalia Plaza 39 / Seefried (Site Plan No. 2022-041) APN No. 077-111-047

RESPONSE TO COMMENTS:

PLANNING DIVISION/PROJECT SPECIFIC INFORMATION:

1. Comment: There is no staff support for development upon the future railroad spur (refer to development to the north were develop upon the easement was avoided).

Response: All surface improvements have been removed from the rail easement. See Sheet HC.

2. Comment: Parking on site to comply with the parking requirements of VMC 17.34, but should the applicant not be able to meet the 1:1,000 parking ratio an Operational Statement detailing the proposed uses, number of employees during the busiest shift, and any other relevant operational detail may be used to determine the parking demand on site.

Response: This site plan proposes 549 total auto parking stalls, which meets the 1:1,000 required parking ratio. See the Parking Table on Sheet HC.

3. Comment: A tree well shall be provided for every 10 consecutive parking stalls.

Response: A tree well is provided every 10 consecutive parking stalls. See Sheet HC.

4. Comment: The site plan shall verify that a minimum 10% of the parking lot is landscaped.

Response: This site plan proposes a minimum of 10% landscaping in the parking lot. See Proposed Site Area Distribution on Sheet HC.

5. Comment: The applicant shall submit landscaping and irrigation plans with the Building Permit submittal.

Response: Acknowledged. This will be provided with the Building Permit submittal.

6. Comment: Provide detail on all existing and proposed fencing onsite- i.e.: location, material, and height.

Response: 7' tall black PVC coated chain link fencing is shown on Sheet HC along Road 76 and around the secured truck courts. The fence on this project will match the fence on the adjacent property to the north.



7. Comment: Requirements from other divisions may require changes to the site design may require resubmittal for Site Plan Review.

Response: Acknowledged.

8. Comment: Fence height is limited to 7 feet in height (10 feet height is not allowed).

Response: Fence height has been revised to 7'. See Sheet HC.

9. Comment: The parking along the southeast must provide a 25-foot side setback as measured from railroad right-of-way lot line.

Response: The parking now sits 28' from the property line. See Sheet HC.

10. Comment: Provide additional information as requested by the Traffic and Engineering Divisions.

Response: Acknowledged. See comment responses below.

SITE PLAN REVIEW COMMENTS:

1. Comment: Install curb and gutter PRIVATE STREET

Response: Curb and gutter on Private Street is labeled on Sheet HC.

 Comment: Drive approach size: 41' MAX; Use radius return; REFER TO CITY COMMERCIAL STDS

Response: The driveway widths were set as a function of truck turning movements. The driveways connect to the private street. A modified City standard driveway is proposed for the ingress and egress to the site. See Sheet HC.

3. Comment: Sidewalk: 5'- 6' width

Response: A proposed six-foot (6') sidewalk on the Private Street is shown on Sheet HC.

4. Comment: 5' parkway width at AMERICAN & PRIVATE ST

Response: A five-foot (5') parkway on Road 76 is shown on Sheet HC. To maximize onsite stormwater basin storage, additional landscaping is provided behind the sidewalk on the Private Street.

5. Comment: Repair and/or replace any sidewalk across the public street frontage(s) of the subject site that has become uneven, cracked or damaged and may constitute a tripping hazard.

Response: Acknowledged. This will be addressed during the construction document engineering phase of this project.

6. Comment: Replace any curb and gutter across the public street frontage(s) of the subject site that has become uneven and has created areas where water can stand.

Response: Acknowledged. This will be addressed during the construction document engineering phase of this project.

Comment: Right-of-way dedication required. A title report is required for verification of ownership.
 AMERICAN

Response: Project will provide required dedication of right-of-way to the City. A title report has been provided with the previous resubmittal.



 Comment: Deed required prior to issuing building permit; RIGHT-OF-WAY FOR PUBLIC STREETS

Response: Acknowledged.

9. Comment: City Encroachment Permit Required. FOR ALL WORK WITHIN THE PUBLIC RIGHT-OF-WAY. Insurance certificate with general & auto liability (\$1 million each) and workers compensation (\$1 million). valid business license, and appropriate contractor's license must be on file with the City, and valid Underground Service Alert # provided prior to issuing the permit. Contact Encroachment Tech. at 713-4414.

Response: Acknowledged.

10. Comment: Landscape & irrigation improvement plans to be submitted for each phase. Landscape plans will need to comply with the City's street tree ordinance. The locations of street trees near intersections will need to comply with Plate SD—1 of the City improvement standards. A street tree and landscape master plan for all phases of the subdivision will need to be submitted with the initial phase to assist City staff in the formation of the landscape and lighting assessment district.

Response: Acknowledged. This will be addressed during the Building Permit phase of this project.

11. Comment: Grading & Drainage plan required. If the project is phased, then a master plan is required for the entire project area that shall include pipe network sizing and grades and street grades. [X] Prepared by registered civil engineer or project architect. [X] All elevations shall be based on the City's benchmark network. Storm run-off from the project shall be handled as follows: a) [X] directed to the City's existing storm drainage system; b) [X] directed to a permanent on-site basin; or [] directed to a temporary on-site basin is required until a connection with adequate capacity is available to the City's storm drainage system. On-site basin: maximum side slopes, perimeter fencing required, provide access ramp to bottom for maintenance. CAPTURE ONSITE DRAINAGE IN PRIVATE RETENTION SWALES/BASINS, FURTHER REVIEW AND COORDINATION WITH CITY ENGINEER REQUIRED FOR PUBLIC STREET DRAINAGE. PROVIDE SD DESIGN CALCS AND SUPPORTING MATERIALS / SUBSURFA CE CHAMBER

Response: Acknowledged. Basin volume calculations are provided on Sheet G-1. Subsurface storage details are shown on Sheet G-2. Kimley-Horn will coordinate with the City Engineer for public street drainage during the construction document engineering phase of the project.

12. Comment: Grading permit is required for clearing and earthwork performed prior to issuance of the building permit.

Response: Acknowledged.

13. Comment: Show finish elevations. (Minimum slopes: A.C. pavement = 1%. Concrete pavement = 0.25%. Curb & Gutter = 0.20%, V-gutter = 0.25%)

Response: Minimum slopes are shown on Sheet G-1 and G-2.



14. Comment: Show adjacent property grade elevations. A retaining wall will be required for grade differences greater than 0.5 feet at the property line.

Response: All grades around the property perimeter match those of the existing grades at the property line. See elevations labeled on Sheets G-1 and G-2. The existing contours are also now shown on Sheets G-1 and G-2.

15. Comment: All public streets within the project limits and across the project frontage shall be improved to their full width, subject to available right of way, in accordance with City policies, standards and specifications. 1/2 STREET AMERICAN (DEFERRED), NEW PRIVATE STREET.

Response: The future right-of-way, curb and gutter, parkway, and sidewalk for Road 76 are shown on Sheet HC. Curb, gutter, and sidewalk are shown on the Private Street on Sheet HC.

 Comment: Traffic indexes per city standards: REFER TO CITY COLLECTOR AND LOCAL STREET STDS

Response: Acknowledged.

17. Comment: Install street striping as required by the City Engineer. **TO BE DETERMINED AT CIVIL REVIEW.**

Response: Acknowledged.

18. Comment: Install landscape curbing (typical at parking lot planters). ONSITE PER DESIGN.

Response: Planter islands are proposed in the parking lots. See Sheet HC. A Landscape Plan will be provided during the Building Permit phase of the project.

19. Comment: Minimum paving section for parking: 2" asphalt concrete paving over 4" Class 2 A99. Base, or 4" concrete pavement over 2" sand.

Response: The proposed pavement sections from the Geotechnical Engineer satisfy these minimum requirements. See the Legend on Sheet G-1 and G-2.

20. Comment: Design Paving section to traffic index of 5.0 min. for solid waste truck travel path.

Response: The proposed pavement section meets this minimum requirement. See G-1 and G-2 for pavement sections.

21. Comment: Provide "R" value tests: 1 each at 300' INTERVALS

Response: This will be provided during the construction document engineering phase of this project for construction within the public right-of-way.

22. Comment: Show Valley Oak trees with drip lines and adjacent grade elevations. [X] Protect Valley Oak trees during construction in accordance with City requirements.

Response: A Landscape Plan will be provided during the Building Permit phase of this project. Protection of Valley Oak Trees during construction will be in conformance with City requirements.

23. Comment: Relocate existing utility poles and/or facilities. **REQUIRED WITH PUBLIC IMPROVEMENTS.**

Response: Should existing utility poles or facilities require relocation, this will be provided during the construction document phase of this project.



24. Comment: Underground all existing overhead utilities within the project limits. Existing overhead electrical lines over 50kV shall be exempt from undergrounding. **REQUIRED WITH PUBLIC IMPROVEMENTS.**

Response: Client will coordinate with the power purveyor for existing overhead power lines located in the existing easement along southerly property line. This will be provided during the construction document phase of this project.

25. Comment: Fugitive dust will be controlled in accordance with the applicable rules of San Joaquin Valley Air District's Regulation VIII. Copies of any required permits will be provided to the City.

Response: Acknowledged.

26. Comment: If the project requires discretionary approval from the City, it may be subject to the San Joaquin Valley Air Districts Rule 9510 Indirect Source Review per the rule's applicability criteria. A copy of the approved AIA application will be provided to the City.

Response: Acknowledged.

27. Comment: If the project meets the one acre of disturbance criteria of the State's Storm Water Program, then coverage under General Permit Order 2009—0009—DWQ Is required, and a Storm Water Pollution Prevention Plan (SWPPP) is needed. A copy of the approved permit and the SWPPP will be provided to the City.

Response: Acknowledged.

ADDITIONAL COMMENTS:

1. Comment: Proposed development will incur impact fees based on acreage of site improvement and building square footage. Refer to page 4 for applicable fees.

Response: Acknowledged.

2. Comment: Rd 76 is a collector roadway identified in the City's Circulation Element and Transportation Impact Fee program. Portions of improvements will qualify as reimbursable in the form of impact fee credits. Site plan layout needs to show adequate ultimate widening dimensions along street frontage. Completion of min. east half-street improvements would be required however it is likely that majority of improvements will need to be deferred due to an existing railroad easement that traverses the westerly parcel boundary. This easement impacts full build-out of Rd 76. Applicant will be required to deposit in cash to the City the cost of the developer responsible improvements along the project frontage as part of project conditions and prior to building permit issuance. Developer is responsible for a 6' sidewalk, street lighting, curb & gutter, parkway landscaping, right-of-way dedication, utility relocations, a 15% inflater for design and construction management, and six-foot wide pavement along development frontage. Further coordination with City Engineer is required.

Response: Half-street improvement dimensions along with existing and proposed right of way lines on the Road 76 frontage are shown on Sheet HC. Sidewalk, street lighting, curb & gutter, and parkway are all shown and labeled on Sheet HC. It has been noted that the street improvements along Road 76 are deferred.

3. Site plan provides dimensions and improvement design information along Rd 76 project frontage as previously requested. The proposed 42-foot dedication from street centerline (which is also County/Section line) appears to be adequate. The existing County street right-of-way appears to



be 40-feet west of the County/Section line. Per City records, previous right-of-way dedications along Rd 76 in the vicinity have been measured from the street centerline (County/Section line).

Response: Acknowledged.

4. The dedication of right-of-way and any easements will need to be included with the project submittals. Further coordinate with City Engineer for deed format and processing.

Response: Acknowledged.

5. Comment: Proposed project is subject to previous development conditions set forth for the 1M sq. ft. building to the north. City agreed to abandon street right-of-way to allow the east/west street to be privately owned/maintained. Staff was in agreement that the onsite access road does not need to be designated as a public street, as per previous development conditions, and the private drive request was supported. Design of the private drive to be similar to City 60' local street design; however, an increased traffic index should be utilized to handle heavier traffic loads.

Response: Acknowledged. The private street pavement will be designed to accommodate the traffic entering this site.

6. Comment: The private access road was designed with an industrial type cul-de-sac, as shown, however the cul-de-sac was considered an interim solution until future connection to American(Rd 76) could be made. Access (permanent or temporary) was to be determined as future development interest of the vacant land was proposed. Per the site plan layout, the proposed drive approach on American would not be supported at this time.

Response: Acknowledged.

7. Should the connection to Rd 76 be deemed necessary, even in an interim design, the proposed westerly drive access on the private road would be too close in proximity to the intersection of Rd 76 & private street. Relocate to approx. 200' from intersection.

Response: The westerly driveway has been relocated to sit roughly 200' away from the location of any potential future connection to Rd 76. See Sheet HC.

8. Comment: Ensure infrastructure does not encroach into existing easements onsite (railroad, SCE, etc.). Provide documentation of acceptance of any proposed private improvements over, under, or across existing easements. Staff recommends applicant pursue abandonment of the rail easement to allow proposed improvements onsite.

Response: All infrastructure has been removed from the onsite easements. See Sheet HC.

- 9. Comment: Project to extend sewer and storm mains accordingly, to extents of parcel limits.
 - Response: A public sewer line is shown on sheet UT-1, extending across the full property frontage. There are no storm mains present surrounding the project property. Kimley-Horn will coordinate with the City Engineer during the construction document engineering phase for public storm drain requirements.
- 10. Comment: Required public improvements shall include, but may not be limited to, pavement, street lighting, sidewalk, parkway landscaping, public storm drainage swales, curb & gutter, signal install/modifications & conduit, curb returns, and street striping.

Response: Acknowledged. Street lighting is shown on Sheet HC. Curb, gutter, and sidewalk are shown on the Private Street and Road 76.



- 11. Comment: Parking lot to comply with City parking lot standards.
 - Response: The parking lot design complies with City standards. See Sheet HC.
- Comment: Site accessibility to comply with current City and building codes. Raised accessible walkways will affect grade design onsite. Accessible path of travel to be provided to the public right-of-way.
 - Response: An accessible path of travel to the right of way is shown on Sheet HC and grading is shown on Sheet G-1 and G-2. Raised walkways will be provided per current City and building codes.
- 13. Comment: Project to retain storm water onsite, including private drive, however the future Rd 76 storm run-off may need to be collected within the landscape setback along street. Site plan is not clear on cross section dimensioning. include setback distance and indicate use of landscape setback and possible swale retention of public run-off- to be determined. Further research is being conducted by City staff as to the master planned storm water capture for the area.
 - Response: Acknowledged. Kimley-Horn will coordinate with City Engineer during construction document engineering phase.
- 14. Comment: Further determination of improvements on Rd 76 to utilize as secondary access will be conducted with site plan resubmittal. Improvements that are temporary but necessary as a means for safety to allow access (providing adequate street lighting, striping & signage, pavement transitions, etc.) are cast responsibility of the developer.
 - Response: Secondary access from Road 76 has been eliminated. See Sheet HC-1. We have provided an emergency access for the fire department.
- 15. The provided emergency access road connection to Rd 76 would require additional pavement improvements up to existing County road. Refer to min. engineered road section requirements per Fire Dept.
 - Response: The emergency access road connection to Rd 76 has been removed. See Sheet HC.
- 16. Comment: Sewer connection, as shown, shall be by proper City std manhole and any additional sewer improvements thereafter (needed for the lift station) would need to be installed on private property and not in public right-of-way.
 - Response: Acknowledged. The sewer lift station is proposed on private property. See UT-1 and UT-2.
- 17. Comment: It is recommended sidewalks and curb ramps are installed along private street to provide accessibility onsite. Street lighting for the private drive is also highly encouraged.
 - Response: Sidewalk and curb ramps are provided along the Private Street. See Sheet HC for location and for ADA path of travel.
- 18. Comment: Site plan layout to indicate desired fencing along frontages. Fencing subject to setback requirements.
 - Response: Site fencing is proposed around the onsite truck courts and along Road 76 to match the property to the north of this project. The fencing will be 7' chain link per notation on Sheet HC.



19. Comment: Public street lighting to be designed to City collector standards, refer to City std details. Provide an electrical design plan with voltage drop calcs, to be submitted with civil drawings. A new service pedestal may be necessary.

Response: Acknowledged. Electrical design will be provided with construction documents.

20. Comment: Coordinate with County of Tulare for any work within existing Rd 76 (American).

Response: Acknowledged.

21. Comment: Site plan indicates new curb ramp improvements on Goshen at Rd 76. This improvement will not be necessary as the ultimate widening of Rd 76 is to be deferred.

Response: The curb ramp improvements at the corner of Goshen and Rd 76 have been removed. See Sheet HC.

22. Comment: Drive approach max width per standards is 41-feet. A wider proposed driveway will require a variance by City Engineer. Refer to further comments from Traffic Safety.

The driveway widths were set as a function of truck turning movements. The driveways connect to the private street. A modified City standard driveway is proposed for the ingress and egress to the site. See Sheet HC. Comment: Development may impact private road to Plaza Dr intersection, requiring signalization. Further analysis will need to be conducted, refer to Traffic Safety Dept. comments.

Response: Acknowledged.

23. Comment: Development may impact private road to Plaza Dr intersection, requiring signalization. Further analysis will need to be conducted, refer to Traffic Safety Dept. comments.

Response: Acknowledged.

24. Comment: Building permits are required, standard plan check and inspection fees apply.

Response: Acknowledged.

BUILDING/SITE PLAN REVIEW COMMENTS:

1. Comment: A building permit will be required. For Information call (559) 713-4444

Response: Acknowledged.

2. Comment: Submit 1 digital set of professionally prepared plans and 1 set of calculations. (Small Tenant improvements)

Response: Acknowledged.

Comment: Meet State and Federal requirements for accessibility for persons with disabilities.

Response: The site complies to State and Federal requirements for accessibility.

4. Comment: School Development fees. Commercial \$0.66 per square foot & Self-storage \$.23 per sf. Residential

Response: Acknowledged.

Comment: Additional comments – Building to be fully sprinklered with type 13 system. Provide smoke and heat ventilation. Provide restrooms with 500ft maximum travel distance for



employees. Provide accessible route to all trash enclosures. Provide future EV charging parking. Provide exterior area for assisted rescue for all elevated exits served by stairs. Landscaping shall meet the MWELO requirements. Provide MDS sheets for Product storage. (Val Garcia 04/20/22)

Response: Acknowledged.

TRAFFIC DIVISION/SITE PLAN REVIEW COMMENTS:

Comment: Install Street Light(s) per City Standards.

Response: Street lights are proposed on the Private Street and on Road 76. See HC.

7. Comment: Install Stop Signs at driveway exit Locations.

Response: Stop signs and stop bars have been added to each driveway exits. See Sheet HC.

8. Comment: Construct parking per City Standards PK-1 through PK-4.

Response: Parking complies with City standard details.

9. Comment: Construct drive approach per City Standards.

Response: The driveway widths were set as a function of truck turning movements. The driveways connect to a private street. A modified City standard driveway is proposed for the ingress and egress to the site. See Sheet HC.

- 10. Comment: Additional traffic information required (Non Discretionary)
 - [X] Trip Generation Provide documentation as to concurrence with General Plan.
 - [X] Site Specific Evaluate access points and provide documentation of conformance with COV standards. If noncomplying, provide explanation.
 - [X] Traffic Impact Fee (TIF) Program Identify improvements needed in concurrence with TIF.

Response: Per coordination call with Leslie Blair on 4/6, Kimley-Horn will provide a Traffic Memo addressing these items.

ADDITIONAL COMMENTS

• Comment: All four intersections require traffic analysis -Plaza at Ferguson and at Goshen; Road 76/American at Ferguson and at Goshen.

Response: Traffic study prepared to address.

Comment: Full median opening for driveway off of Plaza. Analysis required for signalization.

Response: Per coordination call with Leslie Blair on 4/6, Kimley-Horn will provide a Traffic Memo addressing this item.

Comment: Provide site circulation analysis. Note -Driveway off of private road at westerly end
may be too close to intersection when private road is connected to American. Include in analysis.

Response: The connection of the Private Drive to Rd. 76 has been eliminated. In addition, the westerly driveway into the project site has been relocated to sit roughly 200' away from the location of any potential future connection to Rd 76. See Sheet HC.



 Comment: Evaluate site access points. Include future private road access connection to Road 76/American.

Response: Traffic study prepared to address.

 Comment: Note - Non-conforming driveways from City standards require city review and approval. Request shall be in the form of a written letter stating request, explanation for why deviation is needed, and all documentation to support deviation.

Response: The driveway widths were set as a function of truck turning movements. The driveways connect to a private street, and so a modified City standard driveway is proposed for the ingress and egress to the site. See Sheet HC-1.

SOLID WASTE DIVISION/SITE PLAN REVIEW COMMENTS:

1. Comment: Customer responsible for all cardboard and other bulky recyclables to be broken down before disposing of in recycle containers

Response: Acknowledged.

2. Comment: ALL refuse enclosures must be R-3 0R R-4

Response: City Standard R-3 enclosures are called out on Sheet HC.

Comment: Customer must provide combination of keys for access to locked gates/bins.

Response: Acknowledged.

4. Comment: Paved areas should be engineered to withstand a 55,000 lb. refuse truck.

Response: The pavement section was designed to meet this criteria.

5. Comment: Bin enclosure gates are required

Response: Acknowledged. City Standard R-3 enclosures are called out on Sheet HC.

6. Comment: Bin enclosures are for city refuse containers only. Grease drums or any other items are not allowed to be stored inside bin enclosures.

Response: Acknowledged.

7. Comment: Area in front of refuse enclosure must be marked off indicating no parking

Response: Area in front of refuse enclosures have "NO PARKING" lettering. See Sheet HC.

8. Comment: Enclosure will have to be designed and located for a STAB service (DIRECT ACCESS) with no less than 38' clear space in front of the bin, included the front concrete pad.

Response: Required clear space is provided in front of the refuse enclosures, which has been placed per coordination with Nathan Garza. See locations on Sheet HC.

9. Comment: Must be a concrete slab in front of enclosure as per city standards, the width of the enclosure by ten (10) feet. minimum of six (6) inches in depth.

Response: A concrete slab is shown in front of all four enclosures. See location on Sheet HC. The concrete pavement section is shown in the Legend on Sheet CG-1 and CG-2.



10. Comment: City ordinance 8.28.120-130 (effective 07I19I18) requires contractor to contract with City for removal of construction debris unless transported in equipment owned by contractor or unless contracting with a franchise permittee for removal of debris utilizing roll-off boxes.

The proposed city standard (R3/R4) double enclosures looks good for STAB load collection services. Enclosure gates are required, must open 180 degrees, and clearing all curbing Customer to avoid enclosure gates from swinging out into parking stall on the east side of enclosure Cane bolts are to be included to secure gates when opened. The customer is encouraged to contact Solid Waste at 559-713· 4532 to schedule a waste assessment when ready to have bins assigned

Response: Acknowledged.

Sincerely,

Davie Cowan, P.E.

Eugene D. ConowIII

Project Manager

7' TALL BLACK PVC COATED CHAIN LINK FENCE

EX EDGE OF -

PAVEMENT

EX ROAD CL

49' DEFERRED 1/2 ST. IMPROVEMENT

42' R/W DEDICATION

PR. R/W -

GUTTER

0

PARCEL 2: (PORTION OF APN 077-111-047 AND APN 077-111-046)

BEING A PORTION OF THE NORTH HALF AND SOUTH HALF OF THE SOUTHWEST QUARTER OF SECTION 20, TOWNSHIP 18 SOUTH, RANGE 24 EAST, MOUNT DIABLO BASE AND MERIDIAN, IN THE CITY OF VISALIA, COUNTY OF TULARE, STATE OF CALIFORNIA, ACCORDING TO THE OFFICIAL PLAT THEREOF, TOGETHER WITH A PORTION OF THE REMAINDER OF PARCEL MAP NO. 4516, AS PER MAP RECORDED IN BOOK 46, PAGE 21 OF PARCEL MAPS, TULARE COUNTY RECORDS, SAID PORTION BEING DESCRIBED AS FOLLOWS: BEGINNING AT THE NORTHWEST CORNER OF PARCEL 1 OF PARCEL MAP NO. 4516, AS PER MAP

RECORDED IN BOOK 46, PAGE 21 OF PARCEL MAPS, TULARE COUNTY RECORDS. THENCE ALONG THE NORTHERLY LINE OF SAID PARCEL 1 NORTH 89°59'02"EAST 403.01 FEET TO A POINT ON THE WESTERLY LINE OF THE REMAINDER OF SAID PARCEL MAP;

THENCE ALONG SAID WESTERLY LINE SOUTH 00°01'13"EAST 10.02 FEET TO THE SOUTHWEST CORNER OF SAID REMAINDER, SAID CORNER BEING THE BEGINNING OF A NON-TANGENT CURVE, CONCAVE SOUTHERLY, AND HAVING A RADIUS OF 970.00 FEET, A RADIAL LINE TO SAID CURVE THAT BEARS NORTH 00°01'13" WEST;

THENCE ALONG THE SOUTHERLY LINE OF SAID REMAINDER THE FOLLOWING FIVE (5) COURSES:

9.3' 25' 19' 19' 25' 19' 19' 26' 19'

EASTERLY ALONG THE ARC OF SAID CURVE THROUGH A CENTRAL ANGLE OF 17°05'30", AN ARC DISTANCE OF 289.36 FEET TO THE BEGINNING OF A REVERSE CURVE, CONCAVE NORTHERLY, AND HAVING A RADIUS OF 1030.00 FEET, A RADIAL LINE TO SAID CURVE THAT BEARS NORTH

THENCE EASTERLY ALONG THE ARC OF SAID CURVE THROUGH A CENTRAL ANGLE OF 16°37'43", AN ARC DISTANCE OF 298.93 FEET;

3. THENCE TANGENT TO SAID CURVE SOUTH 89°33'26" EAST 33.60 FEET;

THENCE SOUTH 44°53'42" EAST 35.53 FEET;

THENCE NORTH 89°56'52" EAST 2.81 FEET (2.91 FEET PER SAID PARCEL MAP NO. 4516) TO THE SOUTHEAST CORNER OF SAID REMAINDER, SAID CORNER BEING A POINT ON THE WESTERLY RIGHT-OF-WAY OF PLAZA DRIVE (ROAD 80), BEING A 55.00-FOOT-WIDE HALF-STREET, AS SHOWN ON SAID PARCEL MAP;

THENCE ALONG THE EASTERLY LINE OF SAID REMAINDER AND SAID WESTERLY RIGHT-OF-WAY LINE NORTH 00°01'20" WEST 135.19 FEET;

THENCE LEAVING SAID EASTERLY LINE AND SAID WESTERLY RIGHT-OF-WAY LINE SOUTH 89°58'40" WEST

THENCE SOUTH 40°40'51" WEST 52.65 FEET;

GATE WITH KNOX BOX LOCK

- R3 TRASH ENCLOSURE WITH

"NO PARKING" LETTERING

GATE WITH KNOX BOX LOCK

SEWER LIFT STATION

─ BIKE LOCKER AREA

ADA STALLS (TYP)

- EV READY STALLS

- BIKE RACKS

R3 TRASH ENCLOSURE WITH

"NO PARKING" LETTERING

THENCE NORTH 89°33'26", WEST 109.58 FEET TO THE BEGINNING OF A TANGENT CURVE, CONCAVE NORTHEASTERLY, AND HAVING A RADIUS OF 590.00 FEET; THENCE WESTERLY ALONG THE ARC OF SAID CURVE THROUGH A CENTRAL ANGLE OF 16°37'43", AN ARC DISTANCE OF 171.23 FEET; THENCE TANGENT TO SAID CURVE NORTH 72°55'44" WEST 20.59 FEET TO THE BEGINNING OF A NON-TANGENT CURVE. CONCAVE SOUTHERLY, AND HAVING A RADIUS OF 1030.00 FEET, A RADIAL LINE TO SAID POINT THAT

BEARS NORTH 17°04'17" EAST. SAID CURVE BENG CONCENTRIC WITH AND DISTANT 60.00 FEET NORTHERLY FROM THAT CERTAIN COURSE ON THE SOUTHERLY LINE OF SAID REMAINDER, SAID COURSE THENCE LEAVING SAID WESTERLY LINE AND ALONG SAID PARALLEL LINE SOUTH 89°34'26" EAST 95.00 BEING A CURVE, CONCAVE SOUTHWESTERLY, AND HAVING A RADIUS OF 970.00 FEET; THENCE WESTERLY ALONG THE ARC OF SAID CURVE THROUGH A CENTRAL ANGLE OF 17°05'30", AN ARC DISTANCE OF 307.26 FEET TO A POINT OF NON-TANGENCY WITH A LINE, SAID LINE BEING PARALLEL WITH SAID DEED, SAID CORNER ALSO BEING ON THER NORTHERLY RIGHT-OF-WAY LINE OF SAID UNION PACIFIC AND DISTANT 49.98 FEET NORTHERLY FROM THAT CERTAIN COURSE ON THE NORTHERLY LINE OF PARCEL 1 OF SAID PARCEL MAP, SAID COURSE HAVING A BEARING AND DISTANCE OF "NORTH 89°58'02"

EAST 403.01 FEET" (NORTH 89°42'24" EAST 403.00 FEET PER SAID PARCEL MAP); THENCE ALONG SAID PARALLEL LINE SOUTH 89°58'02" WEST 403.06 FEET;

THENCE SOUTH 89°53'12" WEST 1327.30 FEET;

- 6.0' SIDEWALK

PRIVATE ACCESS

ROAD (SHARED)

535,540. FT

W. GOSHEN AVE.

THENCE NORTH 76°29'04" WEST 217.17 FEET TO A POINT ON THE WESTERLY LINE OF THE SOUTHWEST QUARTER OF SAID SECTION 20, SAID POINT BEING DISTANT SOUTHERLY ALONG SAID WESTERLY LINE, 1300.74 FEET FROM THE NORTHWEST CORNER OF SAID SOUTHWEST QUARTER;

- PUBLIC ACCESS EASEMENT

7' TALL BLACK PVC COATED CHAIN LINK FENCE

GATE WITH KNOX BOX LOCK -

BIKE LOCKER AREA -

EV READY STALLS -

R3 TRASH ENCLOSURE WITH -

GATE WITH KNOX BOX LOCK -

CHAIN LINK FENCE

"NO PARKING" LETTERING

R3 TRASH ENCLOSURE WITH-

"NO PARKING" LETTERING

THENCE ALONG WESTERLY LINE SOUTH 00°00'57" WEST 1040.83 FEET TO THE NORTHWEST CORNER OF THAT CERTAIN PORTION OF LAND CONVEYED TO THE CITY OF VISALIA, BY DEED RECORDED DECEMBER 3, 1970, IN BOOK 2925, PAGE 787, OFFICIAL RECORDS OF SAID COUNT, SAID POINT BEING ON A LINE, PARALLEL WITH AND DISTANT 75.00 FEET NORTHERLY FROM THE NORTHERLY RIGHT-OF-WAY LINE OF THE UNION PACIFIC RAILROAD, AS PER SAID DEED;

FEET TO THE NORTHEAST CORNER OF SAID DEED; THENCE ALONG THE EASTERLY LINE OF SAID FEED. PARALLEL WITH SAID WESTERLY LINE, SOUTH 00°00'57" WEST 75.00 FEET TO THE SOUTHEAST CORNER OF

THENCE ALONG SAID NORTHERLY RIGHT OF WAY LINE SOUTH 89°34'26" EAST 1444.35 FEET TO THE SOUTHWEST CORNER OF PARCEL 2 OF PARCEL MAP NO. 4441 AS PER MAP RECORDED IN BOOK 45, PAGE 46 OF PARCEL MAPS, TULARE COUNTY RECORDS;

THENCE LEAVING SAID NORTHERLY RIGHT-OF-WAY LINE AND ALONG THE WESTERLY LINES OF SAID PARCEL 2 AND PARCEL 1 OF SAID PARCEL MAP NO. 4516 AND SAID PARCEL MAP NO. 4441 NORTH 00°01'37" WEST 1029.17 FEET TO THE POINT OF BEGINNING.

ADA CURB RAMP

(IF REQ'D)

| ADDDECC | \A/ EED 0: | IOON A NODE: | DI 474 DD | | |
|--------------------------------------|--------------|---------------------------------------|-------------|--|--|
| ADDRESS (ADA) | W. FERGU | | PLAZA DR. | | |
| ASSESSOR'S PARCEL NUMBER (APN) | | 077-111-047 | | | |
| NUMBER OF EXISTING LOTS | | | 1 | | |
| NUMBER OF PROPOSED LOTS | | | 1 | | |
| PARCEL SUMMARY | | | | | |
| PARCEL 2 | | 1,709,730 | 39.3 | | |
| TOTAL AREA | | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 39.3 | | |
| ZONING INF | ORMATION | | | | |
| ZONING DISTRICT | PLANNED | DEVELOPMENT | DISTRICT | | |
| GENERAL PLAN DESIGNATION | | INDUSTRIAL | | | |
| STATE RESPONSIBILITY AREA? | NO - LOCA | AL RESPONSIBI | LITY AREA | | |
| | REQUIRED | PROV | <u>IDED</u> | | |
| MAX. BUILDING HEIGHT (17.22.060) | 75FT | 55 | FT | | |
| BUILDING SETBACK (17.22.060) | | | | | |
| FRONT | 25FT | 190 |)FT | | |
| SIDE | 0FT | 205 | 5FT | | |
| REAR | | | | | |
| PAR | KING | | | | |
| AUTO STALLS (9' X 19') | | 470 | | | |
| ADA STALLS (9' X 19') | | 24 | | | |
| TOTAL EV READY STALLS (10% OF TOTAL) | | 55 | | | |
| TOTAL AUTO STALLS | | 549 | | | |
| BICYLE PARKING (5% OF TOTAL PARKING) | | 27 | | | |
| TRAILER STALLS | | 142 | | | |
| PROPOSED SITE A | REA DISTRIBL | JTION | | | |
| AREA | SF | | | | |
| BUILDING AREA | 535,540 | 12.3 | 31.3% | | |
| LANDSCAPE AREA | 256,768 | 5.9 | 15.0% | | |
| PAVED AREA | 644,760 | 14.8 | 37.7% | | |
| BASIN AREA | 70,389 | 1.6 | 4.1% | | |
| PRIVATE ROAD | 158,763 | 3.6 | 9.3% | | |
| ROAD DEDICATION | 43,510 | 1.0 | 2.5% | | |
| TOTAL AREA | 1,709,730 | 39.3 100% | | | |

SITE INFORMATION

| LEGEND PROPERTY BOUNDARY | |
|-----------------------------|-------|
| RIGHT-OF-WAY | |
| CENTERLINE | |
| SETBACK | |
| EASEMENT | |
| FENCE | XXXXX |
| BUILDING OUTLINE | |
| ADA PATH OF TRAVEL | |
| ASPHALT PAVEMENT - LIGHT | |
| ASPHALT PAVEMENT - HEAVY | |
| CONCRETE PAVEMENT | A |
| CONCRETE PAVEMENT - HEAVY | |
| CONCRETE SIDEWALK | |
| BMP AREA | |

BENCHMARK

- PROPERTY

- PROPERTY

NATIONAL GEODETIC SURVEY BENCHMARK PID "GT2145" DESIGNATION: CGS BENCHMARK DISK STAMPED "G 827 RESET 1992" ELEVATION: 291.47' DATUM: NAVD 88

DESCRIBED AS: 1.7 MILES EAST ALONG THE SOUTHERN PACIFIC COMPANY RAILROAD FROM GOSHEN JUNCTION STATION IN GOSHEN, IN TOWNSHIP 18 SOUTH, RANGE 24

ELEVATIONS WITHIN THIS PLAN SET ARE BASED ON THE USGS NAVD 88 DATUM. TO CONVERT ELEVATIONS TO THE USGS NGVD 29 DATUM, THE FOLLOWING CONVERSION NGVD 29 DATUM ELEVATION = NAVD 88 DATUM ELEVATION - 1.77'.

OWNER/DEVELOPER:

2201 E CAMELBACK ROAD, SUITE 222 PHOENIX, AZ 85016 **CONTACT: BRYAN FRAREY** PH: 602-337-8730

CIVIL ENGINEER:

BFRAREY@SEEFRIEDPROPERTIES.COM

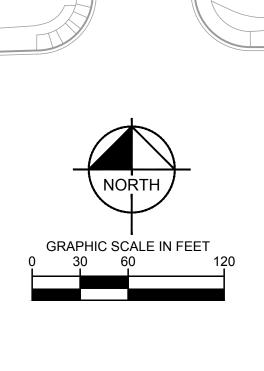
KIMLEY-HORN AND ASSOCIATES, INC. 3880 LEMON STREET, SUITE 420 RIVERSIDE, CA 92101 PH: 619.744.0144 CONTACT: DAVIE COWAN, P.E.

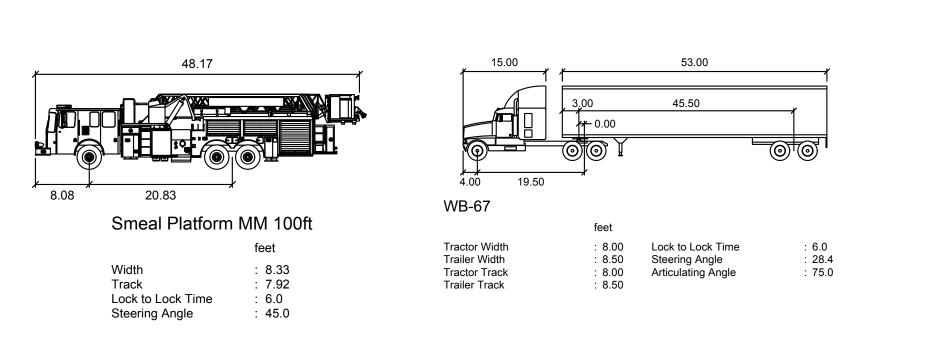
ARCHITECT

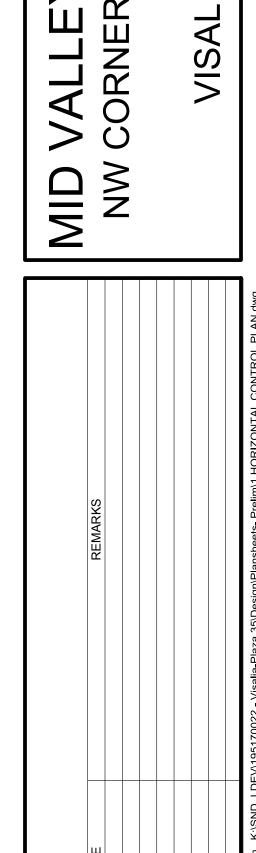
KODY ZEDOLEK 2199 INNERBELT BUSINESS CENTER DR ST. LOUIS, MO 63114 CONTACT: 314.592.2212 PH: 618.494.8680

ADRESS:

EAST OF ROAD 76 AND NORTH OF GOSHEN AVENUE VISALIA, CA 93291







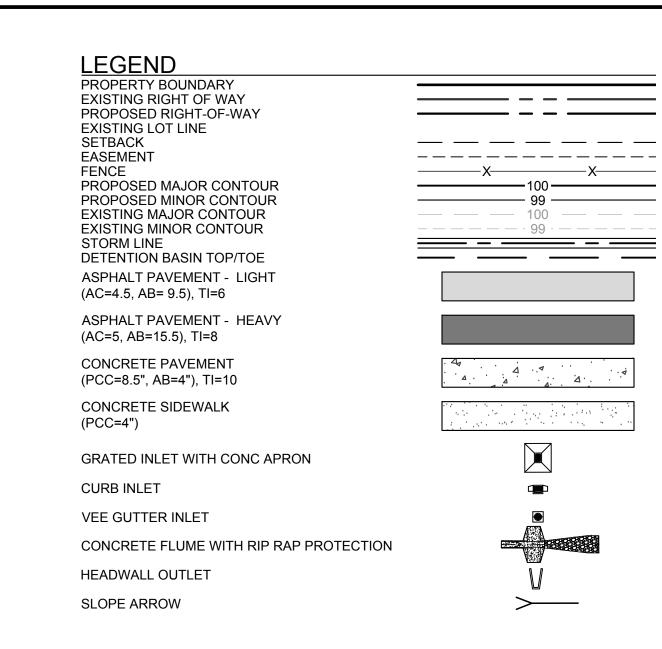
DESIGNER:

HC

PRELIMINARY

Kimley» Horn

Engineer EUGENE D. COWAN III P.E. No. 86803 Date 05/19/22



| EARTHWORK | < | | | |
|--|-------------|------|----------|--|
| LOT SIZE (ACRES) | 39.25 | | | |
| RAW CAD EARTHV | VORK | | | |
| CUT (CU. YD.) | | 77 | 7,424 | |
| FILL (CU. YD.) | | 58 | 3,781 | |
| CUT FACTOR | 1 | | | |
| FILL FACTOR | 1 | | | |
| NET (CU. YD.) | | 18,6 | 643.4 | |
| ADDITIONAL EARTH | IWORK | | | |
| ITEM | QNTY | UNTS | CU. YD. | |
| Building Slab | 535,540 | SF | 10.925 | |
| BUILDING SLAB DEPTH | 12.0 | IN | 19,835 | |
| Light Duty Asphalt (AC =4.5, AB = 9.5), TI=6 | 159,986.0 | SF | - 6,913 | |
| Section | 14.0 | IN | 0,913 | |
| Heavy Duty Asphalt (AC = 5, AB = 15.5), TI=8 | 324,715.0 | SF | 20,545 | |
| Section | 20.5 | IN | | |
| Concrete Parking Areas and Drive Aisles (PCC = 8.5", AB = 4"), TI=10 | 138,264.0 | SF | 5,334 | |
| Section | 12.5 | IN | 3,334 | |
| Sidewalk (PCC = 4") | 7,051.5 | SF | 87 | |
| Section | 4.0 | IN | 07 | |
| Utility Spoils (FW, SS, SD & W) | | CY | - | |
| ADDITIONAL CUT SUM (CU. YD.) | | | 52,714 | |
| SHRINKAGE FACTOR | | | 0.20 | |
| SHRINKAGE VOLUME (RAW FILL x 20%) | | | 11,756 | |
| SHRINKAGE VOLUME - BUILDING PAD | | | 47,604 | |
| SUBSURFACE STORAGE VOLUME | | I | 16,379 | |
| ESTIMATED EARTHWOR | K DESHITS | | | |
| LOT SIZE (ACRES) | | | 39.25 | |
| CUT (CU. YD.) | | | 146,518 | |
| FILL (CU. YD.) | | | 118,141 | |
| FILL (CO. TD.) | | | 118.1411 | |

DACINI CALCUL ATIONIC

BASIN STORAGE AVAILABLE = 12,690 CF(BASIN 1) + 11,691 CF(BASIN 2) + 56,673 CF(BASIN 3) = <math>81,054 CFTOTAL STORAGE NEEDED (SEE CITY STD. D-36): 4.17IN * 1FT/12IN * 39.25AC * 43,560SF/AC = 594,130 CFSUBSURFACE STORAGE NEEDED = 594,130 CF - 81,054 CF = 513,076 CF

BASIN CALCULATIONS

MAX. WATER SURFACE ELEVATION (BASIN 1 AND BASIN 2) = 285.6

MAX. WATER SURFACE ELEVATION (BASIN 3) = 288.0

BASIN STORAGE AVAILABLE = 12.690 CF(BASIN 1) + 11.691 CF(B

GRAPHIC SCALE IN FEE

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401 B STREET, SUITE 600; SAN DIEGO, CA 92101

FOR REVIEW ONLY
Prepared for Concept Plan submittal
Not for construction purposes or permits.

Kimley» Horn

Engineer EUGENE D. COWAN III
P.E. No. 86803

Date 05/19/22

MID VALLEY LOGISTICS CENNW CORNER OF GOSHEN AVE & RI

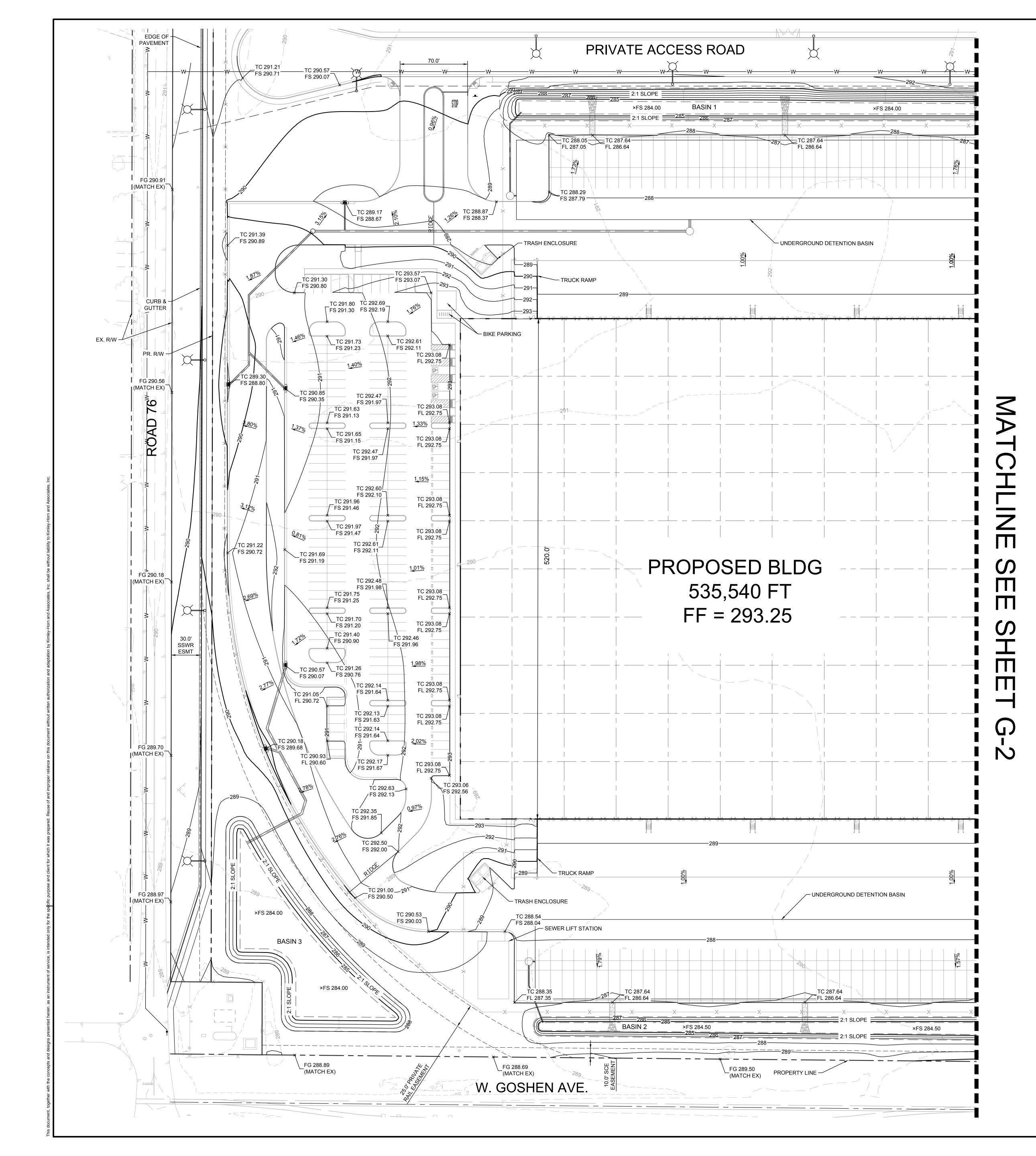
| REMARKS | | | | |
|---------|--|--|--|--|
| DATE | | | | |

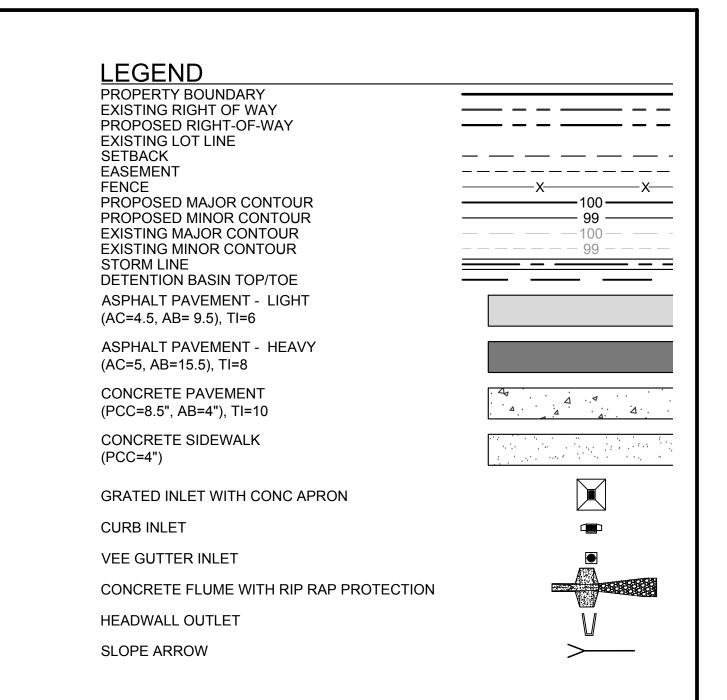
PM: EDC/KPS

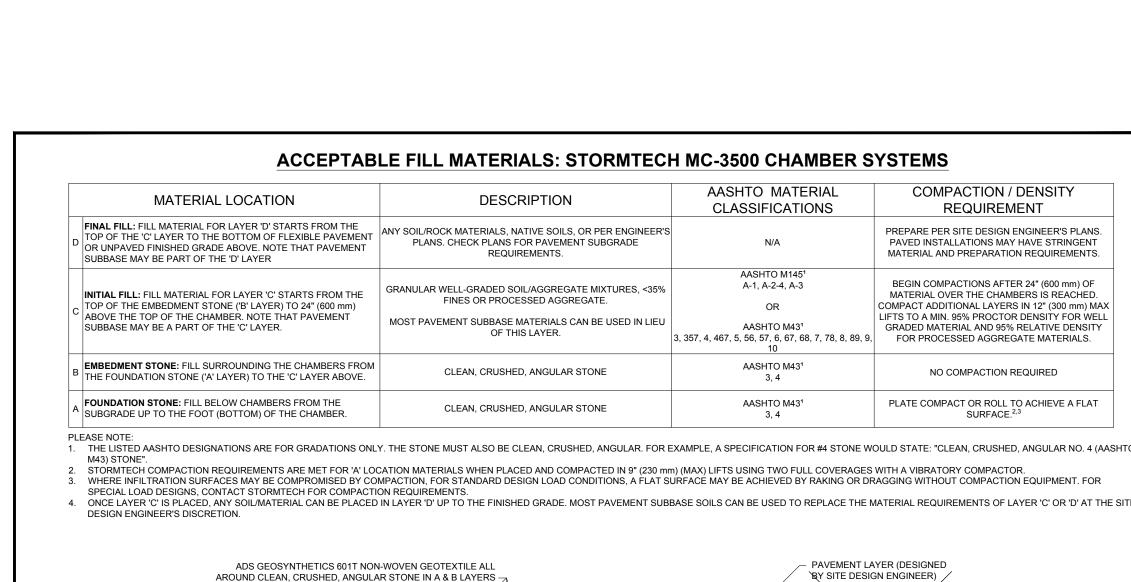
DESIGNER: TB

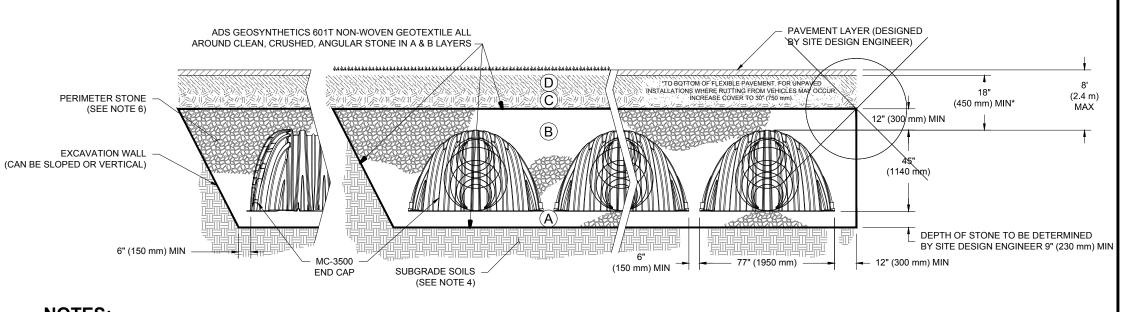
JOB NO.: 195170013

G-1









FS 294.57

FS 292.36

TC 293.20

FS 292.70

FS 291.50

TC 292.25

FS 291.75

TC 293.10

 $_{\rm Z}$ TC 293.33

∠TC 293.10

⊈FL 292.77

FL 293.00

_TC 293.11

TC 293.39 FL 293.06

FS 292.52

TC 289.85 _ _ FS 289.35 _

TC 289.42 TC 290.19_/ _TC 290.25

TC 290.81_/

FS 290.31 FS 290.37

_TC 290.87

TRASH ENCLOSURE -

TRUCK RAMP -

FS 288.56

FS 287.73

TC 287.64 TC 288.13 FS 289.27

ーFS 287.77

TC 289.86_/

FS 289.36

FS 289.42

TC 293.10 TC 292.12

FL 292.77 FS 291.62

TC 293.09 TC 292.38 FL 292.76 FS 291.88

TC 293.10 TC 292.46

√/FL 293.00

FS 291.43

TC 291.67

FS 290.70

FS 291.04

FS 291.52

TC 292.11 TC 291.51

FS 291.87 FS 291.49 →

TC 292.48 TC 292.21

TC 292.18

FS 291.68

FS 291.72 FS 291.23

TC 292.18 FS 291.68

TC 291.87

FS 291.37

TC 291.93

^{_}FS 291.98 FS 291.71

FS 291.61, FS 291.01

TC 289.95

−FL 290.08 FS 292.89

FS 292.94

FS 290.87

TC 291.67_

\FS 291.17 /

TC 291.70

FS 291.20

FS 291.65

FS 291.68

FL 291.37-

FL 292.04

TC 292.37

FS 291.87

TC 292.34

FS 291.84

TC 291.89

FS 291.39

TC 291.86

FS 291.36

FS 290.95

TC 291.42 FS 290.92

TC 292.89 FS 292.39

TC 291.45 🔔

FS 290.95

FS 292.72

FS 289.45

FG 294.03

FG 293.96

FG 293.97

(MATCH EX)

FG 294.07

(MATCH EX)

(MATCH EX)

PROPERTY LINE

- PROPERTY

T(MATCH EX)

(MATCH EX)

PROPERTY LINE

PRIVATE ACCESS ROAD

FL 286.64

FL 286.64

PROPOSED BLDG

535,540 FT FF = 293.25

/ UNDERGROUND DETENTION BASIN

= 2:1 SLOPE

- UNDERGROUND DETENTION BASIN

BASIN 1

TRUCK RAMP -

TC 287.64

FL 286.64

TC 288.49 FS 287.99

TC 288.43

FS 287.93

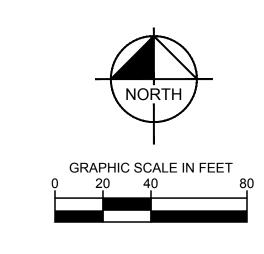
TRASH ENCLOSURE — FS 289.26

TC 289.76

BIKE PARKING -

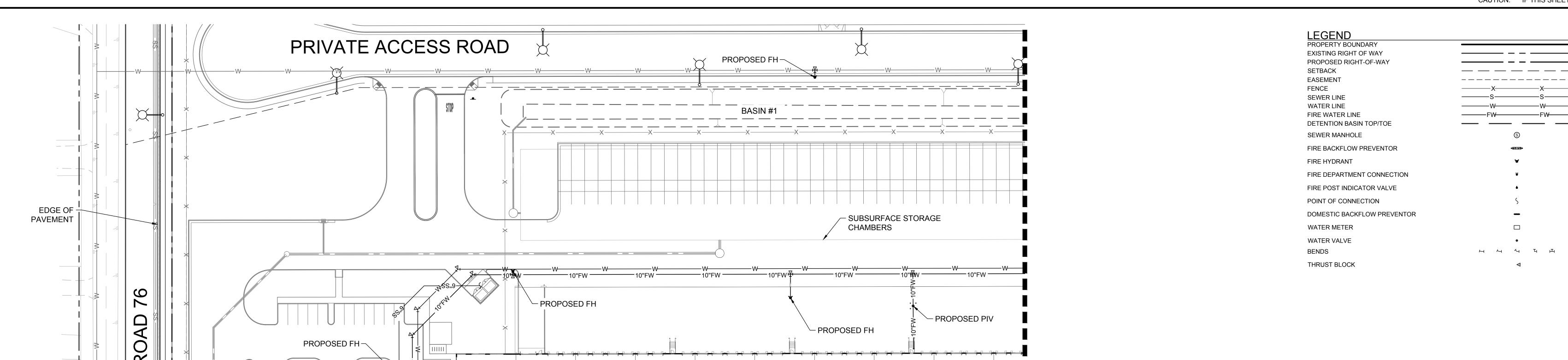
- 2. MC-3500 CHAMBERS SHALL BE DESIGNED IN ACCORDANCE WITH ASTM F2787 "STANDARD PRACTICE FOR STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".
- TO ENSURE A SECURE JOINT DURING INSTALLATION AND BACKFILL. THE HEIGHT OF THE CHAMBER JOINT SHALL NOT BE LESS THAN 3'
- TO ENSURE THE INTEGRITY OF THE ARCH SHAPE DURING INSTALLATION, a) THE ARCH STIFFNESS CONSTANT AS DEFINED IN SECTION 6.2.8 OF ASTM F2418 SHALL BE GREATER THAN OR EQUAL TO 500 LBS/IN/IN.

UNDERGROUND DETENTION BASIN: ADS STORMTECH MC-3500 CHAMBER SYSTEM



PRELIMINARY FOR REVIEW ONLY
Prepared for Concept Plan submittal
Not for construction purposes or permits. Kimley»Horn ngineer EUGENE D. COWAN III P.E. No. 86803 Date 05/19/22

DESIGNER:



PROPOSED BLDG

- PROPOSED FH

W. GOSHEN AVE.

← PROPOSED PIV

- SUBSURFACE STORAGE

293.25 FF

EX. R/W -

PR. R/W -

SSWR ESMT

PROPOSED FH-

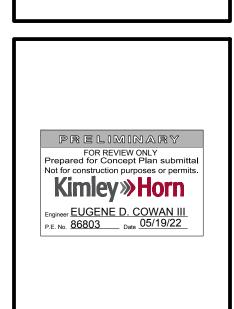
BASIN #3

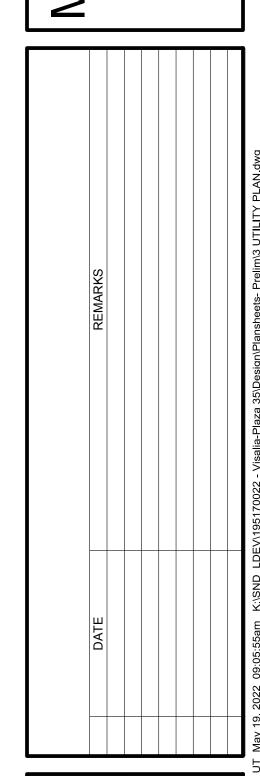
PROPOSED FH-

PROP. OFFSITE WATER -

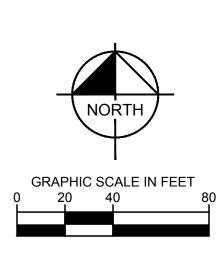
EXIST. SEWER TRUNK LINE

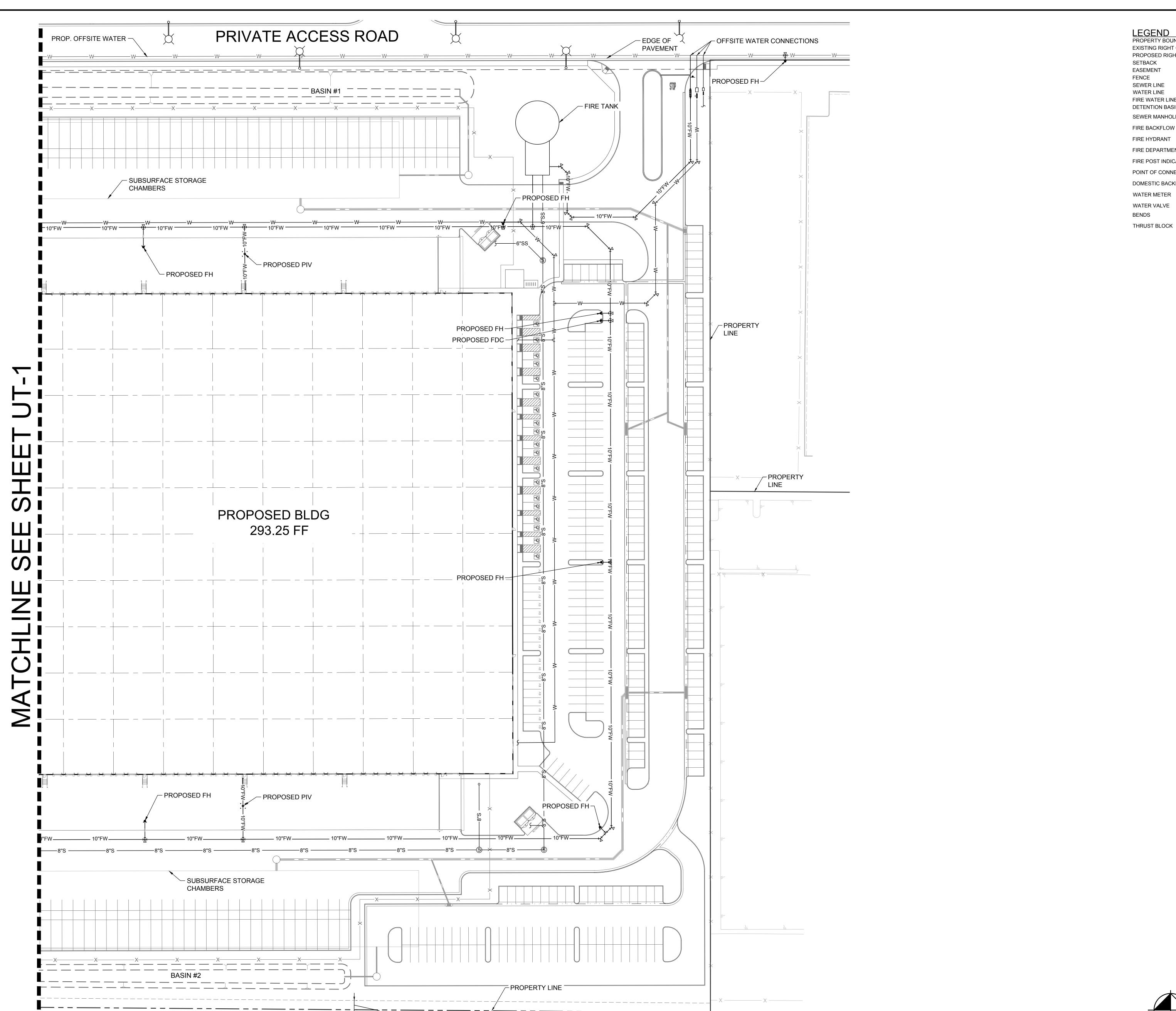
SEWER CONNECTION POINT -





DESIGNER: TB





W. GOSHEN AVE.

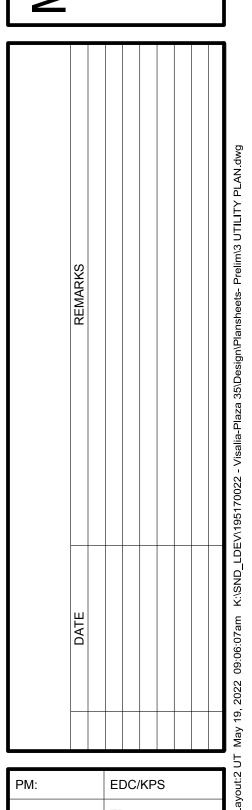
LEGEND PROPERTY BOUNDARY EXISTING RIGHT OF WAY PROPOSED RIGHT-OF-WAY SETBACK EASEMENT SEWER LINE WATER LINE FIRE WATER LINE DETENTION BASIN TOP/TOE SEWER MANHOLE FIRE BACKFLOW PREVENTOR FIRE HYDRANT FIRE DEPARTMENT CONNECTION FIRE POST INDICATOR VALVE POINT OF CONNECTION DOMESTIC BACKFLOW PREVENTOR WATER METER WATER VALVE H 4 4 4 H

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WWWW KIMI FY-HORN COM



MID VALLEY LOGISTICS CENT

NW CORNER OF GOSHEN AVE & RD



PM: EDC/KPS

DESIGNER: TB

JOB NO.: 195170013

UT-2

TRAFFIC ANALYSIS

Plaza 39 Industrial Development

PREPARED FOR:

SEEFRIED DEVELOPMENT PROPERTIES, INC.



MAY 2022 | DRAFT

Prepared By:



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- F CA MUTCD TRAFFIC SIGNAL WARRANTS
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EXECUTIVE SUMMARY

The following Traffic Analysis ("TA") has been prepared to determine potential Level of Service (LOS) deficiencies associated with the Plaza 39 Industrial Development ("Project"), an approximately 536,000-SF industrial building located within the City of Visalia ("City"), just east of the Tulare County ("County") border. The site is located on an undeveloped 39.25-acre site at 2045 N Plaza Drive, approximately 1-mile east of State Route 99 (SR 99), and is classified as Light Industrial Land Use by the City's General Plan. The site is bound by Route 76 to the west, W, Goshen Avenue to the south, existing industrial warehouses to the east and a future Private Access Road to the north. The Project proposes a "speculative" general light industrial development; meaning, a final user and operations for the site is not known at this time. The project proposes two (2) full-access, unsignalized driveways along the south side of the future Private Access Road. The Project is consistent with the City's Light Industrial Land Use designation: light manufacturing, warehousing, storage, distribution, research and development, and secondary office (limited customer access), and a FAR below 0.5 (0.31 proposed). The Project would be developed in one phase with completion expected in 2024.

Based on site plan review comments issued by City staff on March 2, 2022, the Project requires Non-Discretionary approvals, meaning a Traffic Impact Analysis (TIA) is not required, including a CEQA Vehicle Miles Traveled (VMT) analysis. The Project is required to determine the expected trip generation and provide an analysis of the site's access, adjacent intersections, and on-site circulation. This TA provides documentation of the Project's concurrence with the City's General Plan. This TA also addresses the Project's LOS effects in order to assist the City with planning and the identification of conditions of approval, and to mitigate the Project's identified LOS deficiencies, if necessary.

TRIP GENERATION

The Project is expected to generate of 2,744 daily PCE trips, with 403 PCE trips (351 inbound / 51 outbound) during the a.m. peak hour and 354 PCE trips (51 inbound / 303 outbound) during the p.m. peak hour.

PROJECT OPERATIONAL ANALYSIS

The traffic operation analysis shows that the Project would degrade the LOS operations with the addition of the Project's traffic at intersection of N Plaza Drive / Private Access Road. This intersection meets the CA MUTCD 8-hour signal warrant under Opening Year (2024) conditions with the addition of project traffic, and the installation of traffic signals would improve the intersection operations to LOS B or better.

The Project is not expected to cause adverse effects to the turn lanes queuing.

PROJECT IMPROVEMENTS

SITE ACCESS

Access to the Project site would be established through the construction of two (2) full-access unsignalized driveways along the future Private Access Road (under construction by Project Gold Bar). The following summarizes the project access locations:

- Local Access Road & Project Driveway 1
 - Construct a full-access driveway <u>a minimum of 200-feet east of the Road 76 centerline</u> per the City of Visalia standards;
 - Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane; and
 - o Provide one outbound lane (stop-controlled).
- Local Access Road & Project Driveway 2
 - o Construct a full-access driveway per the City of Visalia standards;
 - Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane; and
 - o Provide one outbound lane (stop-controlled).

A sight distance analysis for each Project driveway shows the two (2) proposed access driveways would exceed the 300-foot corner sight distance requirement.

PEDESTRIAN FACILITIES

The Applicant is installing sidewalk and pedestrian ramps along the Local Access Road as part of the Project Goldbar Conditions of Approval. Pedestrian connectivity would also be enhanced by the installation of traffic signal at the N Plaza Drive / Local Access Road intersection.

BICYCLE FACILITIES

The Applicant is installing Class II bike lanes along N Plaza Drive, between W Fergusson Avenue and W Goshen Avenue Project, as part of the Project Gold Bar Conditions of Approval.

OFF-SITE RECOMMENDATIONS

The following intersections improvements are recommended at N Plaza Drive / Private Access Road:

- Provide northbound left-turn pocket (150-foot minimum);
- Provide southbound left-turn pocket (150-foot minimum);
- Provide southbound right-turn lane between the southernmost Project Gold Bar driveway and intersection:
- Provide eastbound left-turn pocket (150-foot minimum);
- Provide eastbound through/right-turn lane;
- Provide westbound left/through/right-turn lane; and
- Install traffic signal (NB/SB Protected LT Phasing & EB/WB Permitted Phasing).

It is recommended that the Applicant modify the street improvement plans for Project Gold Bar for the construction of southbound right-turn pocket.

1. INTRODUCTION

The following Traffic Analysis ("TA") has been prepared to determine potential Level of Service (LOS) deficiencies associated with the Plaza 39 Industrial Development ("Project"), an approximately 536,000-SF industrial building located within the City of Visalia ("City"), just east of the Tulare County ("County") border. The site is located on an undeveloped 39.25-acre site at 2045 N Plaza Drive, approximately 1-mile east of State Route 99 (SR 99), and is classified as Light Industrial Land Use by the City's General Plan. The site is bound by Route 76 to the west, W, Goshen Avenue to the south, existing industrial warehouses to the east and a future Private Access Road to the north. The Project proposes a "speculative" general light industrial development; meaning, a final user and operations for the site is not known at this time. The project proposes two (2) full-access, unsignalized driveways along the south side of the future Private Access Road. The Project is consistent with the City's Light Industrial Land Use designation: light manufacturing, warehousing, storage, distribution, research and development, and secondary office (limited customer access), and a FAR below 0.5 (0.31 proposed). The Project would be developed in one phase with completion expected in 2024. Figure 1 depicts the Project location and study area and Figure 2 shows the proposed site plan.

Based on site plan review comments issued by City staff on March 2, 2022, the Project requires Non-Discretionary approvals, meaning a Traffic Impact Analysis (TIA) is not required, including a CEQA Vehicle Miles Traveled (VMT) analysis. The Project is required to determine the expected trip generation and provide an analysis of the site's access, adjacent intersections, and on-site circulation. This TA provides documentation of the Project's concurrence with the City's General Plan. This TA also addresses the Project's LOS effects in order to assist the City with planning and the identification of conditions of approval, and to mitigate the Project's identified LOS deficiencies, if necessary.

ANALYSIS METHODOLOGY

Study Area

The Project will generate new vehicular trips that will increase traffic volumes on the nearby street network. To assess changes in traffic conditions associated with the proposed project, the intersections in **Table 1** were evaluated. The study intersections and analysis scenarios were determined through coordination with City staff and the Scope of Work submitted to City. **Appendix A** contains the Scope of Work memo. **Figure 1** illustrates the location of each intersection relative to the Project site. The two (2) proposed access driveways would also be evaluated.

Table 1: Study Intersections

| # | Intersection |
|---|---|
| 1 | Road 76 and W Ferguson Avenue (Unsignalized) |
| 2 | Road 76 and W Goshen Avenue (Unsignalized) |
| 3 | N Plaza Drive and W Ferguson Avenue (Signalized) |
| 4 | N Plaza Drive and Private Access Road (Unsignalized); |
| 5 | N Plaza Drive and W Goshen Avenue (Signalized). |

FIGURE 1 - VICINITY MAP

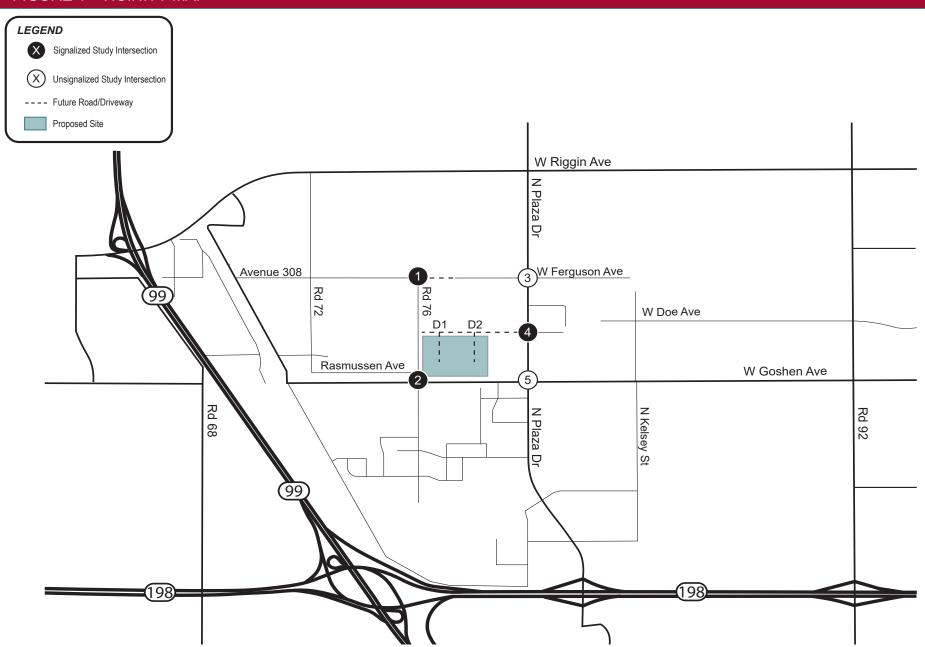
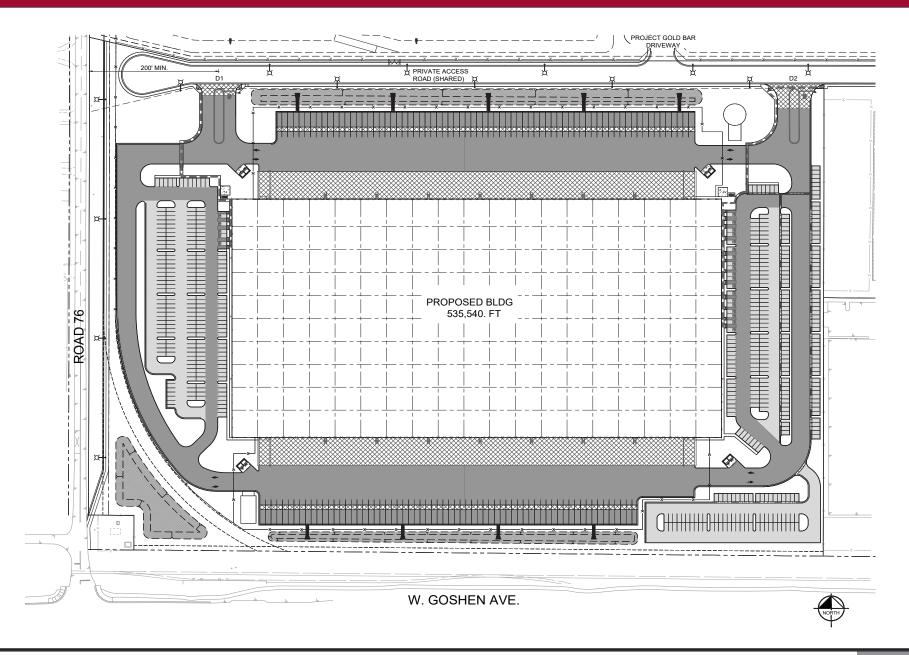


FIGURE 2 - SITE PLAN



Analysis Scenarios

Two (2) scenarios were analyzed as part of the supplemental traffic operations analysis, listed below:

- Opening Year (2024) Baseline Conditions Represents the traffic conditions on the street network assumed in year 2024, the projected opening year of the Project. Existing traffic volume data collected was increased by 1.5% annually (3% total) to account for ambient growth in the vicinity. This scenario does not include Project traffic.
- Opening Year (2024) Baseline Plus Project Conditions Represents the traffic conditions under Opening Year (2024) with the addition of the proposed project traffic and its proposed improvements. Comparison of this scenario to the Opening Year (2024) Baseline Conditions scenario determines whether LOS deficiencies are a direct result of the Project.

Intersection Level of Service

LOS of an intersection is a qualitative measure used to describe operational conditions. LOS ranges from A (best), which represents minimal delay, to F (worst), which represents heavy delay and a facility that is operating at or near its functional capacity. Levels of service for this study were determined using methods defined in the *Highway Capacity Manual*, 6th Edition (HCM 6) within the *Synchro 11* traffic analysis software.

The HCM includes procedures for analyzing side street stop controlled (SSSC), all-way stop controlled (AWSC), and signalized intersections. The SSSC procedure defines LOS as the highest delay of each minor street movements or major street left turns. Conversely, the AWSC and signalized intersection procedures define LOS as a function of average control delay for the entire intersection. **Table 2** relates the operational characteristics associated with each LOS category for signalized and unsignalized intersections.

Table 2: Intersection Level of Service Definitions

| Level of Service | Description | Signalized (Avg. control delay per vehicle sec/veh.) | Unsignalized (Avg. control delay per vehicle sec/veh.) |
|---------------------|---|---|---|
| Α | Free flow with no delays. Users are virtually unaffected by others in the traffic stream | ≤ 10 | ≤ 10 |
| В | Stable traffic. Traffic flows smoothly with few delays. | > 10 – 20 | > 10 – 15 |
| С | Stable flow but the operation of individual users becomes affected by other vehicles. Modest delays. | > 20 – 35 | > 15 – 25 |
| D | Approaching unstable flow. Operation of individual users becomes significantly affected by other vehicles. Delays may be more than one cycle during peak hours. | > 35 – 55 | > 25 – 35 |
| E | Unstable flow with operating conditions at or near the capacity level. Long delays and vehicle queuing. | > 55 – 80 | > 35 – 50 |
| F | Forced or breakdown flow that causes reduced capacity. Stop and go traffic conditions. Excessive long delays and vehicle queuing. | > 80 | > 50 |

Sources: Transportation Research Board, Highway Capacity Manual 2016, National Research Council, 2016.

The following assumptions were included in the analysis:

- Peak-hour factor (PHF) based on the existing traffic data was used for the Opening Year (2024) scenarios.
- Traffic signal timing assumptions based on existing signal phasing and augmented for traffic volumes analyzed.
- Percent of heavy vehicles (PHV) based on a default value of 2%.

Signal Warrants

Traffic signals may be justified when traffic operations fall below acceptable LOS standards and when one or more signal warrants are satisfied. Per the City's *Procedures for Traffic Impact Analysis ("TIA Guidelines")*, traffic volumes at the future Local Access Road intersection were compared against the 8-hour warrant in the 2014 California Manual on Uniform Traffic Control Devices (CA MUTCD)¹. *Traffic Signal Warrant #1 — Eight Hour Vehicular Volume* is satisfied when traffic volumes on the major and minor approaches exceed thresholds for eight hours of the day. This warrant typically applies at locations where a large volume of intersection traffic is the principal reason to consider installing a traffic control signal or when traffic volumes on a major street are so heavy that traffic on the minor street suffers excessive delay or conflict in entering or crossing the major street.

Vehicle Queuing

Queues that exceed the turn pocket length can create potentially hazardous conditions by blocking or disrupting through traffic in adjacent travel lanes. However, these potentially hazardous queues are generally associated with left-turn movements. Locations where the right-turn pocket storage is exceeded are generally not considered hazardous because the right-turn movements generally receive "green indications" at the same time as the adjacent through movement. Therefore, any additional vehicles that spill out of the right-turn pocket will likely not hinder nor disrupt the adjacent through traffic, as would be the case in most left turn pockets.

The effects of vehicle queuing for all exclusive turn-lanes was analyzed by reporting the 95th percentile queues. The 95th percentile queue length represents a condition where 95 percent of the time during the peak hour, traffic queues are expected to be less than or equal to the queue length estimated by the analysis. This is referred to as the "95th percentile queue", which is less than the average queuing. The 95th percentile queue length was determined using HCM 6 methodology via *Synchro 11* Software.

Deficiency Criteria

Project deficiencies were determined by comparing conditions with the proposed project to those without the proposed project.

Level of Service Criteria

As LOS analysis in this study focuses on the peak periods of traffic, LOS D was used as the deficiency threshold. Therefore, a project induced deficiency was assumed if the addition of Project traffic would cause a facility that is operating acceptably (LOS A, B, C, or D) to begin to operate unacceptably (LOS E or F).

¹ California Manual on Uniform Traffic Control Devices, (FHWA's MUTCD 2009 Edition, including Revisions 1 & 2 as amended for use in California), 2014 Edition, Revision 6 (March 30, 2021)

For facilities already operating unacceptably (LOS E or F) without project traffic, any addition of Project traffic resulting in increased delay would result in a Project deficiency.

Vehicle Queueing

Unacceptable or extended queuing may be defined as spill over from turn pockets into through lanes and/or spill over into intersections. This study assumes spill over to mean the estimated 95th percentile queue for a turn pocket exceeds available storage by more than one car length (25 feet). If a turn pocket is anticipated to exceed available storage under no-project conditions, the project would cause constrained access for that movement if it increases the deficient queue by at least one car length (25 feet).

2. EXISTING (2022) CONDITIONS

This chapter describes the existing conditions of the roadway network and traffic volumes within the vicinity of the Project site.

ROADWAY NETWORK

This section provides a description of the specific roadways included in this study.

N PLAZA DRIVE

N Plaza Drive is a four-lane, north-south arterial roadway beginning at Avenue 320 in the north and ending at Airport Drive in the south. The 3.25-mile roadway serves industrial and commercial land uses in the study area. Plaza Drive connects to SR 198. The speed limit ranges from 45 to 55 miles per hour.

W GOSHEN AVENUE

W Goshen Avenue is a four-lane, east-west arterial roadway connecting to Commercial Road in the west and North Divisadero Street in the east. The roadway provides connection from residential communities in east Visalia to industrial land uses near State Route 99. The speed limit on W Goshen Avenue within the study area ranges from 50 to 55 miles per hour.

ROAD 76

Road 76 is a two-lane, north-south collector roadway connecting to Avenue 320 in the north and W Goshen Avenue in the south. The roadway serves industrial and residential land uses in the study area. The speed limit on Road 76 within the study area ranges from 40 to 50 miles per hour.

W FERGUSSON AVENUE

W Fergusson Avenue is a two-lane, east-west collector roadway beginning at Road 76 in the west and ending at Santa Fe St in the east. The roadway serves industrial and residential land uses in the study area. The speed limit on W Ferguson Avenue within the study area ranges from 50 to 45 miles per hour.

The existing intersection lane configuration and traffic controls, as of April 2022, are illustrated in Figure 3.

PEAK-HOUR TURNING MOVEMENT VOLUMES

Intersection turning movement volumes for the study area intersections were collected at five (5) intersections on Thursday, April 21·2021, when local schools were in session. Volumes were collected at the two (2) signalized intersections during the typical 7-9 AM and 4-6 PM commuter peak periods. At the three (3) unsignalized intersections, volumes were collected between 6 AM and 6 PM. The unadjusted Existing (2022) peak hour turning movement volumes are shown in **Figure 4**. Traffic volume data sheets is provided in **Appendix B**.

FIGURE 3 - EXISTING (2022) TRANSPORTATION CONDITIONS

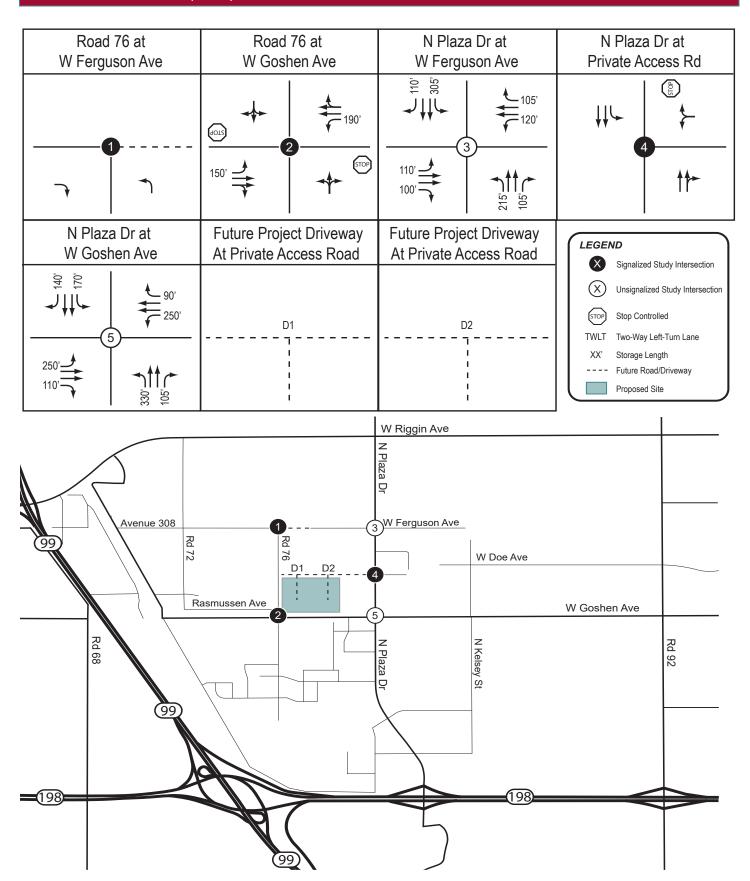
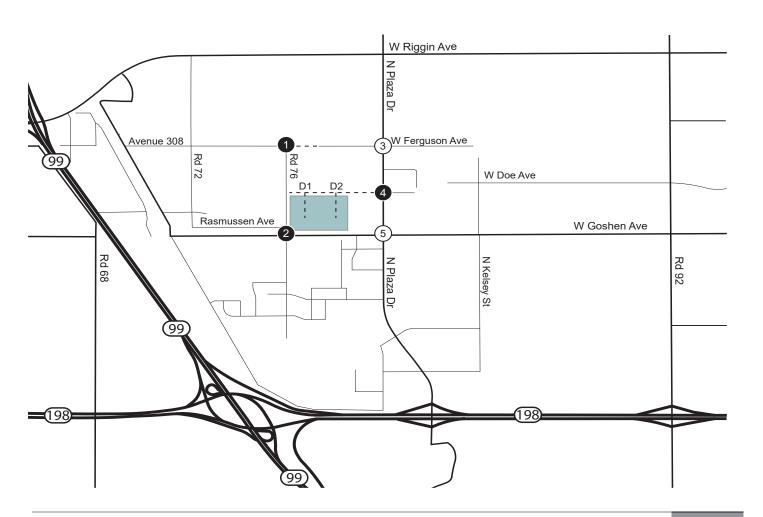


FIGURE 4 - EXISTING (2022) PEAK HOUR TURNING MOVEMENT VOLUMES

| W Ferguson Ave | 5 | 2 0 7 0 0 7 18 / 27 127 Rd 76 Rd 76 | S 88 / 136 ⇔ 153 / 122 ≥ 36 / 22 W Goshen Ave | 3 | S 0/9 2 7/28 W Ferguson Ave | + 594 / 649 | \$ 1/3 2 1/6 Private Access Rd |
|-------------------------|---|-------------------------------------|--|------------------|--|---|--|
| 169 / 98 2 9 | 76 / 149 | 113/215 ⇒ 14/15 № | 8 / 15 6 / 18 18 / 72 | 0/1 ⇒ 24/48 № | 70 / 23 4 475 / 594 57 1 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | | 565 / 610 = 18 / 3 |
| 26 / 70 & 44 8 / 47 3 0 | 180 / 160 / | FUTURE DE | RIVEWAY | FUTURE DR | IVEWAY | Unsignalize Future Roa Proposed S | Study Intersection and Study Intersection and/Driveway Site ak Hour Volume |



3. OPENING YEAR (2024) BASELINE CONDITIONS

This chapter describes the Opening Year (2024) Baseline Conditions of the roadway network and traffic volumes within the vicinity of the Project site, without the Project. This scenario establishes a baseline for determining project-related deficiencies.

ROADWAY NETWORK CHANGES

For the Opening Year (2024) Baseline Conditions, it is assumed that Project Gold Bar (under construction in 2022) would be completed just to the north of the Project. The Project is constructing the following street improvements.

N PLAZA DRIVE

Western portion of N Plaza Drive is being constructed to its ultimate arterial classification to provide two northbound / southbound travel lanes and Class II bike lanes. The improvements will include a raised center median with openings for driveway locations and sidewalk fronting the site.

W FERGUSSON AVENUE

Southern half of W Fergusson Avenue is being constructed to its ultimate collector classification to provide a single eastbound / westbound travel lane, a center two-way left-turn lane, Class II bike lanes and shoulder/parking. The Project would extend the street segment to connect with Road 76, which would become a stop-controlled location. Sidewalk is being constructed along the site frontage.

PRIVATE ACCESS ROAD

The Private Access Road would be constructed and would terminate east of Road 76. The intersection at N Plaza Drive would be full-access stop-controlled.

The assumed Opening Year (2024) Baseline Conditions intersection lane configuration and traffic controls are illustrated in **Figure 5**. **Appendix C** contains the approved signing and striping plans for Project Gold Bar.

TRAFFIC VOLUMES

To account for limited future development and growth within the City, the Existing (2022) Conditions traffic volumes were increased by 1.5 percent annually (3 percent total) to develop the Opening Year (2024) Conditions traffic volumes. The growth rate was determined by the Tulare County Associate of Governments (TCAG) travel demand model. **Appendix B** contains the TCAG Model Plots and growth calculations.

INTERSECTION LEVEL OF SERVICE

Table 3 displays the intersection LOS analysis results under Opening Year (2024) Baseline Conditions, showing all intersections are expected to operate at LOS D or better during the commuter peak periods.

Appendix D contains the intersection LOS calculation worksheets.

OPENING YEAR (2024) BASELINE CONDITIONS PEAK-HOUR INTERSECTION LEVEL OF SERVICE SUMMARY

| | | | | OPENING Y | EAR (2024) | | |
|---|--------------------------------------|-----------------|-----------|------------------|------------|--|--|
| | INTERSECTION | TRAFFIC CONTROL | PEAK HOUR | DELAY (a) | LOS (b) | | |
| 1 | Road 76 & W Ferguson Avenue | Two-Way Stop | AM | 9.8 | А | | |
| ' | Road 70 & W 1 erguson Avenue | Two-vvay Gtop | PM | 9.9 | Α | | |
| 2 | W Goshen Avenue & Road 76 | Two-Way Stop | AM | 17.9 | С | | |
| | W Goshell Avellue & Road 70 | Two-Way Stop | PM | 18.8 | С | | |
| 3 | N Plaza Drive & W Ferguson Ave | Signal | AM | 11.2 | В | | |
| 3 | IN Plaza Dilve & W Felgusoli Ave | Signal | PM | 10.6 | В | | |
| 4 | N Plaza Drive & Private Access Road | Two-Way Stop | AM | 18.5 | С | | |
| | IN Flaza Drive & Frivate Access Road | Two-way Stop | PM | 20.1 | С | | |
| 5 | W Goshen Avenue & N Plaza Drive | Signal | AM | 37.8 | D | | |
| 3 | W Goshell Avellue & N Flaza Dilive | Signal | PM | 39.7 | D | | |
| 6 | Dwy 1 & Private Access Road | One-Way Stop | AM | | | | |
| " | Dwy I & Filvate Access Road | One-way Stop | PM | FUTURE DRIVEWAYS | | | |
| 7 | Duny 2. 8. Private Access Bood | One Way Sten | AM | FUTURE DRIVEWAYS | | | |
| | Dwy 2 & Private Access Road | One-Way Stop | PM | | | | |

Notes:

Bold values indicate intersections operating at LOS E or F.

ECL = Exceeds Calculable Limit. Reported when delay exceeds 180 seconds.

K:\SND_LDEV\195170022 - Visalia-Plaza 35\Traffic\ANALYSIS\EXCEL\[195170022IN01.xlsm]Opening Year

⁽a) Delay refers to the average control delay for the entire intersection, measured in seconds per vehicle. At a two-way stop-controlled intersection, delay refers to the worst movement.

⁽b) LOS calculations are based on the methodology outlined in the Highway Capacity Manual 6th Edition and performed using Synchro 10.0

FIGURE 5 - OPENING YEAR (2024) BASELINE TRANSPORTATION CONDITIONS

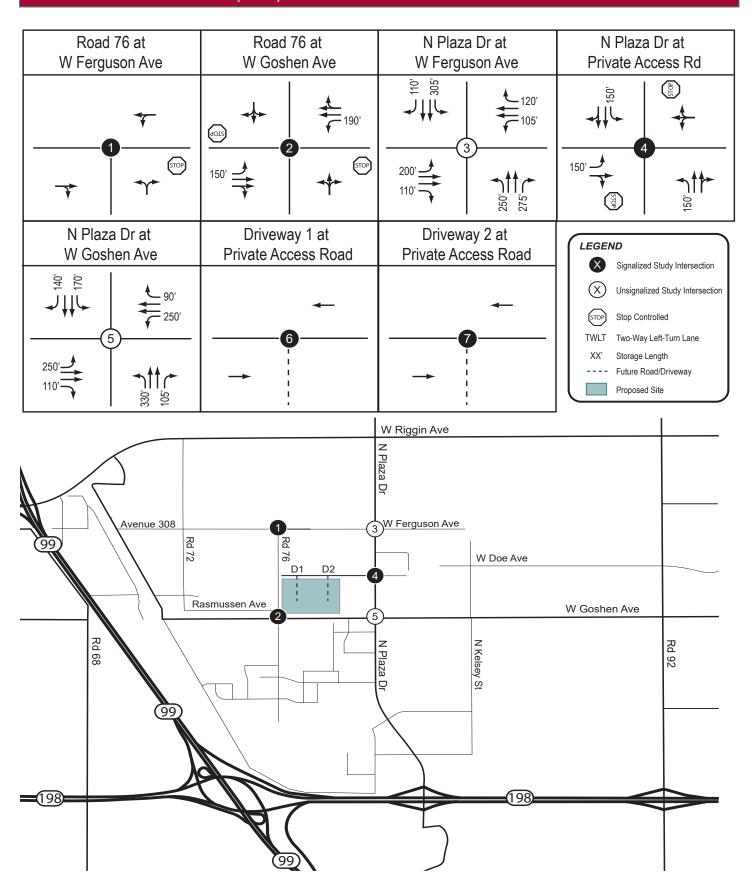
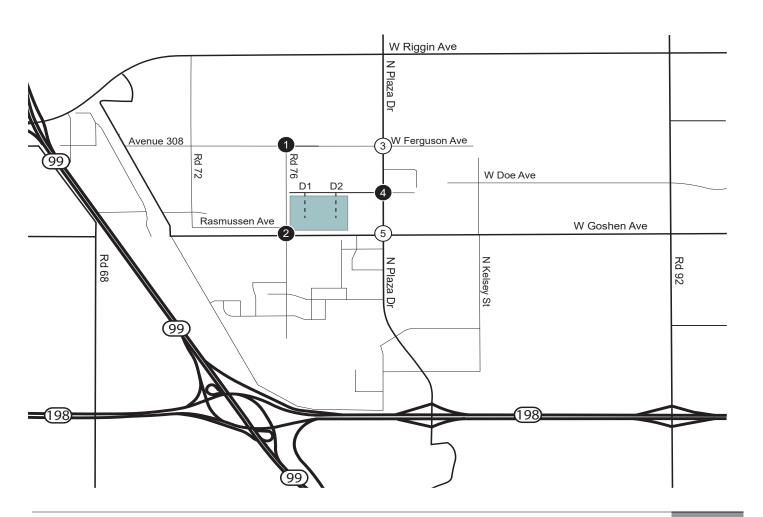


FIGURE 6 - OPENING YEAR (2024) BASELINE CONDITIONS PEAK HOUR TURNING MOVEMENT VOLUMES

| 26 / 15 \$ 92 148 / 86 \$ 92 PM | ⇔ 12 / 23 № 10 / 10 W Ferguson Ave | 2 | S 91/140 ⇔ 158/126 № 37/23 W Goshen Ave | 3 14/28 5 14 | 5 0 / 9 W Ferguson Ave 5 0 Ø | ⇔ 638 / 683 ⇔ 5 / 1 N Plaza Dr | \$ 1/3 \$\alpha\$ 1/6 Private Access Rd \$\alpha\$ 0 60 \$\alpha\$ 0 60 \$\alpha\$ 0 60 |
|---|--|-------------|--|--|--------------------------------|--------------------------------------|--|
| © 42/31 ⇔ 461/487 ⇔ 114/114 N Plaza Dr R | \$ 89 / 102 \$ 125 / 141 \$ 80 / 88 W Goshen Ave | 6 | g 0 0 | 7 | 84 1 489 1 7 7 | | Study Intersection |
| 27 / 72 | 185 / 165 2 10 / 509 2 4 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ | FUTURE DRIV | /EWAY | FUTURE DR | IIVEWAY | Future Roa | ad/Driveway |



4. PROJECT DESCRIPTION

This chapter presents a description of the proposed site use, trip generation, trip distribution, and trip assignment.

PROPOSED SITE USE AND IMPROVEMENTS

The Project includes an approximately 536,000-SF industrial building on an undeveloped 39.25-acre site, which is classified as Light Industrial Land Use by the City's General Plan. The Project proposes a "speculative" general light industrial development; meaning, a final user and operations for the site is not known at this time. The project proposes two (2) full-access, unsignalized driveways along the south side of the future Private Access Road. The Project is consistent with the City's Light Industrial Land Use designation: light manufacturing, warehousing, storage, distribution, research and development, and secondary office (limited customer access), and a FAR below 0.5 (0.31 proposed). The Project would be developed in one phase with completion expected in 2024. The site plan for the Project is shown in **Figure 2**.

TRIP GENERATION

Because a final user operating the site is unknown at this time ("spec" development) and since manufacturing is not intended, traffic generated by the Project is estimated based on the *Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition*, for General Light Industrial (Land Use 110). ITE estimates that the Project would generate a total of 2,610 daily trips, with 397 trips (349 inbound / 48 outbound) during the a.m. commuter peak hour and 348 trips (49 inbound/299 outbound) during the p.m. commuter peak hour. 134 of these daily trips and 5 peak hour trips during both the AM / PM periods are expected by heavy trucks. Consistent with the *Highway Capacity Manual (HCM)* and the City of Visalia's *Procedures for Traffic Impact Analysis* (Updated March 2021), a Passenger Car Equivalent (PCE) of 2.0 was applied to the truck volumes to analyze their effects more accurately on roadway capacity and queueing. The resulting total of 2,744 daily PCE trips, with 403 PCE trips (351 inbound / 51 outbound) during the a.m. peak hour and 354 PCE trips (51 inbound / 303 outbound) during the p.m. peak hour are analyzed. **Table 4** contains a summary of the Project's expected trip generation. **Appendix E** contains relevant ITE Land Use 110 trip generation rate excerpts for passenger vehicles, trucks, and time of day distributions.

TABLE 4 - SUMMARY OF PROJECT TRIP GENERATION - COMMUTER PEAK HOUR

ITE Trip Generation - LU 110 General Light Industrial

| | | | | | | | AM Peak | -Hour | | | | PM Peak- | Hour | | |
|-----------------------------|-----------------------------|----------------------|--------------------|------------------------|-------------|----------|--|-------|-----|-------|-----------------------|---------------------------|------|-----|-------|
| Land Use | Land Use as listed in ITE | ITE Land Use Code | Units ¹ | Trip Rate ² | Daily Trips | % of ADT | ² In:Out Ratio ² | ln | Out | Total | % of ADT ² | In:Out Ratio ² | ln | Out | Total |
| Driveway | <i>r</i> Trips ³ | | | | | | | | | | | | | | |
| Proposed Vehicles | | | | | | | | | | | | | | | |
| Warehouse | General Light Industrial | 110 | 536 ksf | 4.87 / ksf | 2,610 | 15% | 0.88 : 0.12 | 349 | 48 | 397 | 13% | 0.14 : 0.86 | 49 | 299 | 348 |
| Subtotal | | | | | 2,610 | | | 349 | 48 | 397 | | | 49 | 299 | 348 |
| Proposed Passenger Vehicles | | | | | | | | | | | | | | | |
| Warehouse | General Light Industrial | 110 | 536 ksf | 4.62 / ksf | 2,476 | 16% | 0.88 : 0.12 | 346 | 46 | 392 | 14% | 0.13 : 0.87 | 46 | 297 | 343 |
| Proposed Trucks | | | | | | | | | | | | | | | |
| Warehouse | General Light Industrial | 110 | 536 ksf | 0.25 / ksf | 134 | 4% | 0.60 : 0.40 | 3 | 2 | 5 | 4% | 0.50 : 0.50 | 3 | 2 | 5 |
| PCE Breakdown | | | | | | | | | | | | | | | |
| | 2.0 | | | | 268 | 4% | 0.50 : 0.50 | 5 | 5 | 11 | 4% | 0.46 : 0.54 | 5 | 6 | 11 |
| Truck Subtotal (PCE) | | | | | 268 | | | 5 | 5 | 11 | | | 5 | 6 | 11 |
| NET TRIP GENERATION (PCE) = | | | | | 2,744 | | | 351 | 51 | 403 | | | 51 | 303 | 354 |

Note

1. ksf = Thousand Square Feet

K:\SND_LDEV\195170022 - Visalia-Plaza 35\Traffic\ANALYSIS\EXCEL\[195170022TG01.xlsm]110 (SF)

^{2.} Trip rates references from ITE Trip Generation, 11th Edition.

^{3.} Driveway trips are the total number of trips generated by a site.

^{4.} Passenger Car Equivalent (PCE) = 2.0 per City of Visalia TIS Guidelines

PROJECT TRIP DISTRIBUTION AND ASSIGNMENT

The Project's trip distribution was based on Tulare County Association of Governments' Travel Demand Model (TCAG Model). The TCAG Model compiles a wide variety of data and forecasts future transportation demands. The model-based distribution was refined and adjusted based on the current roadway configurations and knowledge of the area. The following is the resulting general project traffic distribution assumed for the LOS analysis for the Opening Year (2024) Baseline Plus Project scenario:

- 35% to/from the north along N Plaza Drive;
- 5% to/from the south along Road 76;
- 40% to/from the south along N Plaza Drive;
- 5% to/from the east along W Fergusson Avenue;
- 5% to/from the east along W Goshen Avenue; and
- 10% to/from the west along W Goshen Avenue.

Appendix B contains the TCAG Model Plots and distribution calculations.

Figure 7 shows the trip distribution for the Opening Year (2024) Baseline Plus Project Conditions.

Based on the assumed trip distribution, the volumes generated by the Project were assigned to the street network. **Figure 8** presents the Project's trip assignment in PCE.

FIGURE 7 - PROJECT TRIP DISTRIBUTION

| 1 | ⇔ (5%) W Ferguson Ave | 2 PA 76 | ⇔ (5%) ঐ (5%) W Goshen Ave | 3 %5¢ + | N Plaza Dr | W Ferguson Ave | 5. 40% N Plaza Dr | Private Access Rd |
|--|--------------------------|---------|----------------------------------|---------|------------|----------------|--------------------|----------------------|
| 84 36 2% ⇔ | | 5% ⇔ | 2 %2 | 5% ⊴ | | (5%) (35%) | (40%) ∅ (60%) ⋈ | © %09 |
| 2 (10%) 4 (40%) (2 (10%) N Plaza Dr | ≅ 10% W Goshen Ave | 6 | | 7 | | ⇔ 50% | | d Study Intersection |
| 10% ⊅ | 40% ū | Dwy 1 | న (%09) | (50%) ⇔ | Dwy 2 | ్ (%09) | | pad/Driveway |



FIGURE 8 - PROJECT TRIP ASSIGNMENT PCE

| 1 | 3 / 15 guson Ave | ⇔ 3 / 15 | c 123 / 18 N Plaza Dr | W Ferguson Ave | 4 07 07 07 07 07 07 07 07 07 07 07 07 07 |
|--|---------------------|---------------------------------|-------------------------|---|--|
| 18/3 ⇒ % B | 18/3 ⇒ | 18/3 & | 18 / 3 ∿ | 3 / 15 % | 20 / 121 Ø % 31 / 182 % & % |
| δ † Ø | 35 / 5 | ය 176 / 26 Private Access Rd | 7 | ⇒ 176 / 26 ≥ 175 / 25 Private Access Rd | LEGEND Signalized Study Intersection Unsignalized Study Intersection |
| 35 / 5 20 07 07 07 07 07 07 07 07 07 07 07 07 07 | Dwy 1 | 26 /152 % | 26 / 152 ⇒ 2 % Q | 25 /151 ss | Future Road/Driveway Proposed Site XX/YY AM/PM Peak Hour Volume |



5. OPENING YEAR (2024) BASELINE CONDITIONS PLUS PROJECT

This chapter summarizes the Opening Year (2024) Plus Project analysis used to determine the effects of the Project on the transportation system, including intersection LOS, signal warrant, and vehicle queuing analyses.

OPENING YEAR (2024) BASELINE PLUS PROJECT CONDITIONS ANALYSIS

Opening Year Plus Project Conditions represent the expected conditions in 2024, when the Project is expected to be complete, with the addition of the Project's improvements and traffic.

LANE GEOMETRY AND CONTROL

The Opening Year (2024) Plus Project Conditions are the same as the Opening Year (2024) conditions with the exception of:

 Private Access Road to provide two (2) one-way stop-controlled full-access driveways to the Project Visalia Plaza 39 site previously referenced in Figure 5.

TRAFFIC VOLUMES

Opening Year (2024) Plus Project volumes were determined by adding the total project traffic, Figure 8, to the Opening Year (2024) Condition's volumes, Figure 6. Opening Year (2024) Plus Project volumes are shown in **Figure 9**.

INTERSECTION LEVEL OF SERVICE

Table 5 displays the intersection LOS analysis results under Opening Year (2024) Plus Project Conditions, showing all intersections would continue to operate at LOS D or better during the commuter peak periods with the exception of:

 Intersection #4 - N Plaza Drive & Private Access Road operate at a LOS F during the AM peak and a LOS E during the PM peak hours of traffic.

Appendix D contains the intersection LOS calculation worksheets.

SIGNAL WARRANTS

Peak hour traffic signal warrants were evaluated at the following unsignalized intersection under the "Plus Project" scenarios using the CA MUTCD traffic signal warrants for the AM and PM peak hours:

Intersection #4 - N Plaza Drive & Private Access Road

The study intersection met the CA MUTCD peak hour signal warrant under "Plus Project" scenarios with the addition of Project traffic. CA MUTCD Peak Hour signal warrants Peak hour traffic signal warrants were evaluated at the deficient intersection identified under the Opening Year (2024) Baseline Plus Project scenario. Based on the 8-hour warrant thresholds, this intersection would meet CA MUTCD warrants for signalization.

OPENING YEAR (2024) BASELINE WITH OPENING YEAR (2024) PLUS PROJECT CONDITIONS PEAK-HOUR INTERSECTION LEVEL OF SERVICE SUMMARY

| | | | | OPENING YEAR | OPENING YEAR (2024) BASELINE | | NG YEAR (2024) WITH P | ROJECT |
|---|--------------------------------------|-----------------|-----------|---------------------|------------------------------|-----------|-----------------------|---------|
| | INTERSECTION | TRAFFIC CONTROL | PEAK HOUR | DELAY (a) | LOS (b) | DELAY (a) | ∆DELAY (a) | LOS (b) |
| 1 | Road 76 & W Ferguson Avenue | Two-Way Stop | AM | 9.8 | A | 10.0 | 0.2 | В |
| | Noad 70 & W Telguson Avenue | Two-Way Stop | PM | 9.9 | Α | 10.0 | 0.1 | В |
| 2 | W Goshen Avenue & Road 76 | Two-Way Stop | AM | 17.9 | С | 19.2 | 1.3 | С |
| | W Gostiell Aveilue & Road 70 | Two-Way Stop | PM | 18.8 | С | 21.3 | 2.5 | С |
| 3 | N Plaza Driva & W Forguson Ava | Signal | AM | 11.2 | В | 12.0 | 0.8 | В |
| 3 | N Plaza Drive & W Ferguson Ave | Signal | PM | 10.6 | В | 10.9 | 0.3 | В |
| | N Plaza Drive & Private Access Road | Two-Way Stop | AM | 18.5 | С | 62.6 | 44.1 | F |
| 4 | IN Flaza Drive & Frivate Access Road | Two-way Stop | PM | 20.1 | С | 41.1 | 21.0 | E |
| 5 | W Goshen Avenue & N Plaza Drive | Signal | AM | 37.8 | D | 37.9 | 0.1 | D |
| 3 | W Gostieli Aveilue & N Flaza Dilve | Signal | PM | 39.7 | D | 40.0 | 0.3 | D |
| 6 | Duni 1 9 Drivete Access Dood | One Way Sten | AM | | | 8.4 | 0.0 | Α |
| 0 | Dwy 1 & Private Access Road | One-Way Stop | PM | PM FUTURE PRIVEWAYO | | 8.9 | 0.0 | A |
| 7 | Duny 2 & British Assess Board | One Way Sten | AM | FUTURE DRIVEWAYS | | 8.5 | 0.0 | A |
| / | Dwy 2 & Private Access Road | One-Way Stop | PM | | | 10.0 | 0.0 | В |

Notes:

Bold values indicate intersections operating at LOS E or F.

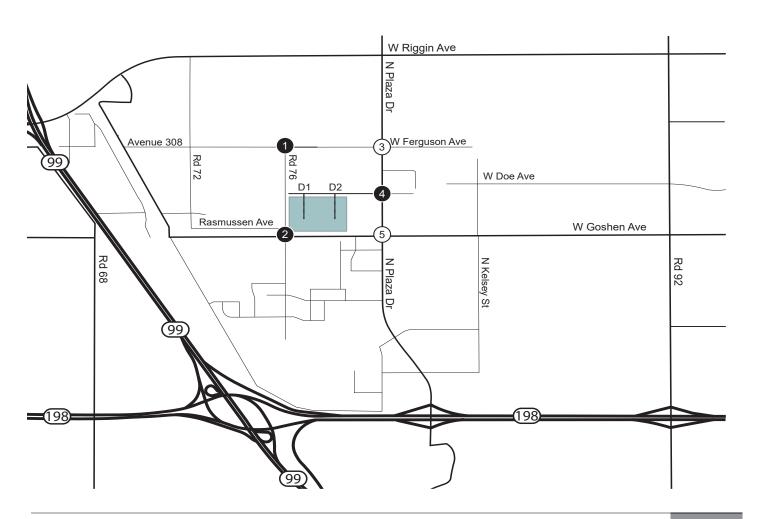
ECL = Exceeds Calculable Limit. Reported when delay exceeds 180 seconds.

(a) Delay refers to the average control delay for the entire intersection, measured in seconds per vehicle. At a two-way stop-controlled intersection, delay refers to the worst movement.

(b) LOS calculations are based on the methodology outlined in the Highway Capacity Manual 6th Edition and performed using Synchro 10.0

K:\SND_LDEV\195170022 - Visalia-Plaza 35\Traffic\ANALYSIS\EXCEL\[195170022IN01.xlsm]Opening Year + OYWP

| 1 | ⇔ 15 / 38 | 7 0 /7 0 19 /28 P 19 /28 P 19 /131 P Rd 76 | □ 91 / 140 □ 161 / 141 □ 40 / 38 W Goshen Ave | 27 /11 \$\times 701/532 \$\times 6/4 \$\text{N Plaza Dr}\$ | □ 0 / 9 2 7 / 29 W Ferguson Ave | 4 07 07 07 07 07 07 07 07 07 07 07 07 07 |
|---|---|--|--|---|-----------------------------------|--|
| 44 / 18 | 66 / 130 & 10 / 10 & | 1/7 | 8 / 15 & 6 / 19 & 37 / 77 & & | 14/28 | 87 / 62 & 507 / 718 & 7 / 18 & | 20 / 121 & \$\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ |
| \$ 47 /61 \$ 481 /608 \$ 119 /144 N Plaza Dr | S 124 / 107 ⇔ 125 / 141 № 80 / 88 W Goshen Ave | 6 | | 7 | ⇔ 176 / 26 | LEGEND Signalized Study Intersection Unsignalized Study Intersection |
| 62 / 77 | 185 / 165 & 650 / 529 & 66 / 59 & | Dwy 1 | 26 /152 % | 26 / 152 ⇒ 7 m d | 25 /151 % | Proposed Site XX/YY AM/PM Peak Hour Volume |



VEHICLE QUEUING

Vehicle queuing that exceeds a turn pocket length can create potentially hazardous conditions by blocking or disrupting through traffic in adjacent travel lanes. The effect of vehicle queuing was analyzed by reporting the 95th percentile queues for turning movements where the Project would add left-turn or right-turn trips at intersections and driveways. The 95th percentile is defined as the queue length that has only a 5-percent probability of being exceeded during the analysis time period. The following movements were evaluated:

- Intersection #1 Road 76 & W Ferguson Avenue (eastbound thru-right, westbound thru-left, and northbound left-right)
- Intersection #2 W Goshen Avenue & Road 76 (eastbound left, eastbound thru-right, westbound left, westbound thru-right, northbound left-thru-right, and southbound left-thru-right)
- Intersection #3 N Plaza Drive & W Ferguson Avenue (eastbound left, eastbound right, westbound left, westbound right, northbound left, northbound right, southbound left, and southbound right)
- Intersection #4 N Plaza Drive & Private Access Road (eastbound left, eastbound thru-right, westbound left-thru-right, northbound left, and southbound right)
- Intersection #5 W Goshen Avenue & N Plaza Drive (eastbound left, eastbound right, westbound left, westbound right, northbound left, northbound right, southbound left, and southbound right)
- Intersection #6 Dwy 1 & Private Access Road (eastbound thru-right, westbound thru-left, and northbound left-right)
- Intersection #7 Dwy 2 & Private Access Road (eastbound thru-right, westbound thru-left, and northbound left-right)

The 95th percentile queue lengths are summarized in **Table 6.** For the Opening Year (2024) Plus Project conditions, there are no queueing deficiencies expected for all study intersections.

Queuing analysis calculation sheets are provided in Appendix E.

Table 6: Vehicle Queuing Summary

| | | | | | 95 th Percentile Queue Length (ft) | | | | | |
|---|---|-----------------|----------|------------------|---|----------------|-------------------------------------|------|-------|--|
| | | | | | | ning (2024) | Opening Year (2024) Plus Project | | | |
| | | | | Queue Storage | | | Queue Storage | | | |
| # | Intersection | Control | Movement | (ft) | AM | PM | (ft) | AM | PM | |
| | Road 76 & W Ferguson Ave | One-Way Stop | EBTR | N/A ¹ | - | - | N/A ¹ | - | - | |
| 1 | | | WBTL | N/A ¹ | - | - | N/A ¹ | - | - | |
| | reiguson Ave | | NBLR | N/A ¹ | <25 | <25 | N/A ¹ | <25 | <25 | |
| | W Goshen Avenue & Road 76 | Two-Way Stop | EBL | 150 | - | - | 150 | <25 | - | |
| 2 | | | EBTR | N/A ¹ | - | - | N/A ¹ | - | - | |
| | | | WBL | 190 | <25 | <25 | 190 | <25 | <25 | |
| | | | WBTR | N/A ¹ | - | - | N/A ¹ | - | - | |
| | | | NBLTR | N/A ¹ | <25 | <25 | N/A ¹ | <25 | <25 | |
| | | | SBLTR | N/A ¹ | 60 | 50 | N/A ¹ | 65 | 62.5 | |
| 3 | N Plaza Drive & W Ferguson Ave | Signal | EBL | 300 | 20 | 36 | 300 | 20 | 36 | |
| | | | EBR | 110 | - | 11 | 110 | - | 13 | |
| | | | WBL | 120 | 15 | 37 | 120 | 15 | 37 | |
| | | | WBR | 105 | - | - | 105 | - | - | |
| 3 | | | NBL | 250 | #113 | 52 | 250 | #118 | #73 | |
| | | | NBR | 275 | - | - | 275 | - | - | |
| | | | SBL | 305 | 14 | 10 | 305 | 14 | 10 | |
| | | | SBR | 110 | - | - | 110 | - | - | |
| | N Plaza Drive & Private Access Road | Two-Way Stop | EBL | N/A ¹ | - | - | N/A ¹ | 45 | 127.5 | |
| | | | EBTR | N/A ¹ | - | - | N/A ¹ | <25 | 30 | |
| 4 | | | WBLTR | N/A ¹ | - | <25 | N/A ¹ | <25 | <25 | |
| | | | NBL | N/A ¹ | - | - | 150 | 35 | <25 | |
| | | | SBL | N/A ¹ | - | - | 150 | - | - | |
| 5 | W Goshen Avenue & N Plaza Drive | Signal | EBL | 250 | 42 | #113 | 250 | #99 | #121 | |
| | | | EBR | 110 | 59 | 61 | 110 | 59 | 61 | |
| | | | WBL | 250 | #131 | #140 | 250 | #131 | #140 | |
| | | | WBR | 90 | 38 | 43 | 90 | 48 | 44 | |
| | | | NBL | 330 | #256 | #242 | 330 | #256 | #242 | |
| | | | NBR | 105 | 11 | 8 | 105 | 11 | 8 | |
| | | | SBL | 170 | #145 | #147 | 170 | #153 | #197 | |
| | | | SBR | 140 | _ | _ | 140 | 3 | 9 | |
| 6 | Dwy 1 & Private Access Road | One-Way | EBTR | DNE ² | - | - | N/A ¹ | - | - | |
| | | Stop | WBTL | DNE ² | - | - | N/A ¹ | <25 | <25 | |
| | Access Noau | | NBLR | DNE ² | - | - | N/A ¹ | <25 | <25 | |
| | Dwy 2 & Private | One-Way | EBTR | DNE ² | - | - | N/A ¹ | - | - | |
| 7 | Access Road | Stop | WBTL | DNE ² | - | - | N/A ¹ | <25 | <25 | |
| | / 100003 1 10du | | NBLR | DNE ² | - | - | N/A ¹ | <25 | <25 | |

Note:

NBR=northbound right, NBL=northbound left, NBLR = northbound left-right, NBLTR = northbound left-thru-right, SBL= southbound left, SBR = southbound right, SBLR = southbound left-right, SBLTR = southbound left-thru-right, EBL= eastbound left, EBR = eastbound right, EBTR = eastbound thru-right, WBL=westbound left, WBR = westbound right, WBTL = westbound thru-right, WBLTR = westbound left-thru-right

95th percentile volume exceeds capacity; queue may be longer. Queue shown is maximum after two cycles.

N/A¹ – Queue storage length not available at this location since no turn pocket for this movement

DNE² – Does not exists, queue storage lengths available for with project scenario only

Project modifications to turn pocket lengths shown <u>underlined</u>. Queue lengths greater than queue storage are **bolded**. Queues length less than 25 feet are reported as <25.

FINDINGS AND CONCLUSIONS

The results of the foregoing analysis indicate that the Project would degrade the LOS operations with the addition of the Project's traffic at intersection of N Plaza Drive / Private Access Road. **Table 7** displays the intersection LOS analysis results under Opening Year (2024) Plus Project with a signalized intersection, showing that the installation of a traffic signal would improve the operations to LOS D or better. **Appendix E** contains the intersection LOS calculation worksheets.

Table 7: Opening Year (2024) Plus Project (With Improvement) Level of Service Summary

| # | Intersection | Control | Opening (2024) Year Plus Project | | | | Opening (2024) Year Plus Project (With Improvement) | | | |
|---|--|---------|----------------------------------|-----|---------|-----|--|-----|---------|-----|
| | | | AM Peak | | PM Peak | | AM Peak | | PM Peak | |
| | | | Delay | LOS | Delay | LOS | Delay | LOS | Delay | LOS |
| | | | (sec) | | (sec) | | (sec) | | (sec) | |
| 4 | N Plaza Drive & Private Access Road | Signal | 62.5 | F | 41.1 | E | 8.8 | Α | 9.5 | Α |

6. ADDITIONAL TOPICS

This section discusses site access, pedestrian, bicycle and sight distance recommendations for the Project.

SITE ACCESS

Access to the Project site would be established through the construction of two (2) full-access unsignalized driveways along the future Private Access Road (under construction by Project Gold Bar). The following summarizes the project access locations:

- Local Access Road & Project Driveway 1
 - Construct a full-access driveway <u>a minimum of 200-feet east of the Road 76 centerline</u> per the City of Visalia standards;
 - o Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane; and
 - o Provide one outbound lane (stop-controlled).
- Local Access Road & Project Driveway 2
 - Construct a full-access driveway per the City of Visalia standards;
 - o Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane; and
 - o Provide one outbound lane (stop-controlled).

Appendix E contains the queuing worksheets for the Project's driveways. These AM/PM Peak Hour worksheets are the results of the Opening Year (2024) Plus Project Conditions and show that the proposed driveway throats are a sufficient length to accommodate the expected queues and not expected to impede the on-site vehicle circulation.

SIGHT DISTANCE

A sight distance analysis for each Project driveway was conducted to determine if vehicles and trucks exiting each of the Project driveways would have adequate sight distance to observe conflicting traffic along the intersecting roadway (Private Access Road). Intersection sight distance for the Project driveways were evaluated following methodology from the American Association of State Highway and Transportation Officials (AAHSTO), A Policy on Geometric Design of Highway and Street, 7th Edition². No spot speed study was conducted since the Private Access Road has not yet been constructed. Because the future Private Access Road is unclassified, a 30-mph design speed was used to determine sight distance (assumed 25-mph posted speed plus 5-mph) for a required. Based on this assumed speed, a corner sight distance of 300-feet is required. Appendix G contains figures showing the two (2) proposed access driveways would exceed the 300-foot corner sight distance requirement.

² A Policy on Geometric Design of Highway and Street, 7th Edition, American Association of State Highway and Transportation Officials (AAHSTO), 2018.

7. CONCLUSIONS AND RECOMMENDATION SUMMARY

The Project proposes an approximately 536,000-SF industrial building located within the City of Visalia. The site is located on an undeveloped 39.25-acre site at 2045 N Plaza Drive, which is classified as Light Industrial Land Use by the City's General Plan. The site is bound by Route 76 to the west, W, Goshen Avenue to the south, existing industrial warehouses to the east and a future Private Access Road to the north. The Project proposes a "speculative" general light industrial development; meaning, a final user and operations for the site is not known at this time. The Project is expected to generate of 2,744 daily PCE trips, with 403 PCE trips (351 inbound / 51 outbound) during the a.m. peak hour and 354 PCE trips (51 inbound / 303 outbound) during the p.m. peak hour.

SITE ACCESS

Access to the Project site would be established through the construction of two (2) full-access unsignalized driveways along the future Private Access Road (under construction by Project Gold Bar). The following summarizes the project access locations:

- Local Access Road & Project Driveway 1
 - Construct a full-access driveway <u>a minimum of 200-feet east of the Road 76 centerline</u> per the City of Visalia standards;
 - o Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane: and
 - o Provide one outbound lane (stop-controlled).
- Local Access Road & Project Driveway 2
 - o Construct a full-access driveway per the City of Visalia standards;
 - o Design driveway to accommodate inbound/outbound truck turning paths;
 - o Provide one inbound lane; and
 - o Provide one outbound lane (stop-controlled).

A sight distance analysis for each Project driveway shows the two (2) proposed access driveways would exceed the 300-foot corner sight distance requirement.

PEDESTRIAN FACILITIES

The Applicant is installing sidewalk and pedestrian ramps along the Local Access Road as part of the Project Goldbar Conditions of Approval. Pedestrian connectivity would also be enhanced by the installation of traffic signal at the N Plaza Drive / Local Access Road intersection.

BICYCLE FACILITIES

The Applicant is installing Class II bike lanes along N Plaza Drive, between W Fergusson Avenue and W Goshen Avenue Project, as part of the Project Gold Bar Conditions of Approval.

OFF-SITE RECOMMENDATIONS

The traffic operation analysis shows that the Project would degrade the LOS operations with the addition of the Project's traffic at intersection of N Plaza Drive / Private Access Road. This intersection meets the CA MUTCD 8-hour signal warrant under Opening Year (2024) conditions with the addition of project traffic, and the installation of traffic signals would improve the intersection operations to LOS B or better.

The following intersections improvements are recommended:

- Provide northbound left-turn pocket (150-foot minimum);
- Provide southbound left-turn pocket (150-foot minimum);
- Provide southbound right-turn lane between the southernmost Project Gold Bar driveway and intersection;
- Provide eastbound left-turn pocket (150-foot minimum);
- Provide eastbound through/right-turn lane;
- Provide westbound left/through/right-turn lane; and
- Install traffic signal (NB/SB Protected LT Phasing & EB/WB Permitted Phasing).

It is recommended that the Applicant modify the street improvement plans for Project Gold Bar for the construction of southbound right-turn pocket. **Appendix C** contains a drawing of the recommended modifications.

The Project is not expected to cause adverse effects to the turn lanes queuing.

APPENDIX

- A PROJECT TRAFFIC SCOPE OF WORK
- B EXISTING TRAFFIC VOLUME DATA SHEETS AND TRAVEL DEMAND MODELS
- C PROJECT GOLD BAR STREET IMPROVEMENTS AND MODIFICATIONS
- D LEVEL OF SERVICE CALCULATION SHEETS & VEHICLE QUEUING CALCULATION SHEETS
- **E ITE TRIP GENERATION EXCERPTS**
- F CA MUTCD TRAFFIC SIGNAL WARRANTS
- G SIGHT DISTANCE ASSESSMENT

A – Project Traffic Scope of Work



MEMORANDUM

To: Leslie Blair, P.E.

City of Visalia

From: Joe Shultz, P.E.

Kimley-Horn and Associates, Inc.

Date: April 11, 2022

Subject: Seefried Industrial Development: Mid-Valley Logistics Center (Visalia Plaza 39)

Trip Generation and Traffic Analysis Scope of Work

Kimley-Horn has prepared a trip generation assessment for an approximately 536,000-SF industrial warehouse (Project) proposed in Visalia, just east of the Tulare County border, in order to provide documentation as to concurrence with the City's General Plan. The Project site is located on an undeveloped 39.25-acre site at 2045 N Plaza Drive, approximately 1-mile east of State Route 99 (SR 99), and is classified as Light Industrial Land Use by the City's General Plan. The site is bound by Route 76 to the west, W, Goshen Avenue to the south, existing industrial warehouses to the east and a future Private Access Road to the north, as shown in **Figure 1**.

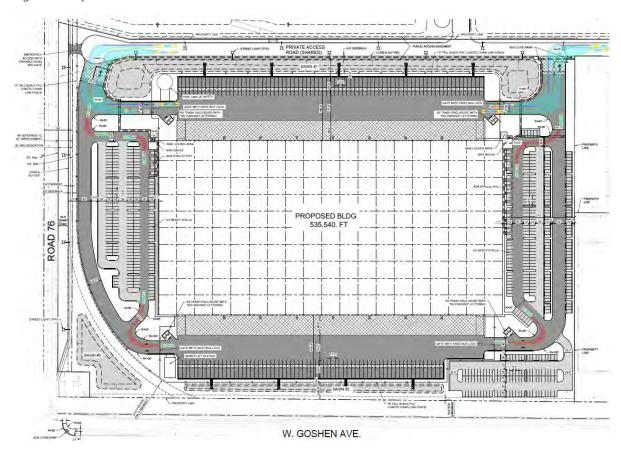
Figure 1: Project Location





Access to the site would be facilitated via two (2) full-access driveways along the future access road to the north. The Project is consistent with the City's Light Industrial Land Use designation: light manufacturing, warehousing, storage, distribution, research and development, and secondary office (limited customer access), and a FAR below 0.5 (Project proposes 0.31). The Project site plan is presented in **Figure 2.**

Figure 2: Project Site Plan



Based on site plan review comments issued by City staff on March 2, 2022, the Project requires Non-Discretionary approvals, meaning a Traffic Impact Analysis (TIA) is not required. The Project is required to determine the expected trip generation and provide an analysis of the site's access, adjacent intersections, and on-site circulation. The following outlines the expected trip generation and summarizes the scope required for the Project's site-specific Traffic Analysis (TA).



Trip Generation

Because a final user operating the site is unknown at this time ("spec" development) and since manufacturing is not intended, traffic generated by the Project is estimated based on the *Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition,* for General Light Industrial (Land Use 110). ITE estimates that the Project would generate a total of 2,610 daily trips, with 397 trips (349 inbound / 48 outbound) during the a.m. commuter peak hour and 348 trips (49 inbound/299 outbound) during the p.m. commuter peak hour. 134 of these daily trips and 5 peak hour trips during both the AM / PM periods are expected by heavy trucks. Consistent with the *Highway Capacity Manual (HCM)* and the City of Visalia's *Procedures for Traffic Impact Analysis* (Updated March 2021), a Passenger Car Equivalent (PCE) of 2.0 was applied to the truck volumes to analyze their effects more accurately on roadway capacity and queueing. The resulting total of 2,744 daily PCE trips, with 403 PCE trips (351 inbound / 51 outbound) during the a.m. peak hour and 354 PCE trips (51 inbound / 303 outbound) during the p.m. peak hour would be analyzed. **Table A** contains a summary of the project's proposed trip generation.

Table A ITE Trip Generation - LU 110 General Light Industrial AM Peak-Hour PM Peak-Hou Daily Trips % of ADT² In:Out Ratio² Out Total % of ADT² In:Out Ratio² Land Use as listed in ITE Land Use Driveway Trips Proposed Vehicles Subtotal 2,610 397 Proposed Passenger Vehicles eral Light Industria Proposed Trucks ral Light Industria PCE Breakdown Truck Subtotal (PCE) 268 11 6 11 NET TRIP GENERATION (PCE) = 351 51 51 303 354 2,744 ksf = Thousand Square Fee

Table 1

Study Area

The Project's trip generation would be evaluated at the following locations:

- Road 76 and W Ferguson Avenue (Unsignalized);
- Road 76 and W Goshen Avenue (Unsignalized);
- 3. N Plaza Drive and W Ferguson Avenue (Signalized);
- 4. N Plaza Drive and Future Access Road (Unsignalized); and
- 5. N Plaza Drive and W Goshen Avenue (Signalized).



Figure 3 shows the location of the study intersections around the site.

Figure 3: Project Study Area



Methodology and Analysis Scenarios

The TA would analyze the following scenarios:

- Opening Year Conditions
- Opening Year Plus Project Conditions

Opening Year volumes will be developed using a growth factor determined by the Tulare County Associate of Governments (TCAG) travel demand model.



The following traffic operation analysis will be conducted:

- Level of Service: Conduct using Synchro software and HCM 6th Edition methodology.
- Traffic signal warrants: Conduct for the new unsignalized study intersection of the "Private Access Road" / N Plaza Drive based on guidance in California's Manual on Uniformed Controlled Devices (CA MUTCD). Assume full median opening for the intersection.
- Queuing Analysis: Evaluate turn lane queuing at study intersections using Synchro software.
- Site Access and On-Site Circulation Evaluation: Evaluate site plan for adequate site access and circulation. Conduct stopping sight and corner sight distance evaluation for proposed access driveways.
- Traffic Impact Fee (TIF): Identify improvements needed in concurrence with TIF

Kimley-Horn will identify any project-related deficiencies based on criteria within the City's TIA guidelines.

Vehicle Miles Traveled

Since the Project requires Non-Discretionary approvals, a CEQA Vehicle Miles Traveled (VMT) analysis is not required by the Project.

B – Existing Traffic Volume Data Sheets and Travel Demand Model

Location: Rd 76 & Ave 308/W Ferguson Ave City: Visalia

Project ID: 22-090052-001

| | | | | | | | | | | | | | P | roject ID: Date: | 22-090052 4/21/2022 | | |
|------------------|----------|--------|------------|--------|-------|--------|-------------|------------|------------|-------------|--------------|------------|----------|---------------------|------------------------|------------|--------------|
| ı | | | | | | | | Data · | - Total | | | | | | | | 1 |
| NS/EW Streets: | | | | | | | | | Av | re 308/W Fe | - | 2 | F | Ave 308/W I | | /e | |
| ΔM | 1 | | OUND 0 | 0 | 0 | | HBOUND 0 | 0 | 0 | EASTB 0 | OUND 1 | 0 | 0 | WEST 0 | BOUND | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | NOON | | 0 0 | 0 0 | 0 | 0 0 | 12 15 | 0 | 0 | 0 0 | 0 0 | 0 | 20 21 | | | | |
| | | | | | _ | | 0 | 0 | 0 | 0 | 22 27 | 0 | 0 | 0 | 0 | 0 | 28 40 |
| | | | | | | | 0 | 0 | 0 | 0 | 17 | 0 | 0 | 0 | 0 | 0 | 31 |
| | | | | | | | 0 | 0 | 0 | 0 | 32 62 | 0 | 0 | 0 | 0 | 0 | 39 72 |
| 7:45 AM | 7 | 0 | 0 | 0 | Ō | 0 | 0 | 0 | 0 | 0 | 62 | Ō | 0 | 0 | 0 | 0 | 69 |
| | | | | | _ | | 0 | 0 | 0 | 0 | 28 17 | 0 | 0 | 0 | 0 | 0 0 | 55 49 |
| 8:30 AM | 13 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 33 |
| | | | | | | | 0 | 0 | 0 | 0 | 13 22 | 0 | 0 | 0 | 0 | 0 | 30 30 |
| | | | | | | | 0 | 0 | 0 | 0 | 21 13 | 0 | 0 | 0 | 0 | 0 | 33 20 |
| | | | | | | | 0 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 37 |
| | NI | NT | NR | NH | SI | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| | 203 | 0 | 0 | 0 | | | 0 | 0 | 0 | 0 | 404 | 0 | 0 | 0 | 0 | 0 | 607 |
| | | | | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | TOTAL |
| | | | | | | | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 169 0.681 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 245 |
| PEAR HR FACTOR: | 0.594 | | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.60 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.851 |
| | | NORTHB | OUND | | | SOUT | HBOUND | | | EASTB | OUND | | | WEST | BOUND | | |
| NOON | | 0 | 0 | | | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | TOTAL |
| | 13 | | 0 | | | 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 18 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 31 |
| | | | | | | | 0 | 0 | 0 | 0 | 18 14 | 0 | 0 | 0 0 | 0 | 0 0 | 31 30 |
| 10:45 AM | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 33 |
| | | | | | | | 0 | 0 | 0 | 0 | 24 14 | 0 1 | 0 | 0 0 | 0 0 | 0 0 | 39 28 |
| | | | | | | | 0 | 0 | 0 | 0 | 13 14 | 0 | 0 | 0 | 0 | 0 | 29 27 |
| 12:00 PM | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 23 |
| | | | | | | | 0 | 0 | 0 | 0 | 18 20 | 0 | 0 | 0 0 | 0 | 0 | 33 41 |
| 12:45 PM | | | | | | | 0 | 0 | 0 | 0 | 21 10 | 0 | 0 | 0 | 0 | 0 | 41 28 |
| 1:15 PM | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 0 | 0 | 0 | 0 | 0 | 36 |
| | 22 13 | | | | | | 0 | 0 | 0 | 0 | 24 25 | 0 | 0 | 0 | 0 | 0 | 46 38 |
| | NII | NIT | ND | | | | SR | SU | | | ER | EU | WL | WT | WR | WU | TOTAL |
| | 254 | 0 | 0 | 1 | | | 0 0 | 0 | EL 0 | ET 0 | 278 | 1 | 0 VVL | 0 | 0 VVR | 0 | 534 |
| | | | | 0.39% | | | | | 0.00% | 0.00% | 99.64% | 0.36% | | | | | TOTAL |
| PEAK HR VOL : | 81 | 0 | 0 | | | | 0 | 0 | 0 | 0 | 70 | 0 | 0 | 0 | 0 | 0 | 151 |
| PEAK HR FACTOR : | 0.920 | | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.729 29 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.821 |
| | | NORTHR | OLIND | | | SOUT | HBOLIND | | | EASTB | OLIND | | | WEST | BOUND | | |
| PM | | 0 | 0 | | | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | |
| 2:00 PM | | | | | | | SR 0 | SU 0 | EL 0 | ET 0 | ER 26 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 52 |
| | | | | | | | 0 | 0 | 0 | 0 | 25 27 | 0 | 0 | 0 0 | 0 | 0 | 61 46 |
| 2:45 PM | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 0 | 0 | 0 | 0 | 0 | 59 |
| | | | | | | | 0 0 | 0 0 | 0 | 0 0 | 21 25 | 0 | 0 | 0 0 | 0 | 0 0 | 49 62 |
| 3:30 PM | 47 | | | | | 0 | 0 | 0 | 0 | 0 | 20 21 | 0 | 0 | 0 | 0 | 0 | 67 51 |
| 4:00 PM | 35 | | 0 | 0 | | | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 67 |
| 1.13 111 | | • | • | • | | • | 0 0 | 0 0 | 0 | 0 0 | 25 27 | 1 0 | 0 | 0 | 0 | 0 | 57 64 |
| 4:45 PM | 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 0 | 0 | 0 | 0 | 50 |
| | | | | | | | 0 0 | 0 0 | 0 | 0 0 | 20 23 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 59 64 |
| | | | | | | | 0 0 | 0 0 | 0 | 0 0 | 27 21 | 0 | 0 | 0 0 | 0 | 0 0 | 60 43 |
| 3.13111 | | | | | | | | | | | | | | | | | |
| TOTAL VOLUMES : | 520 | 0 | 0 | 0 | | | SR 0 | SU 0 | EL 0 | ET 0 | ER 390 | EU 1 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 911 |
| | 100.00% | 0.00% | 0.00% | | | | | | 0.00% | 0.00% | 99.74% | 0.26% | | | | | TOTAL |
| PEAK HR VOL : | 149 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 98 | 0 | 0 | 0 | 0 | 0 | 247 |
| PEAK HR FACTOR : | 0.793 | 0.000 | 0.000 3 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.766 56 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.922 |
| | | | | | | | | | | | | | | | | | |

Location: Rd 76 & Ave 308/W Ferguson Ave

| City: | Visalia No Control | | guson Ave | | | | | | | | | | P | | 22-090052 4/21/2022 | | |
|-----------------------------------|-----------------------|----------------------------|-------------|------------|------------|---------|-------------|---------|------------------|------------------|---------------|------------------|------------|------------|------------------------|---------|--------------|
| ī | | | | | | | | Data | - Cars | | | | | | | | 1 |
| NS/EW Streets: | | Rd 7 | | | | | 76 | | Av | re 308/W Fe | - | 2 | A | | Ferguson Av | re | |
| AM | 1 | NORTH | 0 | 0 | 0 | 0 | -BOUND | 0 | 0 | EASTB 0 | 1 | 0 | 0 | 0 | BOUND 0 | 0 | TOTAL |
| 6:00 AM | NL 6 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | 0 0 | ER 11 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 17 |
| 6:15 AM 6:30 AM | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 22 | 0 | 0 | 0 | 0 | 0 | 21 28 |
| 6:45 AM 7:00 AM | 13 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 16 | 0 | 0 | 0 | 0 | 0 | 39 29 |
| 7:15 AM 7:30 AM | 7 10 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 31 60 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 38 70 |
| 7:45 AM 8:00 AM | 7 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 61 28 | 0 | 0 | 0 | 0 | 0 | 68 55 |
| 8:15 AM 8:30 AM | 32 13 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 17 20 | 0 0 | 0 | 0 0 | 0 0 | 0 | 49 33 |
| 8:45 AM 9:00 AM | 17 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 21 | 0 | 0 | 0 | 0 | 0 | 29 29 |
| 9:15 AM 9:30 AM | 12 6 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 13 | 0 | 0 | 0 | 0 | 0 | 31 19 |
| 9:45 AM | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 36 |
| TOTAL VOLUMES : | NL 199 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 392 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 591 |
| APPROACH %'s : PEAK HR : | | 0.00% 07:30 AM - | | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 76 0.594 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 166 0.680 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 242 0.864 |
| | | 0.59 | | | | | | | | 0.6 | | | | | | | 0.004 |
| NOON | 1 | NORTH 0 | 0 | 0 | 0 | 0 | HBOUND 0 | 0 | 0 | EASTB 0 | 1 | 0 | 0 | 0 | TBOUND 0 | 0 | |
| 10:00 AM | NL 9 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET | ER 18 | EU | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 27 |
| 10:15 AM 10:30 AM | 10 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 18 13 | 0 | 0 | 0 | 0 | 0 | 28 27 |
| 10:45 AM 11:00 AM | 13 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 22 | 0 | 0 | 0 | 0 | 0 | 32 36 |
| 11:15 AM 11:30 AM | 11 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 12 | 0 | 0 | 0 | 0 | 0 | 26 28 |
| 11:45 AM 12:00 PM | 13 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 10 | 0 | 0 | 0 | 0 | 0 | 27 22 |
| 12:15 PM 12:30 PM | 14 21 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 | 18 20 | 0 0 | 0 | 0 | 0 | 0 0 | 32 41 |
| 12:45 PM 1:00 PM | 19 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 40 26 |
| 1:15 PM 1:30 PM | 21 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 24 | 0 | 0 | 0 | 0 | 0 | 36 46 |
| 1:45 PM | 13 | 0 NT | 0 NR | 0 NU | 0 | 0 ST | 0 SR | 0 | 0 | 0 | 23 ER | 0 | 0 WL | 0 WT | 0 WR | 0 WU | 36 TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | NL 238 99.58% | 0 0.00% | 0 0.00% | 1 0.42% | SL 0 | 0 | 0 | SU 0 | EL 0 0.00% | ET 0 0.00% | 270 99.63% | EU 1 0.37% | 0 | 0 | 0 | 0 | 510 |
| PEAK HR : | | 12:45 PM - 0 | | 0.1270 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 0.57 70 | 0 | 0 | 0 | 0 | TOTAL 148 |
| PEAK HR FACTOR : | 0.886 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.729 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.804 |
| 200 | | NORTH | | | | | HBOUND | | | EASTB | | | | | TBOUND | | |
| PM | 1 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 1 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | TOTAL |
| 2:00 PM 2:15 PM | 26 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 25 | 0 | 0 | 0 | 0 | 0 | 52 61 |
| 2:30 PM 2:45 PM | 18 31 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 26 | 0 | 0 | 0 | 0 | 0 | 44 57 |
| 3:00 PM 3:15 PM | 28 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 22 | 0 | 0 | 0 | 0 | 0 | 48 58 |
| 3:30 PM 3:45 PM | 46 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 19 19 | 0 | 0 | 0 | 0 | 0 | 65 48 |
| 4:00 PM 4:15 PM | 33 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 23 | 0 | 0 | 0 | 0 | 0 | 64 54 |
| 4:30 PM 4:45 PM | 36 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 22 | 0 | 0 | 0 | 0 | 0 | 63 49 |
| 5:00 PM 5:15 PM | 38 41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 23 | 0 | 0 | 0 | 0 | 0 | 58 64 |
| 5:30 PM 5:45 PM | 33 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 27 20 | 0 | 0 | 0 | 0 | 0 | 60 40 |
| TOTAL 1/21 | NL FOO | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER 276 | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 100.00% | 0.00% | 0.00% | 0 0.00% | 0 | 0 | 0 | 0 | 0.00% | 0 0.00% | 376 99.73% | 1 0.27% | 0 | 0 | 0 | 0 | 885 |
| PEAK HR : | 144 | 0 0 0 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 91 | 0 | 0 | 0 | 0 | 0 | TOTAL 235 |
| PEAK HR FACTOR : | 0.783 | 0.000 0.78 | 0.000 33 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.734 34 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.904 |

Location: Rd 76 & Ave 308/W Ferguson Ave City: Visalia

Project ID: 22-090052-001

| | No Control | | | | | | | Data | - HT | | | | | Project ID: Date: | 4/21/2022 | | |
|-----------------------------------|------------|---------------------|-------------------|------------|------------|------------|-------------|------------|------------|-------------|-------------|------------|------------|----------------------|------------|------------|-------------|
| NS/EW Streets: | | Rd 7 | 76 | | | Rd | 1 76 | | | re 308/W Fe | erauson Ave | 2 | , | Ave 308/W | erauson A | /e | |
| | | NORTHI | | | | | HBOUND | | 7 | EASTE | - | | | | BOUND | | |
| AM | 1 NL | 0 NT | 0 NR | 0 NU | 0 SL | 0 ST | 0 SR | 0 SU | 0 EL | 0 ET | 1 ER | 0 EU | 0 WL | 0 WT | 0 WR | 0 WU | TOTAL |
| 6:00 AM | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| 6:15 AM 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 7:00 AM 7:15 AM | 1 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 1 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 2 |
| 7:30 AM 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 |
| 8:45 AM 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 9:30 AM 9:45 AM | 1 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 1 | 0 | 0 | 0 0 | 0 0 | 0 | 1 |
| | | | | | | | | | | | | - | 140 | | | | |
| TOTAL VOLUMES : | NL 4 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 12 | O G | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 16 |
| APPROACH %'s : PEAK HR : | 100.00% | 0.00% 07:30 AM - | 0.00% | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.375 75 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.375 |
| | | NODTI | POLIND | | | COLIT | IDOLIND | | I | | | | | WEC | POLIND | | |
| NOON | 1 | NORTHI 0 | 0 | 0 | 0 | 0 | HBOUND 0 | 0 | 0 | EASTE 0 | 1 | 0 | 0 | 0 | BOUND 0 | 0 | |
| 10:00 AM | NL 4 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 4 |
| 10:15 AM | 3 | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 10:30 AM 10:45 AM | 2 | 0 0 | 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 1 | 0 0 | 0 | 0 | 0 0 | 0 | 3 1 |
| 11:00 AM 11:15 AM | 1 1 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 3 2 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | ō | 0 | 0 | Ō | 0 | 1 |
| 11:45 AM 12:00 PM | 0 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM 12:30 PM | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 |
| 12:45 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | 1 |
| 1:00 PM 1:15 PM | 2 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 0 | 0 | 2 |
| 1:30 PM 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 2 |
| 1.15111 | · | | | | | | | | | | | | | | | | |
| TOTAL VOLUMES : | NL 16 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 8 | O G | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 24 |
| APPROACH %'s : PEAK HR : | 100.00% | 0.00% 12:45 PM - | 0.00% 01:45 PM | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | TOTAL |
| PEAK HR VOL : | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| PEAK HR FACTOR : | 0.375 | 0.000 | 0.000 75 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.375 |
| | | NORTHI | BOLIND | | | SOLIT | HBOUND | | | EASTE | OLIND | | | WES | BOUND | | |
| PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | TOTAL |
| 2:00 PM | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 0 |
| 2:15 PM 2:30 PM | 0 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 1 | 0 | 0 | 0 | 0 | 0 | 0 2 |
| 2:45 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 |
| 3:00 PM 3:15 PM | 0 1 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 1 3 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 1 4 |
| 3:30 PM 3:45 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 4:00 PM | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| 4:15 PM 4:30 PM | 1 1 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 2 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 3 1 |
| 4:45 PM 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM 5:45 PM | 0 2 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 1 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 26 |
| APPROACH %'s: PEAK HR: | | 0.00% 03:15 PM - | 0.00% 04:15 PM | 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 5 0.625 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 7 0.583 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 12 |
| FEAR HR FACTOR: | 0.023 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 |
| | | | | | | | | | | | | | | | | | |

Location: Rd 76 & Ave 308/W Ferguson Ave City: Visalia Control: No Control

Data - Bikes

| NS/EW Streets: | | | 1 76 | | | | 76 | | A | ve 308/W F | erguson Av | e | A | ve 308/W F | erguson Av | ve | |
|-----------------------------------|------------|------------|-------------|------------|------------|------------|-------------|------------|------------|------------|--------------|------------|------------|------------|------------|------------|------------|
| A B.4 | 1 | NORTI 0 | HBOUND 0 | 0 | 0 | | HBOUND 0 | 0 | 0 | EASTE 0 | BOUND | 0 | 0 | WEST 0 | BOUND 0 | 0 | |
| AM | NL | NT | NR | NU | SL | 0 ST | SR | SU | EL | ET | 1 ER | EU | WL | WT | WR | WU | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM 7:15 AM | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 |
| 7:15 AM 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 |
| 8:30 AM | Ō | Ō | 0 | 0 | 0 | Ö | 0 | 0 | Ō | 0 | 0 | Ō | 0 | 0 | Ō | 0 | 0 |
| 8:45 AM 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | Ō | Ö | 0 | Ö | Ö | Ö | 0 | 0 | 0 | 0 | Ō | 0 | Ō | 0 | Ō | Ö | Ö |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | U | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | U | 0 | 0 | 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | | | - 08:30 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 |
| 1 EARTH TAGTOR | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | NORTI | HBOUND | | | SOUT | HBOUND | | | EASTF | BOUND | | | WEST | BOUND | | |
| NOON | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | |
| 10:00 AM | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 0 |
| 10:15 AM | 0 | 0 | 0 | Ō | 0 | 0 | 0 | Ō | Ō | 0 | Ō | Ō | 0 | 0 | Ō | 0 | Ō |
| 10:30 AM 10:45 AM | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM 11:45 AM | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM 12:30 PM | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 |
| 12:45 PM | Ö | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM 1:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | | 12:45 PM | - 01:45 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 |
| . Zaki iki zacioki | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | NORTI | HBOUND | | l | SOUT | HBOUND | | | EASTE | BOUND | | | WEST | BOUND | | |
| PM | 1 NL | 0 NT | 0 NR | 0 NU | 0 | 0 | 0 SR | 0 | 0 | 0 | 1 ER | 0 | 0 WL | 0 WT | 0 WR | 0 WU | TOTAL |
| 2:00 PM | 0 | 0 | 0 | 0 | SL 0 | ST 0 | 0 | SU 0 | EL 0 | ET 0 | 0 | EU 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM 3:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | Ö | Ō | Ō | 0 | Ō | Ō | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | Ō | 0 |
| 5:00 PM 5:15 PM | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 1 | 0 | 0 | 0 | 0 | 0 0 | 0 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0.00% | 0 0.00% | 1 100.00% | 0 0.00% | 0 | 0 | 0 | 0 | 1 |
| PEAK HR : | | | - 04:15 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | | | | | | | | | | | | | | | | |

Location: Rd 76 & Ave 308/W Ferguson Ave **City:** Visalia

Project ID: 22-090052-001 **Date:** 4/21/2022

Data - Pedestrians (Crosswalks)

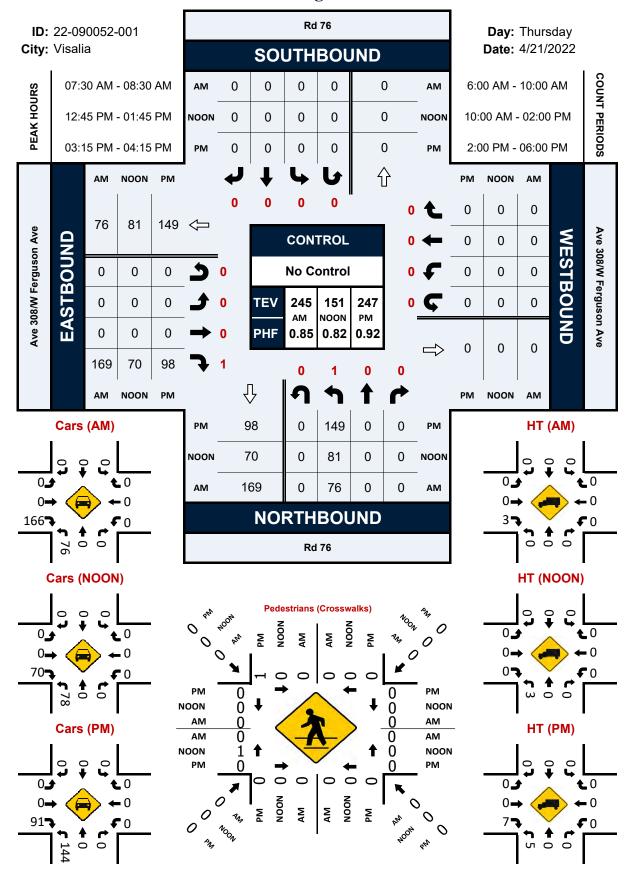
| NS/EW Streets: | Rd | 76 | Rd | l 76 | Ave 308/W F | erguson Ave | Ave 308/W F | erguson Ave | |
|-----------------------------------|----------|------------|------|--------|-------------|-------------|-------------|-------------|-------|
| A B A | NORT | 'H LEG | SOUT | 'H LEG | EAST | LEG | WEST | T LEG | |
| AM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR: | 07:30 AM | - 08:30 AM | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |

| NOON | NOR | TH LEG | SOUT | 'H LEG | FAST | Γ LEG | WEST | T I FG | |
|------------------|----------|------------|-------|--------|------|-------|--------------|--------|-------|
| NOON | EB | WB | EB EB | WB | NB | SB | NB | SB | TOTAL |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 1 | 4 |
| APPROACH %'s: | 0.00% | 100.00% | | | | | 66.67% | 33.33% | |
| PEAK HR: | 12:45 PM | - 01:45 PM | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| PEAK HR FACTOR : | | | | | | | 0.250 0.2 | 250 | 0.250 |

| D0.4 | NORT | 'H LEG | SOUT | 'H LEG | EAS | T LEG | WEST | Γ LEG | |
|-----------------|----------|------------|------|--------|-----|-------|------|-------|-------|
| PM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 2:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| APPROACH %'s: | 50.00% | 50.00% | | | | | | | |
| PEAK HR: | 03:15 PM | - 04:15 PM | | | | • | | • | TOTAL |
| PEAK HR VOL : | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| PEAK HR FACTOR: | 0.250 | | | | | | | | 0.250 |
| | 0.2 | 250 | | | | | | | 0.250 |

Rd 76 & Ave 308/W Ferguson Ave

Peak Hour Turning Movement Count



Location: Rd 76/N American St & W Goshen Ave

| City: | Visalia 2-Way Stop | (NB/SB) | | | | | | | | | | | Pr | oject ID: 2 | 2-090052- 2/21/2022 | 002 | |
|-----------------------------------|-----------------------|----------------------|---------------|------------|---------------|--------------|-------------|------------|-------------|---------------|-------------|------------|--------------|---------------|------------------------|------------|---------------|
| | ,, | (| | | | | | Data - | Total | | | | | | ,, | | |
| NS/EW Streets: | | Rd 76/N An | nerican St | | | Rd 76/N Am | | | | W Goshe | n Ave | | | W Goshe | n Ave | | |
| AM | 0 | NORTH 1 | BOUND 0 | 0 | 0 | SOUTH! | BOUND 0 | 0 | 1 | EASTB0 | OUND 0 | 0 | 1 | WESTB 2 | OUND 0 | 0 | |
| 6:00 AM | NL 5 | NT 3 | NR 6 | NU 0 | SL 9 | ST 3 | SR 0 | SU 0 | EL 0 | ET 39 | ER 1 | EU 0 | WL 23 | WT 30 | WR 10 | WU 0 | TOTAL 129 |
| 6:15 AM | 4 | 0 | 10 | 0 | 14 | 3 | 0 | 0 | 1 | 23 | 1 | 0 | 9 | 23 | 10 9 | 0 | 98 |
| 6:30 AM 6:45 AM | 4 3 | 3 3 | 17 9 | 0 0 | 25 23 | 8 8 | 0 2 | 0 | 2 | 12 23 | 1 5 | 0 0 | 13 | 24 48 | 16 | 0 0 | 112 155 |
| 7:00 AM 7:15 AM | 4 2 | 5 0 | 6 6 | 0 | 13 34 | 1 4 | 0 | 0 0 | 0 | 26 28 | 1 2 | 0 | 8 6 | 23 32 | 13 9 | 0 0 | 100 123 |
| 7:30 AM 7:45 AM | 2 2 | 0 | 5 6 | 0 | 62 65 | 8 6 | 0 | 0 | 1 0 | 24 38 | 4 5 | 0 | 14 9 | 30 42 | 11 5 | 0 | 161 181 |
| 8:00 AM 8:15 AM | 1 3 | 1 3 | 3 4 | 0 | 42 17 | 4 0 | 0 | 0 | 0 | 27 24 | 3 2 | 0 | 6 7 | 41 40 | 29 43 | 0 | 157 143 |
| 8:30 AM | 2 | 3 | 11 | 0 | 17 | 7 2 | 0 | 0 | 1 | 22 | 2 2 | 0 | 6 9 | 19 32 | 22 | 0 | 112 111 |
| 8:45 AM 9:00 AM | 2 | 3 | 6 | 0 | 18 23 | 3 | 1 | 0 | 0 | 16 29 | 1 | 0 | 17 | 20 | 15 9 | 0 | 114 |
| 9:15 AM 9:30 AM | 1 0 | 2 4 | 20 11 | 0 0 | 19 16 | 8 | 0 0 | 0 0 | 0 | 14 19 | 0 5 | 0 0 | 14 12 | 15 21 | 18 8 | 0 | 113 99 |
| 9:45 AM | 2 | 2 | 10 | 0 | 16 | 6 | 1 | 0 | 1 | 23 | 1 | 0 | 6 | 17 | 20 | 0 | 105 |
| TOTAL VOLUMES : | NL 37 | NT 36 | NR 144 | NU 0 | SL 413 | ST 74 | SR 4 | SU 1 | EL 9 | ET 387 | ER 36 | EU 0 | WL 168 | WT 457 | WR 247 | WU 0 | TOTAL 2013 |
| APPROACH %'s: PEAK HR: | 17.05% | 16.59% 07:30 AM - | 66.36% | 0.00% | 83.94% | 15.04% | 0.81% | 0.20% | 2.08% | 89.58% | 8.33% | 0.00% | 19.27% | 52.41% | 28.33% | 0.00% | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 8 0.667 | 6 0.500 | 18 0.750 | 0 0.000 | 186 0.715 | 18 0.563 | 0 0.000 | 1 0.250 | 1 0.250 | 113 0.743 | 14 0.700 | 0 0.000 | 36 0.643 | 153 0.911 | 88 0.512 | 0 0.000 | 642 |
| PEAR IIR PACTOR . | 0.007 | 0.80 | | 0.000 | 0.713 | 0.505 | | 0.230 | 0.230 | 0.743 | | 0.000 | 0.043 | 0.76 | | 0.000 | 0.887 |
| NOON | 0 | NORTH | BOUND 0 | 0 | 0 | SOUTH | | 0 | 1 | EASTB0 | | 0 | 1 | WESTE | | 0 | |
| NOON | NL | 1 NT | NR | NU | SL | ST ST | 0 SR | SU | EL | ET | 0 ER | EU | WL | WT | 0 WR | WU | TOTAL |
| 10:00 AM 10:15 AM | 1 3 | 3 4 | 10 4 | 0 0 | 18 17 | 4 6 | 1 0 | 0 0 | 1 2 | 28 25 | 0 2 | 0 0 | 7 5 | 25 28 | 10 13 | 0 | 108 109 |
| 10:30 AM 10:45 AM | 1 2 | 2 1 | 10 14 | 0 | 18 29 | 3 3 | 2 1 | 0 | 1 0 | 31 29 | 2 | 1 0 | 9 6 | 29 27 | 17 15 | 0 | 126 130 |
| 11:00 AM 11:15 AM | 4 2 | 5 3 | 15 16 | 0 | 16 21 | 7 2 | 1 0 | 0 | 0 3 | 33 25 | 4 5 | 0 | 10 9 | 31 26 | 21 19 | 0 | 147 131 |
| 11:30 AM 11:45 AM | 8 | 1 2 | 20 12 | 0 | 14 19 | 6 | 0 | 0 | 2 | 29 35 | 2 | 0 | 10 16 | 29 32 | 16 20 | 1 | 138 152 |
| 12:00 PM 12:15 PM | 2 | 4 0 | 26 12 | 0 | 17 21 | 1 2 | 2 | 0 | 1 0 | 41 45 | 6 | 0 | 16 15 | 32 42 | 13 23 | 0 | 161 164 |
| 12:30 PM | 7 | 3 | 11 | 0 | 21 23 | 5 | 0 | 0 | 0 | 49 | 3 2 | 0 | 8 | 27 29 | 24 | 0 | 158 |
| 12:45 PM 1:00 PM | 1 | 4 | 10 6 | 0 | 16 | 2 | 1 | 0 | 1 | 24 | 2 | 0 | 3 | 30 | 19 18 | 0 | 135 106 |
| 1:15 PM 1:30 PM | 3 4 | 3 2 | 7 6 | 0 | 15 25 | 3 4 | 1 0 | 0 0 | 0 | 31 29 | 1 4 | 0 0 | 8 8 | 28 28 | 20 29 | 0 | 120 139 |
| 1:45 PM | 5 | 3 | 13 | 0 | 27 | 2 | 0 | 0 | 1 | 27 | 1 | 0 | 14 | 31 | 15 | 0 | 139 |
| TOTAL VOLUMES : | NL 57 | NT 45 | NR 192 | NU 0 | SL 317 | ST 55 | SR 11 | SU 0 | EL 15 | ET 503 | ER 42 | EU 1 | WL 158 | WT 474 | WR 292 | WU 1 | TOTAL 2163 |
| APPROACH %'s: PEAK HR: | | 15.31% L1:45 AM - | | 0.00% | 82.77% | 14.36% | 2.87% | 0.00% | 2.67% | 89.66% | 7.49% | 0.18% | 17.08% | 51.24% | 31.57% | 0.11% | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 19 0.679 | 9 0.563 | 61 0.587 | 0 0.000 | 78 0.929 | 10 0.500 | 3 0.375 | 0 0.000 | 3 0.375 | 170 0.867 | 14 0.583 | 0.000 | 55 0.859 | 133 0.792 | 80 0.833 | 0 0.000 | 635 0.968 |
| | | 0.69 | | | | 0.87 | | | | 0.89 | | | | 0.83 | | | 0.500 |
| PM | 0 | NORTH 1 | 0 | 0 | 0 | SOUTH! | 0 | 0 | 1 | EASTB0 2 | 0 | 0 | 1 | WESTB 2 | 0 | 0 | |
| 2:00 PM | NL 4 | NT 5 | NR 8 | NU 0 | SL 23 | ST 9 | SR 0 | SU 0 | EL 2 | ET 38 | ER 2 | EU 0 | WL 6 | WT 36 | WR 30 | WU 0 | TOTAL 163 |
| 2:15 PM 2:30 PM | 2 | 5 4 | 16 21 | 0 0 | 28 38 | 4 6 | 0 1 | 0 0 | 1 2 | 33 75 | 4 6 | 0 0 | 11 5 | 33 23 | 47 20 | 0 0 | 184 204 |
| 2:45 PM 3:00 PM | 5 2 | 2 8 | 16 13 | 0 | 27 26 | 12 0 | 0 | 0 | 0 | 27 47 | 2 | 0 | 7 13 | 28 25 | 34 31 | 0 | 162 167 |
| 3:15 PM 3:30 PM | 5 | 8 | 21 22 | 0 | 16 26 | 7 5 | 2 | 0 | 0 | 37 47 | 6 | 0 | 11 6 | 34 42 | 31 46 | 0 | 178 212 |
| 3:45 PM | 3 | 6 | 17 | 0 | 21 | 5 | 1 | 0 | 2 | 26 | 3 | 0 | 10 7 | 32 | 40 | 0 | 166 |
| 4:00 PM 4:15 PM | 4 7 | 6 5 | 23 17 | 0 | 46 30 | 10 6 | 3 | 0 | 2 | 53 40 | 5 | 0 | 2 | 29 33 | 30 36 | 0 | 215 182 |
| 4:30 PM 4:45 PM | 2 2 | 3 4 | 16 16 | 0 0 | 24 27 | 4 7 | 1 2 | 0 0 | 2 2 | 86 36 | 6 3 | 0 0 | 5 8 | 32 28 | 35 35 | 0 0 | 216 170 |
| 5:00 PM 5:15 PM | 2 1 | 2 5 | 30 11 | 0 | 27 20 | 3 2 | 0 | 0 0 | 4 0 | 52 34 | 3 0 | 0 | 7 7 | 30 19 | 39 42 | 0 0 | 199 141 |
| 5:30 PM 5:45 PM | 0 1 | 1 3 | 11 2 | 0 | 33 23 | 8 1 | 0 | 0 | 1 | 23 30 | 0 | 0 | 3 4 | 26 16 | 38 19 | 0 | 144 100 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | | 76 19.84% | 260 67.89% | 0.00% | 435 81.16% | 89 16.60% | 12 2.24% | 0 0.00% | 20 2.66% | 684 90.84% | 49 6.51% | 0 0.00% | 112 9.90% | 466 41.20% | 553 48.89% | 0 0.00% | 2803 |
| PEAK HR : | | 04:00 PM - | | 0.0070 | 127 | 27 | 7 | 0.0070 | 7 | 215 | 15 | 0.0070 | 22 | 122 | 136 | 0.0070 | TOTAL 783 |
| PEAK HR VOL : PEAK HR FACTOR : | | 0.750 | 0.783 | 0.000 | 0.690 | 0.675 | 0.583 | 0.000 | 0.875 | 0.625 | 0.625 | 0.000 | 0.688 | 0.924 | 0.944 | 0.000 | 0.906 |
| | | 0.79 | 73 | | | 0.70 | JU | | | 0.63 | U | | | 0.97 | 2 | | |

Location: Rd 76/N American St & W Goshen Ave

| PEAK HR 1: 07:30 AM - 08:30 AM - PEAK HR FACTOR: 0.500 0.500 0.600 0.0000 0.0000 0.0000 0.000 0.00000 0.00000 0.00000 0.00000 0.00000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000 0.000 | City: | Visalia 2-Way Stop | | | | | | | | | | | | Pr | oject ID: 1 Date: 4 | 22-090052- 4/21/2022 | 002 | |
|--|------------------|-----------------------|------------|----------|-------|--------|------------|---------|--------|-------|--------|-------|-------|--------|------------------------|-------------------------|------------|---------------|
| AM O | | | D. 17601.4 | | | | D. 17671.4 | | Data - | Cars | | | | | | | | |
| AMD | NS/EW Streets: | | | | | | | | | | | | | | | | | |
| SIGN AN | AM | | 1 | 0 | | | 1 | 0 | | | 2 | 0 | | | 2 | 0 | | |
| 6:15 AM | 6:00 AM | | | | | | | | | | | | | | | | | TOTAL 111 |
| C-SS AN 3 3 6 0 22 8 2 0 2 138 4 0 0 11 144 15 15 0 17 17 10 10 18 18 10 17 10 10 18 18 10 17 10 10 18 18 10 18 10 18 18 | 6:15 AM | 3 | 0 | 4 | 0 | 14 | 3 | 0 | 0 | 1 | 21 | 1 | 0 | 8 | 19 | 10 | 0 | 84 92 |
| 7:15 AM 1 0 6 0 0 33 4 0 0 0 0 25 2 2 0 6 31 9 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0 7 0 | 6:45 AM | 3 | 3 | 6 | 0 | 21 | 8 | 2 | 0 | 2 | 18 | 4 | 0 | 11 | 44 | 15 | 0 | 137 |
| 7-730-AM | | | | | | | | | | | | | | | | | | 84 117 |
| SCO AN 1 | 7:30 AM | 1 | 0 | 5 | 0 | 60 | 8 | 0 | 0 | 1 | 20 | 4 | 0 | 14 | 26 | 11 | 0 | 150 |
| September Sept | 8:00 AM | 1 | 1 | 3 | 0 | 41 | 4 | 0 | 0 | 0 | 22 | 3 | 0 | 4 | 33 | 29 | 0 | 160 141 |
| 8-85 AM 0 2 2 12 0 166 2 0 0 0 1 1 13 2 2 0 8 24 15 0 0 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 | | | | | | | | | | | | | | | | | | 130 95 |
| 9-15 AM | 8:45 AM | 0 | 2 | 12 | 0 | 16 | 2 | 0 | 0 | 1 | 13 | 2 | 0 | 8 | 24 | 15 | 0 | 95 97 |
| 9-45 AM 2 2 2 6 6 0 155 5 1 0 1 17 1 0 5 13 19 0 1 TOTAL VOLUMES No. IN IT NR NR NR NR NR NR NR N | 9:15 AM | 1 | 2 | 14 | 0 | 17 | 8 | 0 | 0 | 2 | 10 | 0 | 0 | 10 | 12 | 18 | 0 | 94 |
| TOTAL VOLUMES, APPORACH 91. NL | | | | | | | | | | | | | | 7 5 | | | | 82 87 |
| TOTAL VOLUMES A 30 | | | | | | | | | | | | | | | | | | |
| PEAK HR: 07:39 AM - 08:30 AM - 0.50 | | 30 | 34 | 89 | 0 | 395 | 71 | 3 | 1 | 9 | 319 | 30 | 0 | 141 | 396 | 238 | 0 | TOTAL 1756 |
| PEAK HR VOL. 6 | | | | | 0.00% | 84.04% | 15.11% | 0.64% | 0.21% | 2.51% | 89.11% | 8.38% | 0.00% | 18.19% | 51.10% | 30.71% | 0.00% | TOTAL |
| NOON NORTHBOUND NORTHBOUND NORTHBOUND NOTHBOUND NORTHBOUND | PEAK HR VOL : | 6 | 6 | 12 | | | | | | | | | | | | | | 581 |
| NOON | PEAK HR FACTOR : | 0.500 | | | 0.000 | 0./34 | | | 0.250 | 0.250 | | | 0.000 | 0.5/1 | | | 0.000 | 0.908 |
| NOON | | | NORTH | BOLIND | | | SOUTH | IBOLIND | | | FASTR | OLIND | | | WESTE | SOLIND | | |
| 10:00 AM | NOON | | 1 | 0 | | | 1 | 0 | | | 2 | 0 | | | 2 | 0 | | TOTAL |
| 10:30 AM | | 1 | | | | 18 | 4 | | | | 23 | | | 7 | | | | TOTAL 95 |
| 10-05 AM | | | | | | | | | | | | | | | | | | 87 93 |
| 11:15 AM | 10:45 AM | 2 | 1 | 11 | 0 | 28 | 3 | 1 | 0 | 0 | 21 | 3 | 0 | 5 | 19 | 14 | 0 | 108 |
| 11-45 AM | 11:15 AM | 1 | 3 | | 0 | 19 | 2 | 0 | | 3 | 21 | | | 6 | 23 | | 0 | 127 110 |
| 12:00 PM | | | | | | | | | | | | | | | | | | 117 131 |
| 12:30 PM | 12:00 PM | 1 | 4 | 23 | 0 | 17 | 1 | 2 | 0 | 1 | 38 | | 0 | 15 | 29 | 13 | 0 | 148 |
| 1:00 PM | 12:30 PM | | 3 | 9 | | 21 | 5 | | | | 43 | 3 | | 7 | 23 | 24 | 0 | 147 144 |
| 1:15 PM 3 | | • | | | | | | | | | | | | | | | | 118 87 |
| TOTAL VOLUMES: N.L. N.T. N.R. N.U. S.L. S.T. S.R. S.U. EL. ET. ER. EU. W.L. W.T. W.R. W.U. W.T. W | 1:15 PM | | 3 | 6 | 0 | 15 | 3 | 1 | 0 | | 25 | 1 | 0 | 5 | 22 | 19 | 0 | 103 |
| TOTAL VOLUMES: 49 | | | | | | | | | | | | | | | | | | 121 118 |
| PEAK HR VOL: PEAK HR VOL: PEAK HR FACTOR: 1.1:45 MH - 1.2:45 PM 1.1 | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| PEAK HR VOL: PEAK HR VOL: 0.583 | | | | | | | | | | | | | | | | 273 34.82% | 0 0.00% | 1854 |
| PIV | PEAK HR : | | 11:45 AM - | 12:45 PM | | | | | | | | | | | | | | TOTAL |
| PM O | | | | | | | | | | | | | | | | | | 570 |
| PW NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU | | | 0.6 | 79 | ' | | 0.8 | 65 | | | 0.87 | 0 | | | 0.8 | 36 | | 0.963 |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU 2:00 PM | DNA | 0 | | | 0 | 0 | | | 0 | | | | 0 | | | | 0 | |
| 2:15 PM | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 2:30 PM | | | | | | | | | | | | | | | | | | 143 164 |
| 3:00 PM 2 8 12 0 24 0 0 0 0 44 1 0 9 17 28 0 3:15 PM 5 8 17 0 15 7 1 0 0 33 2 0 9 27 31 0 3:30 PM 3 9 20 0 25 5 1 0 0 43 4 0 4 35 45 0 3:45 PM 1 4 16 0 21 5 1 0 0 2 23 1 0 7 26 38 0 4:00 PM 4 5 18 0 46 10 1 0 1 5 0 3 0 6 21 28 0 4:15 PM 6 5 14 0 28 6 3 0 0 2 34 1 0 7 26 38 0 4:15 PM 6 5 14 0 28 6 3 0 0 2 34 1 0 2 29 33 0 4:30 PM 2 3 15 0 24 4 1 0 2 2 34 1 0 2 2 29 33 0 4:30 PM 2 3 15 0 24 4 1 0 2 79 4 0 4 31 34 0 0 4 435 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 2:30 PM | 1 | 4 | 19 | 0 | 37 | 6 | 1 | | 2 | 69 | 5 | | 2 | 18 | 19 | 0 | 183 143 |
| 3:30 PM 3 9 20 0 25 5 1 0 0 43 4 0 4 35 45 0 3:45 PM 1 4 16 0 21 5 1 0 2 23 1 0 7 26 38 0 4:00 PM 4 5 18 0 46 10 1 0 1 50 3 0 6 21 28 0 4:15 PM 6 5 14 0 28 6 3 0 2 34 1 0 2 2 29 33 0 4:30 PM 2 3 15 0 24 4 1 0 2 2 79 4 0 4 31 34 0 4:45 PM 1 4 14 0 25 7 2 0 2 34 1 0 2 2 29 33 0 4:45 PM 1 4 14 0 25 7 2 0 2 34 3 0 6 26 35 0 5:00 PM 2 2 2 29 0 27 3 0 0 3 49 3 0 6 26 35 0 5:00 PM 1 5 10 0 20 2 0 0 0 3 49 3 0 3 27 39 0 5:15 PM 1 5 10 0 20 2 0 0 0 0 32 0 0 3 17 42 0 5:30 PM 0 1 1 10 0 33 7 0 0 0 1 22 0 0 0 3 17 42 0 5:30 PM 0 1 1 10 0 33 7 0 0 0 1 22 0 0 0 0 2 24 38 0 5:45 PM 1 2 2 2 0 0 22 1 0 0 0 1 22 16 19 0 TOTAL VOLUMES: 36 72 230 0 423 88 11 0 19 625 35 0 79 390 535 0 APPROACH %'s: 10.65% 21.30% 68.05% 0.00% 81.03% 16.86% 2.11% 0.00% 2.80% 92.05% 5.15% 0.00% 7.87% 38.84% 53.29% 0.00 | 3:00 PM | 2 | 8 | 12 | 0 | 24 | 0 | 0 | 0 | 0 | 44 | 1 | 0 | 9 | 17 | 28 | 0 | 145 |
| 3:45 PM | 3:30 PM | | | | 0 | | | | | | 43 | | | | | | 0 | 155 194 |
| 4:15 PM 6 5 14 0 28 6 3 0 2 34 1 0 2 29 33 0 4:30 PM 2 3 15 0 24 4 1 0 2 79 4 0 4 31 34 0 4:45 PM 1 4 14 0 25 7 2 0 2 34 3 0 6 26 35 0 5:00 PM 2 2 29 0 27 3 0 0 3 49 3 0 3 27 39 0 5:15 PM 1 5 10 0 20 2 0 0 0 32 0 0 3 17 42 0 5:30 PM 0 1 10 0 33 7 0 0 1 22 0 0 2 24 38 0 5:45 PM 1 2 2 0 22 | 3:45 PM | 1 | | 16 | 0 | 21 | 5 | | | | 23 | 1 | | 7 | 26 | 38 | 0 | 145 193 |
| 4:45 PM | 4:15 PM | 6 | 5 | 14 | 0 | 28 | 6 | 3 | 0 | 2 | 34 | 1 | 0 | 2 | 29 | 33 | 0 | 163 |
| 5:00 PM 2 2 2 29 0 27 3 0 0 3 49 3 0 3 27 39 0 5:15 PM 1 5 10 0 20 2 0 0 0 0 32 0 0 0 3 17 42 0 5:30 PM 0 1 10 0 33 7 0 0 1 1 22 0 0 0 2 24 38 0 5:45 PM 1 2 2 2 0 22 1 0 0 0 1 30 0 0 2 24 38 0 0 5:45 PM 1 2 2 2 0 5 22 1 0 0 0 1 30 0 0 0 2 16 19 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 1 1 0 0 0 0 1 1 0 | 4:45 PM | 1 | 4 | 14 | 0 | 25 | 7 | 2 | 0 | 2 | 34 | 3 | 0 | | 26 | 35 | 0 | 203 159 |
| 5:30 PM 0 1 10 0 33 7 0 0 1 122 0 0 2 24 38 0 5:45 PM 1 2 2 0 0 22 1 0 0 0 1 30 0 0 2 24 38 0 TOTAL YOLUMES: 36 72 230 0 423 88 11 0 19 625 35 0 79 390 535 0 APPROACH 96's: 10.65% 21.30% 68.05% 0.00% 81.03% 16.86% 2.11% 0.00% 2.80% 92.05% 5.15% 0.00% 7.87% 38.84% 53.29% 0.00 | | | | | | | | | | | | | | | | | | 187 132 |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TOTAL VOLUMES: 36 72 230 0 423 88 11 0 19 625 35 0 79 390 535 0 APPROACH %'s: 10.65% 21.30% 68.05% 0.00% 81.03% 16.86% 2.11% 0.00% 2.80% 92.05% 5.15% 0.00% 7.87% 38.84% 53.29% 0.00 | 5:30 PM | 0 | 1 | 10 | 0 | 33 | 7 | 0 | 0 | 1 | 22 | 0 | Ō | 2 | 24 | 38 | 0 | 138 |
| TOTAL VOLUMES: 36 72 230 0 423 88 11 0 19 625 35 0 79 390 535 0 APPROACH %'s: 10.65% 21.30% 68.05% 0.00% 81.03% 16.86% 2.11% 0.00% 2.80% 92.05% 5.15% 0.00% 7.87% 38.84% 53.29% 0.00 | 5:45 PM | | | | | | | | | | | | | | | | | 96 |
| APPROACH %'s: 10.65% 21.30% 68.05% 0.00% 81.03% 16.86% 2.11% 0.00% 2.80% 92.05% 5.15% 0.00% 7.87% 38.84% 53.29% 0.00 | TOTAL VOLUMES : | | | | | | | | | | | | | | | | | TOTAL 2543 |
| | APPROACH %'s: | 10.65% | 21.30% | 68.05% | | | | | | | | | | | | 53.29% | 0.00% | |
| PEAK HR: 04:00 PM - 05:00 PM 05:00 PM PEAK HR VOL: 13 17 61 0 123 27 7 0 7 197 11 0 18 107 130 0 | PEAK HR VOL : | 13 | 17 | 61 | | | | | | | | | | | | | | TOTAL 718 |
| PEAK HR FACTOR: 0.542 0.850 0.847 0.000 0.668 0.675 0.583 0.000 0.875 0.623 0.688 0.000 0.750 0.863 0.929 0.000 0.632 0.632 0.924 | PEAK HR FACTOR : | 0.542 | | | 0.000 | 0.668 | | | 0.000 | 0.875 | | | 0.000 | 0.750 | | | 0.000 | 0.884 |
| 0.000 0.002 0.921 | | | 0.0 | | | | 0.0 | | | | 0.02 | | | | 0.3. | , | | |

${\tt National\ Data\ \&\ Surveying\ Services} \\ Intersection\ Turning\ Movement\ Count$

Location: Rd 76/N American St & W Goshen Ave City: Visalia Control: 2-Way Stop(NB/SB)

| Control: | 2-Way Stop | (NB/SB) | | | | | | Data | - HT | | | | | Date: 4 | 1/21/2022 | | |
|-----------------------------------|------------|-----------------------|-------------|------------|------------|------------|------------|------------|------------|-------------|------------|------------|------------|-------------|------------|------------|--------------|
| NS/EW Streets: | | Rd 76/N Am | erican St | | | Rd 76/N Am | nerican St | Jutu | | W Goshe | n Ave | | | W Goshe | en Ave | | |
| | | NORTHE | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | 0 | 1 NT | 0 ND | 0 | 0 | 1 CT | 0 CD | 0 | 1 EL | 2 | 0 ED | 0 EU | 1 WL | 2 WT | 0 M/D | 0 WU | TOTAL |
| 6:00 AM | NL 1 | 1 | NR 4 | NU 0 | SL 1 | ST 0 | SR 0 | SU 0 | EL | ET | ER 0 | 0 | 5 5 | 1 | WR 1 | 0 | 18 18 |
| 6:15 AM | 1 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | Ō | 2 | 0 | 0 | 1 | 4 | 0 | 0 | 14 |
| 6:30 AM | 0 | 0 | 13 | 0 | 2 | 2 0 | 0 | 0 | 0 | 1 5 | 1 | 0 | 1 2 | 0 | 0 | 0 | 20 |
| 6:45 AM 7:00 AM | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 1 | 4 | 5 | 0 | 18 16 |
| 7:15 AM | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 6 |
| 7:30 AM 7:45 AM | 1 | 0 | 0 4 | 0 | 2 4 | 0 | 0 | 0 | 0 | 4 8 | 0 | 0 | 0 | 4 | 0 | 0 | 11 21 |
| 8:00 AM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 2 | 8 | 0 | 0 | 16 |
| 8:15 AM | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 2 | 4 | 0 | 0 | 13 |
| 8:30 AM 8:45 AM | 0 | 0 | 6 | 0 | 0 2 | 0 | 0 | 0 | 0 | 5 3 | 1 0 | 0 | 1 | 4 8 | 0 | 0 | 17 16 |
| 9:00 AM | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 9 | 0 | 0 | 1 | 5 | 0 | 0 | 17 |
| 9:15 AM | 0 | 0 | 6 | 0 | 2 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 5 | 3 | 0 | 0 | 19 17 |
| 9:30 AM 9:45 AM | 0 | 1 0 | 2 4 | 0 | 1 | 1 | 0 | 0 | 0 | 2 6 | 1 0 | 0 | 1 | 5 4 | 1 | 0 | 18 |
| | - | | | | | | | | | | | | | | | | |
| TOTAL VOLUMES : | NL 7 | NT 2 | NR 55 | O NN | SL 18 | ST 3 | SR 1 | SU 0 | EL 0 | ET 68 | ER 6 | EU O | WL 27 | WT 61 | WR 9 | O OM | TOTAL 257 |
| APPROACH %'s: | 10.94% | 3.13% | 85.94% | 0.00% | 81.82% | 13.64% | 4.55% | 0.00% | 0.00% | 91.89% | 8.11% | 0.00% | 27.84% | 62.89% | 9.28% | 0.00% | 237 |
| PEAK HR : | | 07:30 AM - (| | | _ | | • | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 2 0.500 | 0 0.000 | 6 0.375 | 0 0.000 | 7 0.438 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 22 0.688 | 2 0.250 | 0 0.000 | 4 0.500 | 18 0.563 | 0 0.000 | 0 0.000 | 61 |
| | | 0.40 | | | | 0.43 | | | | 0.60 | | | | 0.55 | | | 0.726 |
| | | NORTHE | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| NOON | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| 10:00 AM | NL 0 | NT 2 | NR 1 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL | ET 5 | ER 0 | EU 0 | WL 0 | WT 5 | WR 0 | WU 0 | TOTAL 13 |
| 10:15 AM | ő | 1 | î | 0 | Ö | 1 | Ö | 0 | Ö | 5 | 2 | 0 | 1 | 9 | 2 | Ö | 22 |
| 10:30 AM 10:45 AM | 0 | 0 | 4 | 0 | 1 1 | 1 0 | 0 | 0 | 0 | 9 8 | 2 | 1 0 | 8 1 | 5 8 | 2 | 0 | 33 22 |
| 11:00 AM | 0 | 0 | 5 | 0 | 2 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 5 | 2 | 0 | 20 |
| 11:15 AM | 1 | 0 | 5 | 0 | 2 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 3 | 3 | 2 | 0 | 21 |
| 11:30 AM 11:45 AM | 1 | 0 | 4 | 0 | 2 0 | 0 | 0 | 0 | 0 1 | 5 6 | 1 0 | 0 | 5 1 | 2 5 | 0 | 1 0 | 21 21 |
| 12:00 PM | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | î | 3 | 0 | 0 | 13 |
| 12:15 PM 12:30 PM | 0 1 | 0 | 0 2 | 0 | 1 0 | 0 | 0 | 0 | 0 | 9 6 | 0 0 | 0 | 0 1 | 5 4 | 2 0 | 0 | 17 14 |
| 12:45 PM | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 4 | 4 | 1 | 0 | 17 |
| 1:00 PM | 0 | 0 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 6 | 0 | 0 | 1 | 5 | 3 | 0 | 19 |
| 1:15 PM 1:30 PM | 0 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 6 4 | 0 2 | 0 | 3 2 | 6 8 | 1 0 | 0 | 17 18 |
| 1:45 PM | Ō | 0 | 3 | Ō | 2 | Ō | Ō | Ō | Ō | 2 | 0 | Ō | 6 | 7 | 1 | Ō | 21 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 8 | 3 | 41 | 0 | 13 | 2 | 1 | 0 | 1 | 86 | 12 | 1 | 37 | 84 | 19 | 1 | 309 |
| APPROACH %'s : PEAK HR : | 15.38% | 5.77% 11:45 AM - : | 78.85% | 0.00% | 81.25% | 12.50% | 6.25% | 0.00% | 1.00% | 86.00% | 12.00% | 1.00% | 26.24% | 59.57% | 13.48% | 0.71% | TOTAL |
| PEAK HR VOL : | 5 | 0 0 | 8 8 | 0 | 1 | 0 | 0 | 0 | 1 | 24 | 2 | 0 | 3 | 17 | 4 | 0 | 65 |
| PEAK HR FACTOR : | 0.417 | 0.000 | 0.667 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.250 | 0.667 | 0.250 | 0.000 | 0.750 | 0.850 | 0.500 | 0.000 | 0.774 |
| | | 0.54 | 12 | | | 0.25 | 00 | | | 0.75 | 0 | | | 0.75 | 50 | | |
| DA4 | | NORTHE | | | | SOUTHE | | • | | EASTB | | • | | WESTE | | | |
| PM | 0 NL | 1 NT | 0 NR | 0 NU | 0 SL | 1 ST | 0 SR | 0 SU | 1 EL | 2 ET | 0 ER | 0 EU | 1 WL | 2 WT | 0 WR | 0 WU | TOTAL |
| 2:00 PM | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 1 | 0 | 0 | 8 | 0 | 0 | 20 |
| 2:15 PM 2:30 PM | 1 2 | 0 | 1 2 | 0 | 0 1 | 0 | 0 | 0 | 0 0 | 3 6 | 0 1 | 0 | 4 3 | 8 5 | 3 1 | 0 | 20 21 |
| 2:45 PM | 1 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 5 | 2 | 0 | 19 |
| 3:00 PM 3:15 PM | 0 | 0 | 1 4 | 0 0 | 2 1 | 0 | 0 1 | 0 0 | 0 | 3 4 | 1 4 | 0 0 | 4 2 | 8 | 3 | 0 | 22 23 |
| 3:30 PM | 1 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 2 | 7 | 1 | 0 | 18 |
| 3:45 PM | 2 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 0 | 3 | 6 | 2 | 0 | 21 |
| 4:00 PM 4:15 PM | 0 1 | 1 0 | 5 3 | 0 | 0 2 | 0 | 0 0 | 0 | 0 | 3 6 | 2 0 | 0 0 | 1 0 | 8 4 | 2 | 0 0 | 22 19 |
| 4:30 PM | Ō | 0 | 1 | 0 | 0 | 0 | 0 | 0 | Ō | 7 | 2 | 0 | 1 | 1 | 1 | 0 | 13 |
| 4:45 PM 5:00 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 4 | 3 | 0 | 0 | 11 12 |
| 5:15 PM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 4 | 2 | 0 | 0 | 9 |
| 5:30 PM 5:45 PM | 0 | 0 1 | 1 0 | 0 | 0 1 | 1 0 | 0 | 0 | 0 0 | 1 0 | 0 0 | 0 | 1 2 | 2 0 | 0 | 0 | 6 4 |
| J.7J FM | | | | | | | | | | | | | | | | | |
| TOTAL VOLUMES : | NL 11 | NT 4 | NR 30 | NU 0 | SL 12 | ST 1 | SR 1 | SU 0 | EL 1 | ET 59 | ER 14 | EU 0 | WL 33 | WT 76 | WR 18 | WU 0 | TOTAL 260 |
| APPROACH %'s: | 24.44% | 8.89% | 66.67% | 0.00% | 85.71% | 7.14% | 7.14% | 0.00% | 1.35% | 79.73% | 18.92% | 0.00% | 25.98% | 59.84% | 14.17% | 0.00% | |
| PEAK HR : | | 04:00 PM - (| | | 4 | 0 | 0 | 0 | | | | | 4 | 15 | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 2 0.500 | 1 0.250 | 11 0.550 | 0.000 | 4 0.500 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 18 0.643 | 4 0.500 | 0 0.000 | 4 0.500 | 15 0.469 | 6 0.500 | 0.000 | 65 |
| | | 0.58 | | | , | 0.50 | | | | 0.61 | | | | 0.56 | | | 0.739 |
| | | | | | | | | | | | | | | | | | |

Location: Rd 76/N American St & W Goshen Ave City: Visalia Control: 2-Way Ston(NB/SB)

NL 0 0.00%

0.000

TOTAL VOLUMES: APPROACH %'s: PEAK HR: PEAK HR VOL: PEAK HR FACTOR:

NT 0 0.00%

0 0.000

04:00 PM - 05:00 PM

NR 1 100.00%

0.000

NU 0 0.00%

0 0.000 0.000

ST 0

0 0.000

0 0.000

SU 0

0 0.000

EL 0

0 0.000

ET 0

0 0.000

ER 0

0 0.000

EU 0

0 0.000

Project ID: 22-090052-002

WL 1 50.00%

0 0.000

WT 1 50.00%

0 0.000

WR 0 0.00%

0 0.000

0 0.000

TOTAL 3

TOTAL

| Control: | 2-Way Sto | p(NB/SB) | | | | | | Data - | Bikes | | | | | Date: | 4/21/2022 | | |
|-----------------------------------|-----------|------------|-------------|------------|------------|------------|-------------|---------|------------|------------|------------|------------|---------|-----------|------------|---------|------------|
| NS/EW Streets: | | Rd 76/N A | American St | | | Rd 76/N A | merican St | Data - | DIKES | W Goshe | en Ave | | | W Gosh | ien Ave | | |
| , | | | HBOUND | | | | HBOUND | | | EASTB | | | | | BOUND | | |
| AM | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 2 | 0 | 0 | 1 | 2 | 0 | 0 | |
| 6:00 AM | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 | ET 0 | ER 0 | EU 0 | WL 0 | WT 0 | WR 1 | WU 0 | TOTAL 1 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM 7:15 AM | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 1 0 |
| 7:30 AM | 0 | 0 | Ō | Ō | 0 | Ō | 0 | 0 | 0 | 0 | 0 | Ō | 0 | Ō | Ō | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 2 |
| APPROACH %'s : PEAK HR : | | 07:30 AM | - 08:30 AM | | | | | | 0.00% | 100.00% | 0.00% | 0.00% | 0.00% | 0.00% | 100.00% | 0.00% | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | HODE | | | | 001177 | HBOUND | | | E 1 0 E D | | | | | | | |
| NOON | 0 | 1 | HBOUND 0 | 0 | 0 | 1 | 0 HROOND | 0 | 1 | EASTB 2 | OUND 0 | 0 | 1 | WES1 2 | BOUND 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 10:00 AM 10:15 AM | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM 11:15 AM | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | Ö | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 0 | Ō | 0 | 0 | Ö | Ō | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 0 | Ō | 0 | 0 | Ō | 0 | Ō | 0 | 0 | Ō | Ō | 0 | Ō | 0 | 0 | Ō |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR : | | | - 12:45 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0.000 | 0 0.000 | 0.000 | 0 |
| . Lak intraction | 0.000 | 0.000 | 0.000 | 0.000 | 1 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | NORT | HBOUND | | | SOUTI | HBOUND | | | EASTB | OUND | | | WEST | BOUND | | |
| PM | 0 | 1 NT | 0 NR | 0 NU | 0 | 1 CT | <u>0</u> | 0 | 1 EL | 2 ET | 0 | 0 EU | 1 WL | 2 WT | 0 WR | 0 WU | TOTAL |
| 2:00 PM | NL 0 | 0 0 | 0 0 | NU | SL 0 | ST 0 | SR 0 | SU 0 | 0 0 | 0 0 | ER 0 | EU | 0 0 | 0 0 | 0 0 | 0 | 0 0 |
| 2:15 PM | 0 | 0 | Ō | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 PM 3:45 PM | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | U | | | | | | | | | | | | | | |
| 5:00 PM 5:15 PM | Ö | 0 | Ö | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | 0 | 0 |
| 5:00 PM | | | _ | | | | | | | | | | | | | | |

Location: Rd 76/N American St & W Goshen Ave **City:** Visalia

Project ID: 22-090052-002 **Date:** 4/21/2022

Data - Pedestrians (Crosswalks)

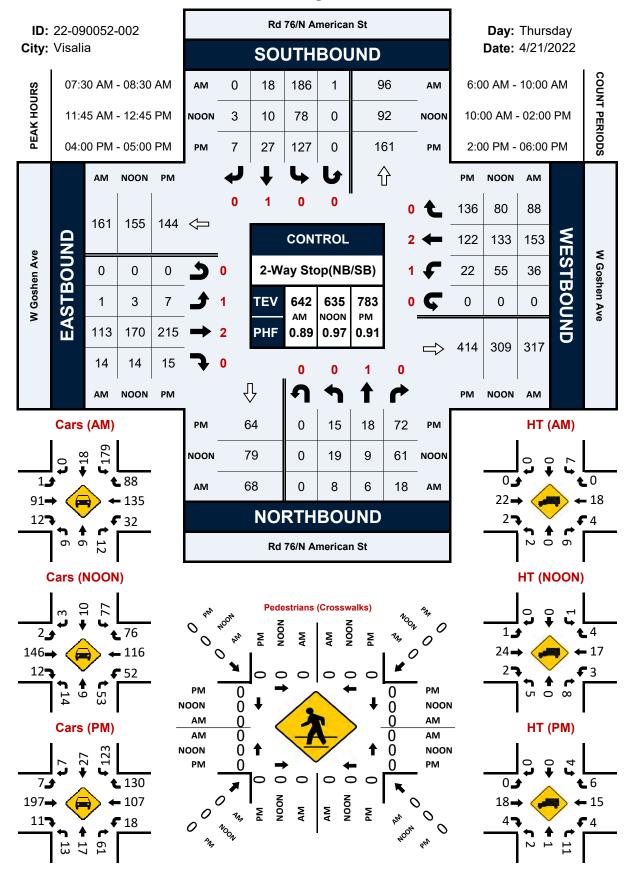
| NS/EW Streets: | Rd 76/N A | American St | Rd 76/N Ai | merican St | W Gosł | nen Ave | W Gos | hen Ave | |
|-----------------------------------|-----------|-------------|--------------|------------|--------|---------|------------|--------------|-------|
| A B 4 | NORT | TH LEG | SOUTI | H LEG | EAST | Γ LEG | WES | T LEG | |
| AM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 1 100.00% | 0 0.00% | 0 | 0 | 0 0.00% | 1 100.00% | 2 |
| PEAK HR: | 07:30 AM | - 08:30 AM | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | THIEC | COUT | | | TLEC | | TIEC | |
| | | | | | | | | | |

| 10:00 AM 10:15 AM 10:30 AM 10:45 AM 11:00 AM 11:15 AM 11:30 AM | NORTH LEG EB WB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | EB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | JTH LEG | NB 0 0 0 0 | SB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | WEST NB 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | SB 0 0 0 | TOTAL 0 0 0 |
|--|---|--|-------------|------------------------|--|---|-------------------|----------------------|
| 10:15 AM 10:30 AM 10:45 AM 11:00 AM 11:15 AM 11:30 AM | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 | 0 0 0 | 0 |
| 10:30 AM 10:45 AM 11:00 AM 11:15 AM 11:30 AM | 0 0 0 0 0 0 0 0 | 0 0 | 0 0 0 | | 0 | 0 | 0 0 | • |
| 10:45 AM 11:00 AM 11:15 AM 11:30 AM | 0 0 0 0 0 0 | 0 | 0 0 0 | | 0 | • | 0 | 0 |
| 11:00 AM 11:15 AM 11:30 AM | 0 0 0 | 0 | 0 | _ | 0 | • | | |
| 11:15 AM 11:30 AM | 0 0 | - | 0 | | U | 0 | 0 | 0 |
| 11:30 AM | - | 0 | • | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| | - • | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1.10 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 |
| | | | | | | | | |
| | EB WB | EB | WB | NB | SB | NB | SB | TOTAL |
| | 0 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 |
| APPROACH %'s: | | | | | | 50.00% | 50.00% | |
| | 45 AM - 12:45 PM | | | | | | | TOTAL |
| | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR: | | | | | | | | |

| DAA | NORT | H LEG | SOUT | 'H LEG | EAST | LEG | WES | T LEG | |
|-----------------|------------|------------|-------|---------|---------|-------|-------|---------|-------|
| PM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 2:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 3:30 PM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 3:45 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 1 | 4 |
| APPROACH %'s: | 100.00% | 0.00% | 0.00% | 100.00% | 100.00% | 0.00% | 0.00% | 100.00% | |
| PEAK HR: | 04:00 PM - | - 05:00 PM | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR: | | | | | | | | | |
| | | | | | | | | | |

Rd 76/N American St & W Goshen Ave

Peak Hour Turning Movement Count



Location: N Plaza Dr & W Ferguson Ave City: Visalia Control: Signalized

Data - Total

| _ | | | | | | | | Data - | Total | | | | | | | | |
|--------------------|----------|------------|----------|--------|--------|------------|--------|--------|--------|----------|---------|-------|--------|----------|--------|-------|------------|
| NS/EW Streets: | | N Plaz | a Dr | | | N Plaza | a Dr | | | W Fergus | on Ave | | | W Fergus | on Ave | | |
| | | NORTH | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 15 | 110 | 0 | 0 | 1 | 117 | 4 | 2 | 2 | 0 | 2 | 0 | 0 | 1 | 1 | 0 | 255 |
| 7:15 AM | 9 | 114 | 2 | 0 | 0 | 120 | 7 | 1 | 4 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 260 |
| 7:30 AM 7:45 AM | 22 28 | 129 107 | 3 2 | 0 | 0 | 166 152 | 3 9 | 1 0 | 4 | 0 | 4 11 | 0 | 2 | 0 | 0 | 0 | 334 313 |
| 7:45 AM 8:00 AM | 10 | 107 | 2 | 1 | 0 | 123 | 6 | 1 | 6 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 265 |
| 8:15 AM | 9 | 131 | 0 | 0 | 4 | 120 | 8 | 0 | 2 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 278 |
| 8:30 AM | 12 | 100 | 0 | 0 | 0 | 115 | 5 | 1 | 4 | 1 | 8 | 0 | 1 | 0 | 2 | 0 | 249 |
| 8:45 AM | 7 | 86 | 3 | Ô | 1 | 105 | 3 | ō | 2 | Ō | 20 | Ô | 2 | Ö | ī | Ô | 230 |
| 01.15711.1 | • | - | _ | ŭ | - | 100 | | • | - | • | | ŭ | _ | | - | ŭ | 250 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 112 | 885 | 12 | 1 | 6 | 1018 | 45 | 6 | 26 | 1 | 55 | 0 | 11 | 2 | 4 | 0 | 2184 |
| APPROACH %'s: | 11.09% | 87.62% | 1.19% | 0.10% | 0.56% | 94.70% | 4.19% | 0.56% | 31.71% | 1.22% | 67.07% | 0.00% | 64.71% | 11.76% | 23.53% | 0.00% | |
| PEAK HR : | | 07:30 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 69 | 475 | 7 | 1 | 4 | 561 | 26 | 2 | 14 | 0 | 24 | 0 | 7 | 0 | 0 | 0 | 1190 |
| PEAK HR FACTOR : | 0.616 | 0.906 | 0.583 | 0.250 | 0.250 | 0.845 | 0.722 | 0.500 | 0.583 | 0.000 | 0.545 | 0.000 | 0.875 | 0.000 | 0.000 | 0.000 | 0.891 |
| | | 0.89 | 96 | | | 0.87 | 2 | | | 0.73 | 51 | | | 0.87 | /5 | | |
| | | NORTH | BOLIND | | | SOUTHE | SULIND | | | EASTB | OLIND | | | WESTE | OLIND | | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| FIVI | NL | NT | NR | NU | SL | ST | SR | SU | ĒL | ET | ĒR | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 9 | 130 | 9 | 0 | 0 | 136 | 3 | 0 | 9 | 1 | 19 | 0 | 5 | 0 | 2 | 0 | 323 |
| 4:15 PM | 3 | 147 | 6 | 0 | 0 | 126 | 3 | 0 | 6 | 0 | 9 | 0 | 9 | 0 | 3 | 0 | 312 |
| 4:30 PM | 5 | 153 | 1 | 1 | 0 | 122 | 2 | 1 | 4 | 0 | 10 | 0 | 10 | 0 | 1 | 0 | 310 |
| 4:45 PM | 5 | 164 | 1 | 0 | 3 | 115 | 3 | 0 | 8 | 0 | 10 | 0 | 4 | 0 | 3 | 0 | 316 |
| 5:00 PM | 4 | 146 | 3 | 1 | 1 | 121 | 1 | 1 | 7 | 0 | 22 | 0 | 6 | 0 | 2 | 0 | 315 |
| 5:15 PM | 2 | 145 140 | 2 | 0 | 0 | 113 | 4 | 0 | 8 | 0 | 29 | 0 | 0 | 0 | 3 | 0 | 306 |
| 5:30 PM 5:45 PM | 2 11 | 118 | 1 | 1 0 | 0 2 | 134 123 | 1 | 0 | 7 1 | 0 | 11 7 | 0 | 1 3 | 0 | 0 | 0 | 298 270 |
| 5:45 PM | 11 | 118 | 1 | U | 2 | 123 | 4 | U | 1 | U | / | U | 3 | U | U | U | 2/0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 41 | 1143 | 24 | 3 | 6 | 990 | 21 | 2 | 50 | 1 | 117 | 0 | 38 | 0 | 14 | 0 | 2450 |
| APPROACH %'s: | 3.39% | 94.38% | 1.98% | 0.25% | 0.59% | 97.15% | 2.06% | 0.20% | 29.76% | 0.60% | 69.64% | 0.00% | 73.08% | 0.00% | 26.92% | 0.00% | |
| PEAK HR : | | | 05:00 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 22 | 594 | 17 | 1 | 3 | 499 | 11 | 1 | 27 | 1 | 48 | 0 | 28 | 0 | 9 | 0 | 1261 |
| | 0.611 | 0.905 | 0.472 | 0.250 | 0.250 | 0.917 | 0.917 | 0.250 | 0.750 | 0.250 | 0.632 | 0.000 | 0.700 | 0.000 | 0.750 | 0.000 | |
| PEAK HR FACTOR: | 0.011 | 0.905 | | 0.230 | 0.230 | 0.92 | | 0.250 | 0.750 | 0.65 | | | | 0.77 | | 0.000 | 0.976 |

Location: N Plaza Dr & W Ferguson Ave City: Visalia Control: Signalized

Data - Cars

| _ | | | | | | | | Data · | · Cars | | | | | | | | |
|--------------------|---------|------------|--------|-------|-------|------------|--------|--------|--------|----------|--------|-------|--------|----------|--------|-------|------------|
| NS/EW Streets: | | N Plaz | a Dr | | | N Plaz | a Dr | | | W Fergus | on Ave | | | W Fergus | on Ave | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 10 | 89 | 0 | 0 | 0 | 103 | 2 | 2 | 1 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 210 |
| 7:15 AM | 7 | 103 | 2 | 0 | 0 | 107 | 7 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 230 |
| 7:30 AM | 20 | 111 | 3 | 0 | 0 | 157 | 1 | 1 | 2 | 0 | 3 | 0 | 2 | 0 | 0 | 0 | 300 |
| 7:45 AM | 25 | 93 87 | 2 | 0 | 0 | 138 | 8 | 0 | 1 | 0 | 10 | 0 | 2 | 0 | 0 | 0 | 279 |
| 8:00 AM | 7 | 87 110 | 2 | 1 | 0 | 104 | 4 6 | 1 0 | 6 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 216 238 |
| 8:15 AM 8:30 AM | 5 10 | 84 | 0 | 0 | 0 | 110 104 | 2 | 1 | 1 | 0 | 2 4 | 0 | 1 | 0 | 1 | 0 | 238 |
| 8:45 AM | 6 | 72 | 2 | 0 | 0 | 90 | 2 | 0 | 1 | 0 | 13 | 0 | 2 | 0 | 0 | 0 | 188 |
| 6:45 AM | 0 | 72 | 2 | U | U | 90 | 2 | U | 1 | U | 13 | U | 2 | U | U | U | 100 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 90 | 749 | 11 | 1 | 3 | 913 | 32 | 6 | 15 | 0 | 37 | 0 | 10 | 0 | 2 | 0 | 1869 |
| APPROACH %'s: | 10.58% | 88.01% | 1.29% | 0.12% | 0.31% | 95.70% | 3.35% | 0.63% | 28.85% | 0.00% | 71.15% | 0.00% | 83.33% | 0.00% | 16.67% | 0.00% | |
| PEAK HR : | | 7:30 AM - | | | _ | | | _ | | | | _ | _ | | | _ | TOTAL |
| PEAK HR VOL : | 57 | 401 | 7 | 1 | 3 | 509 | 19 | 2 | 10 | 0 | 17 | 0 | 7 | 0 | 0 | 0 | 1033 |
| PEAK HR FACTOR : | 0.570 | 0.903 | 0.583 | 0.250 | 0.250 | 0.811 | 0.594 | 0.500 | 0.417 | 0.000 | 0.425 | 0.000 | 0.875 | 0.000 | 0.000 | 0.000 | 0.861 |
| | | 0.0 | 09 | | | 0.6 | 30 | | | 0.6 | 14 | | | 0.6 | ′5 | | |
| | | NORTH | ROLIND | | | SOUTH | BOLIND | | | EASTB | OLIND | | | WESTE | OLIND | | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| r IVI | NL | NT | NR | NU | SL | ST | SR | SU | ĒĹ | ET | ĒR | EU | WL. | WT | WR | WU | TOTAL |
| 4:00 PM | 7 | 112 | 7 | 0 | 0 | 124 | 2 | 0 | 6 | 1 | 18 | 0 | 4 | 0 | 2 | 0 | 283 |
| 4:15 PM | 1 | 129 | 3 | 0 | 0 | 115 | 1 | 0 | 5 | 0 | 6 | 0 | 9 | 0 | 2 | 0 | 271 |
| 4:30 PM | 3 | 142 | 1 | 1 | 0 | 108 | 1 | 1 | 2 | 0 | 8 | 0 | 10 | 0 | 1 | 0 | 278 |
| 4:45 PM | 3 | 150 | 1 | 0 | 1 | 105 | 2 | 0 | 3 | 0 | 10 | 0 | 4 | 0 | 2 | 0 | 281 |
| 5:00 PM | 3 | 130 | 2 | 1 | 1 | 111 | 0 | 1 | 6 | 0 | 19 | 0 | 5 | 0 | 1 | 0 | 280 |
| 5:15 PM | 2 | 136 | 1 | 0 | 0 | 102 | 2 | 0 | 7 | 0 | 26 | 0 | 0 | 0 | 3 | 0 | 279 |
| 5:30 PM | 2 | 126 | 1 | 1 | 0 | 125 | 1 | 0 | 6 | 0 | 9 | 0 | 1 | 0 | 0 | 0 | 272 |
| 5:45 PM | 7 | 108 | 1 | 0 | 0 | 117 | 4 | 0 | 0 | 0 | 6 | 0 | 2 | 0 | 0 | 0 | 245 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 28 | 1033 | 17 | 3 | 2 | 907 | 13 | 2 | 35 | 1 | 102 | 0 | 35 | 0 | 11 | 0 | 2189 |
| APPROACH %'s: | 2.59% | 95.56% | 1.57% | 0.28% | 0.22% | 98.16% | 1.41% | 0.22% | 25.36% | 0.72% | 73.91% | 0.00% | 76.09% | 0.00% | 23.91% | 0.00% | |
| PEAK HR : | | 04:00 PM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 14 | 533 | 12 | 1 | 1 | 452 | 6 | 1 | 16 | 1 | 42 | 0 | 27 | 0 | 7 | 0 | 1113 |
| PEAK HR FACTOR : | 0.500 | 0.888 | 0.429 | 0.250 | 0.250 | 0.911 | 0.750 | 0.250 | 0.667 | 0.250 | 0.583 | 0.000 | 0.675 | 0.000 | 0.875 | 0.000 | 0.983 |
| | | 0.9 | ng | | | 0.9 | 13 | | | 0.59 | 20 | | | 0.77 | 72 | | 0.505 |

Location: N Plaza Dr & W Ferguson Ave City: Visalia Control: Signalized

NT 110 84.62%

61 0.847

5 0.417

8 1.000

TOTAL VOLUMES : APPROACH %'s : PEAK HR : PEAK HR VOL : PEAK HR FACTOR :

NU

0.00%

0 0.000 2 0.250

Project ID: 22-090052-003 **Date:** 4/21/2022

EU 0 0.00%

0 0.000

15 50.00%

0

0 6 0.000 0.500 0.850

WL 3 50.00%

1 0.250

0 0.000

TOTAL 261

148 0.902

3 50.00%

2 0.500

0 0.000

| L | n | та | - | п | |
|---|---|----|---|---|--|

| NS/EW Streets: | | N Plaz | a Dr | | | N Plaz | a Dr | | | W Fergus | on Ave | | | W Fergus | on Ave | | |
|---|----------------------------------|--|--|--------------------------------------|--|--|--|--|--------------|--|---|--------------------------------------|--|--|--|---|---|
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | OUND | ' | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | TOTAL |
| 7:00 AM | NL 5 | NT 21 | NR 0 | NU 0 | SL | ST 14 | SR 2 | SU | EL | ET | ER 0 | EU 0 | WL 0 | WT | WR 0 | WU 0 | TOTAL 45 |
| 7:15 AM | 2 | 11 | 0 | 0 | 0 | 13 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 30 |
| 7:30 AM | 2 | 18 | Ô | 0 | ů. | 9 | 2 | Ô | 2 | n | 1 | n | ñ | ñ | 0 | Ô | 34 |
| 7:45 AM | 3 | 14 | Ö | Ö | Ö | 14 | 1 | Ö | 1 | Ö | ī | Ö | Ŏ | Õ | Ö | Ö | 34 |
| 8:00 AM | 3 | 21 | 0 | 0 | 0 | 19 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 49 |
| 8:15 AM | 4 | 21 | 0 | 0 | 1 | 10 | 2 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 40 |
| 8:30 AM | 2 | 16 | 0 | 0 | 0 | 11 | 3 | 0 | 3 | 1 | 4 | 0 | 0 | 0 | 1 | 0 | 41 |
| 8:45 AM | 1 | 14 | 1 | 0 | 1 | 15 | 1 | 0 | 1 | 0 | 7 | 0 | 0 | 0 | 1 | 0 | 42 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | UU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 22 13.84% | 136 85.53% | 1 0.63% | 0 0.00% | 3 2.48% | 105 86.78% | 13 10.74% | 0 0.00% | 11 36.67% | 1 3.33% | 18 60.00% | 0 0.00% | 1 20.00% | 2 40.00% | 2 40.00% | 0 0.00% | 315 |
| APPROACH %'s: | | 85.53% 07:30 AM - | | 0.00% | 2.48% | 86.78% | 10./4% | 0.00% | 36.6/% | 3.33% | 60.00% | 0.00% | 20.00% | 40.00% | 40.00% | 0.00% | TOTAL |
| | | | | | | | | | | | | | | | | | |
| PEAK HR: | | | | 0 | 1 | 52 | 7 | 0 | 4 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | |
| PEAK HR VOL : | 12 | 74 | 0 | 0 | 1 | 52 0.684 | 7 0.875 | 0 | 4 0.500 | 0 | 7 0.438 | 0 | 0 | 0 | 0 | 0 | 157 |
| | | 74 0.881 | 0.000 | 0 0.000 | 1 0.250 | 0.684 | 0.875 | 0 0.000 | 4 0.500 | 0.000 | 0.438 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | |
| PEAK HR VOL : | 12 | 74 | 0.000 | | | | 0.875 | | | | 0.438 | | | | | | 157 |
| PEAK HR VOL : PEAK HR FACTOR : | 12 | 74 0.881 | 0 0.000 50 | | | 0.684 | 0.875 14 | | | 0.000 | 0.438 88 | | | | 0.000 | | 157 |
| PEAK HR VOL : PEAK HR FACTOR : | 12 0.750 | 74 0.881 0.86 NORTH 2 | 0 0.000 50 BOUND 1 | 0.000 | 0.250 | 0.684 0.71 SOUTHE 2 | 0.875 14 BOUND 1 | 0.000 | 0.500 | 0.000 0.60 EASTB | 0.438 88 | 0.000 | 0.000 | 0.000 WESTB | 0.000 BOUND 1 | 0.000 | 157 0.801 |
| PEAK HR VOL: PEAK HR FACTOR: | 12 0.750 | 74 0.881 0.86 NORTH 2 NT | 0 0.000 50 BOUND 1 NR | 0.000 0 NU | 0.250 1 SL | 0.684 0.71 SOUTHE 2 ST | 0.875 14 | 0.000 O SU | | 0.000 0.66 EASTB 2 ET | 0.438 88 | 0.000 0 EU | | 0.000 WESTB 2 WT | 0.000 BOUND 1 WR | 0.000 0 WU | 157 0.801 TOTAL |
| PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM | 12 0.750 | 74 0.881 0.86 NORTH 2 NT 18 | 0 0.000 50 BOUND 1 | 0.000 0 NU 0 | 0.250 1 SL 0 | 0.684 0.71 SOUTHE 2 ST 12 | 0.875 14 BOUND 1 | 0.000 | 0.500 | 0.000 0.60 EASTB | 0.438 88 OUND 1 | 0.000 0 EU 0 | 0.000 | 0.000 WESTB | 0.000 BOUND 1 | 0.000 0 WU 0 | 157 0.801 TOTAL 40 |
| PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.80 NORTH 2 NT 18 18 | 0 0.000 60 BOUND 1 NR 2 3 | 0.000 0 NU 0 | 0.250 1 SL 0 0 | 0.684 0.71 SOUTHI 2 ST 12 11 | 0.875 14 BOUND 1 | 0.000 0 SU 0 0 | 0.500 | 0.000 0.66 EASTB 2 ET | 0.438 88 OUND 1 | 0.000 0 EU 0 0 | 0.000 | 0.000 WESTB 2 WT 0 0 | 0.000 BOUND 1 WR | 0.000 0 WU 0 0 | 157 0.801 TOTAL 40 41 |
| PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:30 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.86 NORTH 2 NT 18 18 11 | 0 0.000 50 BOUND 1 NR 2 3 | 0.000 0 NU 0 0 | 0.250 1 SL 0 0 0 | 0.684 0.71 SOUTHI 2 ST 12 11 14 | 0.875 14 BOUND 1 | 0.000 0 SU 0 0 0 | 0.500 | 0.000 0.60 EASTB 2 ET 0 0 | 0.438 88 OUND 1 ER 1 3 2 | 0.000 0 EU 0 0 | 0.000 1 WL 1 0 0 | 0.000 WESTE 2 WT 0 0 0 0 | 0.000 BOUND 1 WR | 0.000 0 WU 0 0 | 157 0.801 TOTAL 40 41 32 |
| PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.86 NORTH 2 NT 18 18 11 14 | 0 0.000 60 BOUND 1 NR 2 3 | 0.000 0 NU 0 0 | 0.250 1 SL 0 0 0 2 | 0.684 0.71 SOUTHE 2 ST 12 11 14 10 | 0.875 14 BOUND 1 | 0.000 0 SU 0 0 0 0 0 | 0.500 | 0.000 0.6i EASTB 2 ET 0 0 0 | 0.438 88 OUND 1 | 0.000 0 EU 0 0 0 0 | 0.000 | 0.000 WESTE 2 WT 0 0 0 0 | 0.000 BOUND 1 WR | 0.000 0 WU 0 0 0 | 157 0.801 TOTAL 40 41 32 35 |
| PEAK HR VOL: PEAK HR FACTOR: PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.80 NORTH 2 NT 18 18 11 14 | 0 0.000 50 BOUND 1 NR 2 3 | 0.000 0 NU 0 0 0 0 | 0.250 1 SL 0 0 0 2 0 | 0.684 0.71 SOUTHE 2 ST 12 11 14 10 | 0.875 14 BOUND 1 SR 1 2 1 1 | 0.000 0 SU 0 0 0 0 | 0.500 | 0.000 0.66 EASTB 2 ET 0 0 0 | 0.438 88 OUND 1 ER 1 3 2 | 0.000 0 EU 0 0 0 0 | 0.000 1 WL 1 0 0 0 1 | 0.000 WESTB 2 WT 0 0 0 0 0 | 0.000 BOUND 1 WR 0 1 0 1 | 0.000 0 WU 0 0 0 | 157 0.801 TOTAL 40 41 32 35 35 |
| PEAK HR VOL: PEAK HR FACTOR: PM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM 5:15 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.80 NORTH 2 NT 18 18 11 14 16 9 | 0 0.000 50 BOUND 1 NR 2 3 0 0 | 0.000 0 NU 0 0 0 0 | 0.250 1 SL 0 0 0 2 0 0 | 0.684 0.71 SOUTHE 2 ST 12 11 14 10 10 | 0.875 14 BOUND 1 SR 1 2 1 1 1 | 0.000 SU 0 0 0 0 | 0.500 | 0.000 0.6i EASTB 2 ET 0 0 0 | 0.438 88 OUND 1 ER 1 3 2 | 0.000 EU 0 0 0 0 0 | 0.000 1 WL 1 0 0 0 1 0 | 0.000 WESTE 2 WT 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 0.000 BOUND 1 WR 0 1 0 1 0 | 0.000 0 WU 0 0 0 0 0 | TOTAL 40 41 32 35 35 27 |
| PEAK HR VOL: PEAK HR FACTOR: PIM 4:00 PM 4:15 PM 4:30 PM 4:45 PM 5:00 PM | 12 0.750 1 NL 2 2 | 74 0.881 0.80 NORTH 2 NT 18 18 11 14 | 0 0.000 50 BOUND 1 NR 2 3 | 0.000 0 NU 0 0 0 0 | 0.250 1 SL 0 0 0 2 0 | 0.684 0.71 SOUTHE 2 ST 12 11 14 10 | 0.875 14 BOUND 1 SR 1 2 1 1 | 0.000 0 SU 0 0 0 0 | 0.500 | 0.000 0.66 EASTB 2 ET 0 0 0 | 0.438 88 OUND 1 ER 1 3 2 | 0.000 0 EU 0 0 0 0 | 0.000 1 WL 1 0 0 0 1 | 0.000 WESTB 2 WT 0 0 0 0 0 | 0.000 BOUND 1 WR 0 1 0 1 | 0.000 0 WU 0 0 0 | 157 0.801 TOTAL 40 41 32 35 35 |

15 50.00%

11 0.550

ST 83 87.37%

47 0.839

8 8.42%

0 0.000

5 39 0.625 0.900

Location: N Plaza Dr & W Ferguson Ave City: Visalia Control: Signalized

| | oig.idii.Ecc | | | | | | | | | | | | | | .,, | | |
|--------------------|--------------|----------|------------|-------|-------|---------|-------|--------|-------|---------|----------|-------|-------|---------|---------|-------|-------|
| | | | | | | | | Data - | Bikes | | | | | | | | - |
| NS/EW Streets: | | N Pla | ıza Dr | | | N Plaz | a Dr | | | W Fergu | ison Ave | | | W Fergu | son Ave | | |
| | | NORTI | HBOUND | | | SOUTH | BOUND | | | FAST | BOUND | | | WEST | BOUND | | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| AIVI | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | Ó | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ó | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | | | | | | | | | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| APPROACH %'s: | | | | | | | | | | | | | l | | | | |
| PEAK HR : | | 07:30 AM | - 08:30 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR: | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | | | | | | | | | | | | | | | | |
| | | | | | | | | - | | | | | | | | | 1 |
| 200 | | | HBOUND | _ | | SOUTH | BOUND | _ | | | BOUND | _ | | | BOUND | _ | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| 4 00 014 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM 5:15 PM | - | 0 | 0 | | 0 | | 0 | | 0 | - | 0 | - | 0 | 0 | 0 | | |
| 5:15 PM 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | U | U | U | U | U | U | U | U | U | U | U | U | U | U | U | U | U |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| APPROACH %'s: | | | | | 0.00% | 100.00% | 0.00% | 0.00% | | | | | l . | | | | |
| PEAK HR : | | 04:00 PM | - 05:00 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| PEAK HR FACTOR: | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 |
| | | | | | | 0.2 | | | | | | | | | | | |

National Data & Surveying Services Intersection Turning

Location: N Plaza Dr & W Ferguson Ave

N Plaza Dr & W Ferguson Ave

Location: N Plaza Dr & W Ferguson Ave

Project ID: 22-090052-003

Date: 4/21/2022

Data - Pedestrians (Crosswalks)

0

0

TOTAL

1

0.250

| NS/EW Streets: | N Pla | za Dr | N Pla | za Dr | W Fergu | ison Ave | W Ferg | uson Ave | |
|----------------|-------|--------|---------|-------|---------|----------|--------|----------|-------|
| A | NORT | 'H LEG | SOUTI | 1 LEG | EAST | Γ LEG | WES | T LEG | |
| AM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 3 |
| APPROACH %'s: | | | 100.00% | 0.00% | | | 0.00% | 100.00% | |

0.250

0.250

PEAK HR:

PEAK HR VOL:

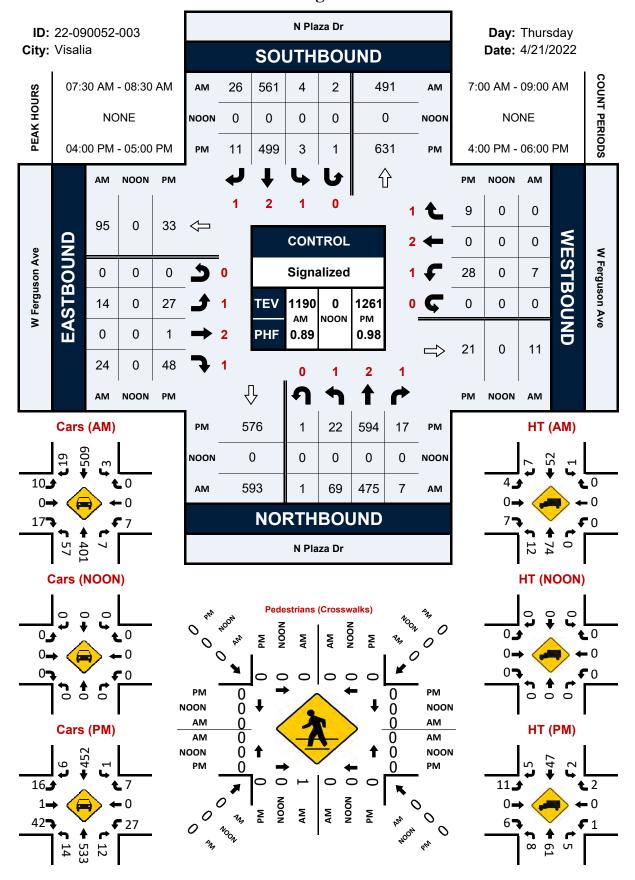
PEAK HR FACTOR:

07:30 AM - 08:30 AM

| PM | NORT | 'H LEG | SOUT | 'H LEG | EAST | LEG | WEST | Γ LEG | |
|------------------|----------|------------|------|--------|------|-----|------|-------|-------|
| PIVI | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| APPROACH %'s: | | | | | | | | | |
| PEAK HR : | 04:00 PM | - 05:00 PM | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | | | | | | | | | |
| | | | | | | | | | |

N Plaza Dr & W Ferguson Ave

Peak Hour Turning Movement Count



Location: CR J19/Rd 80/N Plaza Dr & California Dairies Dwy City: Visalia Control: No Control

Data - Total

| NS/EW Streets: | С | R J19/Rd 80 |)/N Plaza D | r | CI | R J19/Rd 80 | /N Plaza D | r | Total | California I | Dairies Dwy | | (| California Da | airies Dwy | | |
|-----------------------------------|------------|----------------------|----------------|------------|------------|----------------|-------------|------------|---------|--------------|-------------|---------|--------------|---------------|-------------|------------|---------------|
| | _ | NORTHI | | _ | _ | SOUTHE | | _ | _ | | BOUND | _ | _ | WESTB | | _ | |
| AM | 0 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 1 WT | 0 WR | 0 WU | TOTAL |
| 6:00 AM | 0 | 121 | 1 | 0 | 0 | 77 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 200 |
| 6:15 AM 6:30 AM | 0 0 | 146 131 | 0 | 0 | 1 0 | 82 91 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 1 0 | 0 | 230 222 |
| 6:45 AM | 0 | 136 | 0 | 0 | 0 | 146 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 282 |
| 7:00 AM 7:15 AM | 0 0 | 131 137 | 1 2 | 0 | 0 1 | 123 112 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 255 252 |
| 7:30 AM | 0 | 158 | 2 | 0 | 0 | 184 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 344 |
| 7:45 AM 8:00 AM | 0 | 141 127 | <u>9</u> 5 | 0 | 4 | 163 130 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 318 264 |
| 8:15 AM | 0 | 139 | 2 | 0 | 1 0 | 117 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 258 |
| 8:30 AM | 0 | 119 | 1 | 0 | 0 | 115 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 235 |
| 8:45 AM 9:00 AM | 0 | 101 84 | 0 | 0 | 1 | 144 137 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 246 224 |
| 9:15 AM | 0 | 87 | 1 | 0 | 1 | 123 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 212 |
| 9:30 AM 9:45 AM | 0 0 | 109 85 | 2 | 0 | 0 | 161 120 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 2 | 0 | 272 210 |
| | | | | | | | | | | | | | _ | | | | |
| TOTAL VOLUMES : | NL 0 | NT 1952 | NR 28 | O NN | SL 10 | ST 2025 | SR 0 | SU 1 | EL 0 | ET 0 | ER 0 | EU 0 | WL 3 | WT 0 | WR 5 | WU 0 | TOTAL 4024 |
| APPROACH %'s: | 0.00% | 98.59% | 1.41% | 0.00% | 0.49% | 99.46% | 0.00% | 0.05% | Ů | | | 0 | 37.50% | 0.00% | 62.50% | 0.00% | |
| PEAK HR : PEAK HR VOL : | 0 | 07:30 AM - 565 | 08:30 AM 18 | 0 | 5 | 594 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | TOTAL 1184 |
| PEAK HR VOL : | 0.000 | 0.894 | 0.500 | 0.000 | 0.313 | 0.807 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.250 | 0.000 | 0.860 |
| | | 0.91 | 11 | | | 0.81 | .4 | | | | | | | 0.50 | 0 | | 0.860 |
| | | NORTHI | BOUND | | | SOUTHE | BOUND | | | EAST | BOUND | | | WESTB | OUND | | |
| NOON | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | TOTAL |
| 10:00 AM | NL 0 | NT 110 | NR 0 | NU 0 | SL 0 | ST 117 | SR 0 | SU 0 | EL 0 | ET0 | ER 0 | EU | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 227 |
| 10:15 AM | 0 | 107 | 0 | 0 | 0 | 109 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 216 |
| 10:30 AM 10:45 AM | 0 | 105 101 | 0 | 0 | 0 0 | 110 108 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 1 | 0 0 | 0 1 | 0 | 215 211 |
| 11:00 AM | 0 | 82 | 0 | 0 | 0 | 155 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 240 |
| 11:15 AM 11:30 AM | 0 0 | 106 125 | 2 | 0 | 0 1 | 148 136 | 0 0 | 0 | 0 | 0 | 0 | 0 | 1 3 | 0 0 | 0 1 | 0 | 257 266 |
| 11:45 AM | 0 | 107 | 1 | 0 | 0 | 98 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 212 |
| 12:00 PM 12:15 PM | 0 | 124 113 | 0 1 | 0 1 | 0 0 | 111 106 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 2 | 0 0 | 1 | 0 | 236 224 |
| 12:30 PM | Ö | 108 | 3 | 0 | 0 | 92 | 0 | 0 | 0 | Ö | 0 | 0 | 0 | Ö | 0 | 0 | 203 |
| 12:45 PM 1:00 PM | 0 | 108 98 | 0 | 0 1 | 2 | 92 92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 199 193 |
| 1:15 PM | 0 | 107 | 1 | 0 | 0 | 153 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 263 |
| 1:30 PM | 0 | 161 | 2 | 0 | 0 | 194 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 360 |
| 1:45 PM | 0 | 161 | 2 | 0 | 2 | 176 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 343 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 0.00% | 1823 99.08% | 15 0.82% | 2 0.11% | 5 0.25% | 1993 99.75% | 0 0.00% | 0 0.00% | 0 | 0 | 0 | 0 | 20 74.07% | 0 0.00% | 7 25.93% | 0 0.00% | 3865 |
| PEAK HR : | | 01:00 PM - | 02:00 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0.000 | 527 0.818 | 5 0.625 | 1 0.250 | 4 0.500 | 615 0.793 | 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0.000 | 6 0.750 | 0.000 | 1 0.250 | 0 0.000 | 1159 |
| PLAK HICTACION . | 0.000 | 0.81 | | 0.230 | 0.500 | 0.79 | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.58 | | 0.000 | 0.805 |
| | | NORTHI | BOLIND | | | SOUTHE | SOLIND | | | FAST | BOUND | | | WESTB | OLIND | | |
| PM | 0 | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | |
| 2:00 PM | NL 0 | NT 123 | NR 2 | NU 0 | SL 2 | ST 144 | SR 0 | SU 0 | EL 0 | ET0 | ER 0 | EU | WL 1 | WT 0 | WR 2 | WU 0 | TOTAL 274 |
| 2:15 PM | 0 | 107 | 1 | 0 | 1 | 143 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 252 |
| 2:30 PM 2:45 PM | 0 | 129 121 | 0 | 0 1 | 0 | 161 130 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 290 252 |
| 3:00 PM | 0 | 119 | 0 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 252 |
| 3:15 PM | 0 | 117 122 | 0 | 0 | 0 | 165 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 283 277 |
| 3:30 PM 3:45 PM | 0 | 125 | 1 | 0 | 0 | 155 186 | 0 | 0 | 0 | 0 0 | 0 | 0 | 1 | 0 | 1 | 0 | 314 |
| 4:00 PM | 0 | 156 | 2 | 0 | 0 | 157 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 318 |
| 4:15 PM 4:30 PM | 0 0 | 161 168 | 0 | 0 0 | 0 1 | 165 141 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 1 2 | 0 0 | 1 0 | 0 | 328 312 |
| 4:45 PM | 0 | 177 | Ŏ | 0 | 0 | 128 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 310 |
| 5:00 PM 5:15 PM | 0 0 | 160 147 | 1 0 | 0 | 0 0 | 150 152 | 0 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 3 0 | 0 | 318 300 |
| 5:30 PM | 0 | 139 | 0 | 1 | 0 | 142 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 283 |
| 5:45 PM | 0 | 120 | 0 | 0 | 0 | 149 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 272 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 0.00% | 2191 99.59% | 7 0.32% | 2 0.09% | 4 0.17% | 2401 99.83% | 0 0.00% | 0 0.00% | 0 | 0 | 0 | 0 | 21 70.00% | 0 0.00% | 9 30.00% | 0 0.00% | 4635 |
| PEAK HR : | | 99.59% 03:45 PM - | | 0.09% | 0.17% | 39.03% | 0.00% | 0.00% | | | | | 70.00% | 0.00% | 30.00% | 0.00% | TOTAL |
| PEAK HR VOL : | 0 | 610 | 3 | 0 | 1 | 649 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 3 | 0 | 1272 |
| PEAK HR FACTOR : | 0.000 | 0.908 | 0.375 L2 | 0.000 | 0.250 | 0.872 0.87 | 0.000 '4 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.750 | 0.000 | 0.970 |
| | | 0.5 | | | | 0.07 | | | | | | | | 0.75 | | | |

Location: CR J19/Rd 80/N Plaza Dr & California Dairies Dwy City: Visalia

Project ID: 22-090052-004

| | Visalia No Control | | | | | | | D-4- | C | | | | Pr | oject ID: Date: | 22-090052- 4/21/2022 | 004 | |
|-----------------------------------|-----------------------|----------------------|---------------|------------|------------|----------------|-------------|------------|---------|------------|-------------|------------|--------------|--------------------|-------------------------|------------|---------------|
| | | | | | | | | Data | - Cars | | | | | | | | 1 |
| NS/EW Streets: | С | R J19/Rd 8 | | r | С | R J19/Rd 80 | | r | | | Dairies Dwy | | 1 | California D | | | |
| AM | 0 | NORTH 2 | BOUND | 0 | 0 | SOUTHI 2 | BOUND 0 | 0 | 0 | EAST 0 | BOUND | 0 | 0 | WESTE 1 | BOUND 0 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 6:00 AM 6:15 AM | 0 | 106 127 | 1 0 | 0 | 0 | 70 71 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 1 | 0 | 178 200 |
| 6:30 AM | 0 | 114 | 0 | 0 | 0 | 80 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ö | Ō | 0 | 194 |
| 6:45 AM | 0 | 119 | 0 | 0 | 0 | 131 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 250 |
| 7:00 AM 7:15 AM | 0 | 104 125 | 1 2 | 0 | 0 1 | 106 97 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 211 225 |
| 7:30 AM | 0 | 141 | 2 | 0 | 0 | 169 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 312 |
| 7:45 AM 8:00 AM | 0 | 121 102 | <u>9</u> 5 | 0 | 1 | 153 109 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 288 218 |
| 8:15 AM | 0 | 119 | 2 | 0 | 0 | 107 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 228 |
| 8:30 AM 8:45 AM | 0 | 99 85 | 1 0 | 0 | 0 | 104 121 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 204 207 |
| 9:00 AM | 0 | 64 | 0 | 0 | 1 | 115 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 182 |
| 9:15 AM 9:30 AM | 0 | 71 87 | 1 2 | 0 | 1 0 | 84 115 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 157 204 |
| 9:45 AM | Ö | 72 | 2 | 0 | 0 | 104 | 0 | 0 | 0 | Ö | Ö | 0 | 1 | Ö | 2 | Ö | 181 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 1656 | 28 | 0 | 10 | 1736 | 0 | 1 | 0 | 0 | 0 | 0 | 3 | 0 | 5 | 0 | 3439 |
| APPROACH %'s : | 0.00% | 98.34% | 1.66% | 0.00% | 0.57% | 99.37% | 0.00% | 0.06% | | | | | 37.50% | 0.00% | 62.50% | 0.00% | TOTAL |
| PEAK HR : PEAK HR VOL : | 0 | 07:30 AM - 483 | 18 | 0 | 5 | 538 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | TOTAL 1046 |
| PEAK HR FACTOR : | 0.000 | 0.856 | 0.500 | 0.000 | 0.313 | 0.796 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.250 | 0.000 | 0.250 | 0.000 | 0.838 |
| | | 0.8 | /6 | | | 0.80 | J3 | | | | | | | 0.5 | JU | | |
| NOON | _ | NORTH | | _ | | SOUTH | | _ | | | BOUND | | | WESTE | | _ | |
| NOON | 0 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 1 WT | 0 WR | 0 WU | TOTAL |
| 10:00 AM | 0 | 98 | 0 | 0 | 0 | 103 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 201 |
| 10:15 AM 10:30 AM | 0 | 89 79 | 0 0 | 0 | 0 | 91 86 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 180 165 |
| 10:45 AM | 0 | 75 | 0 | 0 | 0 | 91 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 168 |
| 11:00 AM 11:15 AM | 0 | 64 92 | 0 2 | 0 | 0 | 139 124 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 206 219 |
| 11:30 AM | 0 | 104 | 0 | 0 | 1 | 112 | 0 | 0 | 0 | 0 | 0 | Ō | 3 | 0 | 1 | 0 | 221 |
| 11:45 AM 12:00 PM | 0 | 95 104 | 0 | 0 | 0 | 80 89 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 1 | 0 | 182 194 |
| 12:15 PM | 0 | 86 | 1 | 1 | Ō | 93 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 184 |
| 12:30 PM 12:45 PM | 0 | 91 94 | 3 | 0 | 0 | 83 74 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 177 171 |
| 1:00 PM | 0 | 84 | 0 | 1 | 2 | 82 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 169 |
| 1:15 PM 1:30 PM | 0 | 92 144 | 1 2 | 0 | 0 | 142 178 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 2 2 | 0 | 0 1 | 0 | 237 327 |
| 1:45 PM | Ö | 143 | 2 | Ö | 2 | 159 | 0 | Ö | 0 | Ö | Ö | 0 | 2 | Ö | Ō | Ö | 308 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 1534 | 15 | 2 | 5 | 1726 | 0 | 0 | 0 | 0 | 0 | 0 | 20 | 0 | 7 | 0 | 3309 |
| APPROACH %'s : PEAK HR : | 0.00% | 98.90% 01:00 PM - | 0.97% | 0.13% | 0.29% | 99.71% | 0.00% | 0.00% | | | | | 74.07% | 0.00% | 25.93% | 0.00% | TOTAL |
| PEAK HR VOL : | 0 | 463 | 5 | 1 | 4 | 561 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 1 | 0 | 1041 |
| PEAK HR FACTOR : | 0.000 | 0.804 | 0.625 03 | 0.250 | 0.500 | 0.788 | 0.000 94 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 | 0.000 | 0.250 83 | 0.000 | 0.796 |
| | | | | | | | | | | E10E | | | | | | | |
| PM | 0 | NORTH 2 | 0 BOOND | 0 | 0 | SOUTHI 2 | 0 BOOND | 0 | 0 | 0 0 | BOUND 0 | 0 | 0 | WESTE 1 | 0 0 | 0 | |
| 2:00 PM | NL | NT | NR | NU | SL | ST | SR 0 | SU | EL 0 | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 2:15 PM | 0 | 99 88 | 2 1 | 0 | 2 1 | 126 123 | 0 | 0 | 0 | 0 0 | 0 0 | 0 | 1 0 | 0 0 | 2 0 | 0 | 232 213 |
| 2:30 PM | 0 | 114 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 262 |
| 2:45 PM 3:00 PM | 0 | 102 106 | 0 | 0 | 0 | 111 113 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 214 219 |
| 3:15 PM | 0 | 103 | 0 | 0 | 0 | 147 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 251 |
| 3:30 PM 3:45 PM | 0 | 109 111 | 0 1 | 0 | 0 | 137 172 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 1 | 0 0 | 0 1 | 0 | 246 286 |
| 4:00 PM | 0 | 132 | 2 | 0 | 0 | 141 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 278 |
| 4:15 PM 4:30 PM | 0 | 138 157 | 0 0 | 0 | 0 1 | 145 126 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 2 | 0 0 | 0 | 0 0 | 285 286 |
| 4:45 PM | 0 | 163 | 0 | 0 | 0 | 111 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 279 |
| 5:00 PM 5:15 PM | 0 | 141 136 | 1 0 | 0 | 0 | 136 137 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 4 1 | 0 0 | 3 0 | 0 | 285 274 |
| 5:30 PM | 0 | 126 | 0 | 1 | 0 | 131 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 259 |
| 5:45 PM | 0 | 108 | 0 | 0 | 0 | 140 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 251 |
| TOTAL VOLUMES | NL 0 | NT 1022 | NR | NU | SL | ST | SR | SU | EL | ET | ER 0 | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 0.00% | 1933 99.54% | 7 0.36% | 2 0.10% | 4 0.19% | 2144 99.81% | 0 0.00% | 0 0.00% | 0 | 0 | 0 | 0 | 21 70.00% | 0 0.00% | 9 30.00% | 0 0.00% | 4120 |
| PEAK HR: | | 03:45 PM - | 04:45 PM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0.000 | 538 0.857 | 3 0.375 | 0 0.000 | 1 0.250 | 584 0.849 | 0 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 6 0.750 | 0 0.000 | 3 0.750 | 0.000 | 1135 |
| | | 0.8 | | | | 0.8 | | | | | | | | 0.7 | | | 0.992 |
| | | | | | | | | | | | | | | | | | |

Location: CR J19/Rd 80/N Plaza Dr & California Dairies Dwy City: Visalia Control: No Control

Data - HT

| C-030 AR | NS/EW Streets: | (| CR J19/Rd 80 | D/N Plaza D | r | C | R J19/Rd 80 |)/N Plaza D | r | | California I | Dairies Dwy | | | California | Dairies Dwy | | |
|--|------------------|-------|--------------|-------------|-------|-------|-------------|-------------|-------|-------|--------------|-------------|-------|-------|------------|-------------|---------|--------------|
| Max. No. No. | | | NORTH | BOUND | | | SOUTH | BOUND | | | EAST | BOUND | | | WEST | BOUND | | |
| COLOMB 0 15 0 0 0 7 0 0 0 0 0 0 | AM | | | | | | | | | | | | | | | | | |
| SISS AM | 6:00 AM | | | | | | | | | | | | | | | | | TOTAL 22 |
| S-SS AM | 6:15 AM | | | Ō | | | | | | | | | | | | | ō | 30 |
| 7-30 AM | 6:30 AM | | 17 | | | | | | | | | | | | - | | 0 | 28 |
| 7-35 AM 0 12 0 0 0 15 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | | | | | | | | | | | | 32 44 |
| 7-33 AM | | | | | | | | | | | | | | | | | | 27 |
| SCO AM 0 25 0 0 0 0 0 0 0 0 0 | 7:30 AM | | | | | | 15 | | | | | | | | Ö | | | 32 |
| S15 AM 0 20 0 0 0 0 10 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | • | | | | | | | | | • | | | | 30 |
| R330 AM 0 20 0 0 0 0 11 1 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | | | | | | | | | | | | 46 30 |
| Section Sect | | | | | | | | | | | | | | | | | | 31 |
| 9-15 AM 9-30 AM 0 215 0 0 0 0 39 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | 23 | | | | | | | | | | | 39 |
| 9-33 AM 9-45 AM 0 22 0 0 0 0 46 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | 22 | | | | | | | | | | | 42 55 |
| 9-45 AM 0 13 0 0 16 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | | | | | | | | | | | | | | | 68 |
| TOTAL VOLUMES: 0.00% 0.0 | 9:45 AM | | | | | | 16 | | | Ö | | | | | | | | 29 |
| TOTAL VOLUMES: 0.00% 0.0 | | | | | | | | | | | | | | | | | | |
| APPROACH *Ws: 0.00% 100.00% 0. | TOTAL VOLUMES. | | | | | | | | | | | | | | | | | TOTAL 585 |
| PEAK HR 18: 07:30 AM - 08:30 AM PEAK HR 74CTOR: 0.000 0.22 | | | | | | | | | | U | U | U | U | U | U | U | U | 363 |
| PEAK HR FACTOR: 0.000 0.820 0.000 0. | PEAK HR : | | 07:30 AM - | 08:30 AM | | | | | | | | | | | | | | TOTAL |
| NOON | | | | | | | | | | | | | | | | | | 138 |
| NOON | PEAK HR FACTOR : | 0.000 | | 0.000 | 0.000 | 0.000 | | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.750 |
| NOON | | | υ.8 | 20 | | | 0.6 | U/ | | | | | | | | | | |
| NIL NTT NR NU SL ST SR SU EL ET ER EU WIL NTT WR WU TT | | | | | | | | | | | | | | | | | | |
| 10:00 AM | NOON | | | | | | | | | | | | | | | | | TOTAL |
| 10:15 AM | 10:00 AM | | | | | | | | | | | | | | | | | TOTAL 26 |
| 10:45 AM | | | | | | | | | | | | | | | | | | 36 |
| 11:00 AM | | • | | | • | | | | • | | | | | | • | | | 50 |
| 11:15 AM | | | | | | | | | | | | | | | | | | 43 34 |
| 11:30 AM | | | | | | | | | | | | | | | | | | 38 |
| 12:00 PM | 11:30 AM | 0 | 21 | 0 | | 0 | 24 | | 0 | 0 | 0 | | 0 | 0 | | | 0 | 45 |
| 12:15 PM | 11:45 AM | | | | | | | | | | | | | | | | | 30 |
| 12:30 PM | | | | | | | | | | | | | | | - | | | 42 40 |
| 12:45 PM | | • | | | | | | | | | | | | | • | | | 26 |
| 1:15 PM | 12:45 PM | | 14 | | | | | | | | | | | _ | | | 0 | 28 |
| 1:30 PM | | | | | | | | | | | | | | | | | | 24 26 |
| TOTAL VOLUMES: NIL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TO SL ST SR SU O O O O O O O O O | | | | | | | | | | | | | | | | | | 33 |
| TOTAL VOLUMES: 0 289 | 1:45 PM | | | | | | 17 | | | Ō | | | Ō | | | | | 35 |
| TOTAL VOLUMES: 0 289 | | NII | NIT | ND | NIII | CI | CT | CD | CII | | | - FD | FII | 14/1 | VA/T | WD | VA/II I | TOTAL |
| APPROACH %s: 0.00% 100.00% 0.0 | TOTAL VOLUMES : | | | | | | | | | | | | | | | | | 556 |
| PEAK HR VOL PEAK HR FACTOR 0.000 0.889 0.000 | APPROACH %'s: | | | | | | | | | Ů | Ü | · | · | Ů | ŭ | · | · | |
| PEAK HR FACTOR: 0.000 0.889 0.0000 0.000 0.000 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00 | | | | | _ | | | | _ | _ | | | | _ | | | | TOTAL |
| PM 0 NORTHBOUND 0 0 2 0 0 0 0 0 0 0 0 0 0 1 0 0 0 0 0 0 | | | | 0 | | | | | | | | | | | | | | 118 |
| PM | PLAKTIK PACTOR. | 0.000 | | 89 | 0.000 | 0.000 | | | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.843 |
| PM | | | | | | | | | | | | | | | | | | |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TT 2:00 PM 0 24 0 0 0 0 18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DM | 0 | | | 0 | 0 | | | 0 | 0 | | | 0 | 0 | | | 0 | |
| 2:00 PM | FIVI | | | | | | | | | | | | | | | | | TOTAL |
| 2:30 PM 0 15 0 0 0 13 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 0 | 24 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 |
| 2:45 PM | 2:15 PM | | | | | | | | | | | | | | | | | 39 28 |
| 3:00 PM | | | | | | | | | | | | | | | | | | 38 |
| 3:30 PM 0 13 0 0 0 18 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 3:00 PM | 0 | 13 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 33 |
| 3:45 PM | 3:15 PM | | 14 | | | | | | | | | | | | | | | 32 |
| 4:00 PM 0 24 0 0 0 16 0 | | - | | | | | | | | | | | | | - | | | 31 28 |
| 4:15 PM 0 23 0 0 0 20 | | | 24 | 0 | | 0 | | | 0 | 0 | | | | | | 0 | 0 | 40 |
| 4:45 PM 0 14 0 0 17 0 | 4:15 PM | | 23 | 0 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 |
| S:00 PM | | | | | | | | | | | | | | | | | | 26 31 |
| 5:15 PM 0 11 0 0 0 15 0 | | | | | | | | | | | | | | | | | | 33 |
| 5:45 PM 0 12 0 0 0 9 0 0 0 0 0 0 0 0 0 0 0 0 | 5:15 PM | 0 | 11 | 0 | | 0 | 15 | 0 | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | 26 |
| | | | | | | | | | | | | | | | | | | 24 |
| NL NT NR NU SL ST SR SU EL ET ER EU WL WT WR WU TO | 5:45 PM | 0 | 12 | 0 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 |
| | | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES: 0 258 0 0 0 257 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | 0 | 258 | 0 | 0 | 0 | 257 | 0 | 0 | | | | | | | | | 515 |
| APPROACH %'s: 0.00% 100.00% 0.00% 0.00% 0.00% 0.00% 0.00% 0.00% | | | | | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | | | | | | | TOTAL |
| | | | | | 0 | 0 | 65 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | TOTAL 137 |
| PEAK HR FACTOR: 0.000 0.750 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 | | | | | | | 0.813 | 0.000 | | | | | | | | | | 0.797 |
| 0.750 0.813 0. | | | | | | | | | | | | | | | | | | 0.797 |

Location: CR J19/Rd 80/N Plaza Dr & California Dairies Dwy City: Visalia Control: No Control

Data - Bikes

| NS/EW Streets: | C | R J19/Rd 8 | D/N Plaza D | r | C | R J19/Rd 8 | 0/N Plaza D | r | | California I | Dairies Dwy | | | California I | Dairies Dwy | | |
|-----------------------------------|------------|-----------------------|-------------------|------------|------------|------------|-------------|------------|---------|--------------|-------------|------------|---------|--------------|-------------|------------|--------|
| A B.4 | 0 | | BOUND | • | 0 | | IBOUND | 0 | | | BOUND | 0 | | | BOUND | 0 | |
| AM | 0 NL | 2 NT | NR | 0 NU | 0 SL | 2 ST | 0 SR | SU | 0 EL | 0 ET | ER | 0 EU | 0 WL | 1 WT | 0 WR | WU | TOTAL |
| 6:00 AM 6:15 AM | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | Ō | 0 | 0 | Ō | 0 | 0 | 0 | Ō | 0 | 0 | Ö | Ö | 0 | ō | Ō | 0 | 0 |
| 8:00 AM 8:15 AM | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | Ō | Ō | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ō | 0 | 0 | 0 | Ō | 0 | 0 | 0 |
| 8:45 AM 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM 9:30 AM | 0 0 | 0 1 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | ŏ | Ō | Ö | ő | Ö | ŏ | Ö | Ö | ő | Ö | Ö | Ö | Ö | Ö | ő | ő | Ô |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 0.00% | 1 100.00% | 0 0.00% | 0 0.00% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| PEAK HR : | | 07:30 AM - | 08:30 AM | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 |
| T ZARTINET ACTOR. | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | NORTH | BOUND | | | | IBOUND | | | EAST | BOUND | | | WEST | BOUND | | |
| NOON | 0 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 1 WT | 0 WR | 0 WU | TOTAL |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM 10:30 AM | 0 0 | 0 0 | 0 0 | 0 | 0 | 0 1 | 0 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 |
| 10:45 AM 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM 11:45 AM | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM 1:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM 1:45 PM | 0 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| APPROACH %'s : PEAK HR : | | 01:00 PM - | 02:00 PM | | 0.00% | 100.00% | 0.00% | 0.00% | | | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0.000 | 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 |
| PLAKTIK FACTOR . | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | | BOUND | | | | IBOUND | | | | BOUND | | | WEST | BOUND | | |
| PM | 0 NL | 2 NT | 0 NR | 0 NU | 0 SL | 2 ST | 0 SR | 0 SU | 0 EL | 0 ET | 0 ER | 0 EU | 0 WL | 1 WT | 0 WR | 0 WU | TOTAL |
| 2:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:15 PM 2:30 PM | 0 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 |
| 2:45 PM 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | Ō | Ō | Ō | Ō | 0 | Ö | Ō | Ō | Ö | ō | Ö | Ö | Ö | ō | Ō | Ō | 0 |
| 3:30 PM 3:45 PM | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 |
| 4:00 PM 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | Ö | ō | 0 | 0 | 0 | Ō | Ö | 0 | 0 | Ö | Ö | 0 | 0 | Ō | Ō | 0 |
| 4:45 PM 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM 5:45 PM | 0 0 | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 | WR 0 | WU 0 | 3 |
| APPROACH %'s : PEAK HR : | 0.00% | 100.00% 03:45 PM - | 0.00% 04:45 PM | 0.00% | 0.00% | 100.00% | 0.00% | 0.00% | | | _ | | | | _ | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR : | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | |
| | | | | | | | | | | | | | | | | | |

Location: CR J19/Rd 80/N Plaza Dr & California Dairies Dwy **City:** Visalia

Project ID: 22-090052-004 **Date:** 4/21/2022

Data - Pedestrians (Crosswalks)

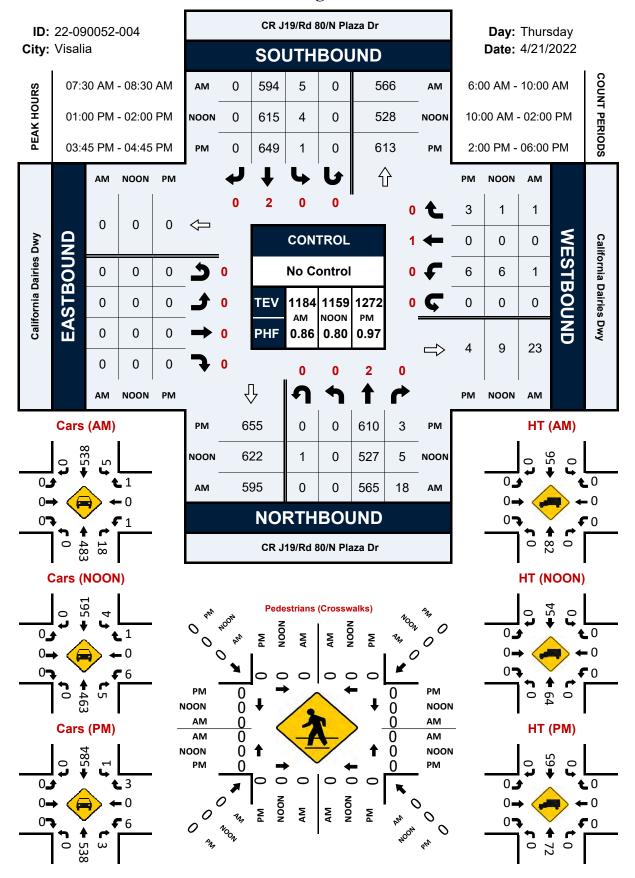
| NS/EW Streets: | CR J19/Rd | 80/N Plaza Dr | CR J19/Rd | 80/N Plaza Dr | California | Dairies Dwy | California D | airies Dwy | |
|-----------------------------------|-----------|---------------|-----------|---------------|------------|--------------|--------------|------------|-------|
| ARA | NORT | 'H LEG | SOUT | 'H LEG | EAS | T LEG | WEST | LEG | |
| AM | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 6:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 | 0 | 0 | 0 | 0 0.00% | 1 100.00% | 0 | 0 | 1 |
| PEAK HR: | 07:30 AM | - 08:30 AM | | | | | | | TOTAL |
| PEAK HR VOL : PEAK HR FACTOR : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| NOON | NORT | 'H LEG | SOUT | H LEG | EAST | Γ LEG | WEST | T LEG | |
|-----------------|----------|------------|------|-------|------|-------|------|-------|-------|
| NOON | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 10:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| APPROACH %'s: | | | | | | | | | |
| PEAK HR: | 01:00 PM | - 02:00 PM | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR: | | | | | | | | | |
| | | | | | | | | | |

| 2:00 PM 2:15 PM | EB 0 | WB | EB | | | | | | |
|--------------------|------------|----------|----|----|----|----|----|----|-------|
| | 0 | | LD | WB | NB | SB | NB | SB | TOTAL |
| 2-15 DM | | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2.13 [11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| APPROACH %'s: | | | | | | | | | |
| PEAK HR: | 03:45 PM - | 04:45 PM | | | | | | | TOTAL |
| PEAK HR VOL : | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| PEAK HR FACTOR: | | | | | | | | | |

CR J19/Rd 80/N Plaza Dr & California Dairies Dwy

Peak Hour Turning Movement Count



Location: CR J19/Rd 80/N Plaza Dr & W Goshen Ave City: Visalia Control: Signalized

| _ | | | | | | | | Data - | · Total | | | | | | | | |
|------------------|--------|-------------|-------------|-------|--------|------------|-------------|--------|---------|---------|--------|-------|--------|---------|--------|-------|-------|
| NS/EW Streets: | CF | R J19/Rd 80 | /N Plaza Dr | | CF | 319/Rd 80, | /N Plaza Di | | | W Goshe | en Ave | | | W Goshe | n Ave | | |
| | | NORTH | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTE | OUND | | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| 7 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 25 | 113 | 13 | 2 | 34 | 85 | 9 | 0 | 6 | 21 | 33 | 0 | 4 | 22 | 15 | 1 | 383 |
| 7:15 AM | 32 | 106 | 19 | 4 | 24 | 88 | 8 | 0 | 8 | 28 | 36 | 1 | 12 | 30 | 21 | 1 | 418 |
| 7:30 AM | 34 | 140 | 16 | 5 | 29 | 126 | 11 | 0 | 4 | 42 | 59 | 0 | 8 | 25 | 19 | 6 | 524 |
| 7:45 AM | 31 | 131 | 14 | 4 | 36 | 126 | 10 | 0 | 5 | 41 | 68 | 0 | 16 | 25 | 20 | 4 | 531 |
| 8:00 AM | 42 | 110 | 19 | 4 | 26 | 104 | 11 | 0 | 8 | 46 | 29 | 0 | 17 | 34 | 21 | 7 | 478 |
| 8:15 AM | 55 | 114 | 15 | 5 | 20 | 92 | 9 | 0 | 9 | 22 | 27 | 0 | 16 | 37 | 26 | 4 | 451 |
| 8:30 AM | 24 | 97 | 8 | 2 | 22 | 85 | 9 | 0 | 3 | 27 | 28 | 0 | 15 | 24 | 18 | 9 | 371 |
| 8:45 AM | 30 | 90 | 9 | 8 | 21 | 107 | 13 | 0 | 6 | 18 | 27 | 0 | 18 | 21 | 12 | 3 | 383 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 273 | 901 | 113 | 34 | 212 | 813 | 80 | 0 | 49 | 245 | 307 | 1 | 106 | 218 | 152 | 35 | 3539 |
| APPROACH %'s: | 20.67% | 68.21% | 8.55% | 2.57% | 19.19% | 73.57% | 7.24% | 0.00% | 8.14% | 40.70% | 51.00% | 0.17% | 20.74% | 42.66% | 29.75% | 6.85% | |
| PEAK HR : | | 7:30 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 162 | 495 | 64 | 18 | 111 | 448 | 41 | 0 | 26 | 151 | 183 | 0 | 57 | 121 | 86 | 21 | 1984 |
| PEAK HR FACTOR : | 0.736 | 0.884 | 0.842 | 0.900 | 0.771 | 0.889 | 0.932 | 0.000 | 0.722 | 0.821 | 0.673 | 0.000 | 0.838 | 0.818 | 0.827 | 0.750 | 0.934 |
| | | 0.94 | 4/ | | | 0.87 | 2 | | | 0.78 | 39 | | | 0.85 | 8 | | |
| | | NORTH | BOLIND | | | SOUTHE | ROLIND | | | EASTB | OLIND | | | WESTE | OLIND | | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| 1 171 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 29 | 116 | 19 | 7 | 33 | 124 | 12 | 0 | 14 | 66 | 63 | 0 | 22 | 36 | 23 | 3 | 567 |
| 4:15 PM | 32 | 122 | 16 | 10 | 30 | 132 | 10 | 0 | 17 | 50 | 36 | 0 | 13 | 34 | 24 | 2 | 528 |
| 4:30 PM | 32 | 124 | 13 | 6 | 29 | 111 | 6 | 0 | 22 | 57 | 75 | 0 | 16 | 36 | 25 | 2 | 554 |
| 4:45 PM | 38 | 132 | 9 | 6 | 19 | 106 | 2 | 0 | 17 | 38 | 37 | 0 | 24 | 31 | 27 | 3 | 489 |
| 5:00 PM | 33 | 117 | 17 | 4 | 17 | 147 | 6 | 0 | 21 | 52 | 55 | 0 | 22 | 34 | 22 | 3 | 550 |
| 5:15 PM | 37 | 129 | 11 | 2 | 14 | 124 | 7 | 0 | 7 | 36 | 32 | 0 | 17 | 30 | 11 | 3 | 460 |
| 5:30 PM | 37 | 108 | 16 | 4 | 21 | 119 | 6 | 0 | 9 | 39 | 27 | 0 | 14 | 29 | 20 | 6 | 455 |
| 5:45 PM | 21 | 98 | 7 | 4 | 29 | 124 | 3 | 0 | 6 | 23 | 27 | 0 | 17 | 16 | 18 | 4 | 397 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 259 | 946 | 108 | 43 | 192 | 987 | 52 | 0 | 113 | 361 | 352 | 0 | 145 | 246 | 170 | 26 | 4000 |
| APPROACH %'s: | 19.10% | 69.76% | 7.96% | 3.17% | 15.60% | 80.18% | 4.22% | 0.00% | 13.68% | 43.70% | 42.62% | 0.00% | 24.70% | 41.91% | 28.96% | 4.43% | |
| PEAK HR : | | 04:00 PM - | | 20 | | 470 | | | =0 | | | | | 400 | | 4.0 | TOTAL |
| PEAK HR VOL : | 131 | 494 | 57 | 29 | 111 | 473 | 30 | 0 | 70 | 211 | 211 | 0 | 75 | 137 | 99 | 10 | 2138 |
| PEAK HR FACTOR: | 0.862 | 0.936 | 0.750 | 0.725 | 0.841 | 0.896 | 0.625 | 0.000 | 0.795 | 0.799 | 0.703 | 0.000 | 0.781 | 0.951 | 0.917 | 0.833 | 0.943 |
| | | 0.96 | 51 | | | 0.89 | 2 | | | 0.79 | 99 | | | 0.94 | 14 | | |

Location: CR J19/Rd 80/N Plaza Dr & W Goshen Ave City: Visalia Control: Signalized

Data - Cars

| _ | | | | | | | | Data · | - Cars | | | | | | | | |
|---------------------------|---------|----------------------|-------------|---------|---------|--------------|-------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------|
| NS/EW Streets: | CF | R J19/Rd 80 | /N Plaza Dr | | CF | R J19/Rd 80, | /N Plaza Di | | | W Goshe | en Ave | | | W Goshe | en Ave | | |
| | | NORTHI | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTB | OUND | | |
| AM | 1 NL | 2 NT | 1 NR | 0 NU | 1 SL | 2 ST | 1 SR | 0 SU | 1 EL | 2 ET | 1 ER | 0 EU | 1 WL | 2 WT | 1 WR | 0 WU | TOTAL |
| 7:00 AM | 21 | 91 | 9 | 1 | 30 | 75 | 6 | 0 | 6 | 20 | 29 | 0 | 3 | 19 | 13 | 1 | 324 |
| 7:15 AM | 31 | 101 | 14 | 4 | 20 | 76 | 8 | 0 | 6 | 28 | 33 | 1 | 10 | 29 | 17 | 1 | 379 |
| 7:30 AM | 32 | 129 | 15 | 5 | 28 | 116 | 10 | 0 | 4 | 41 | 57 | 0 | 7 | 23 | 14 | 6 | 487 |
| 7:45 AM | 28 | 117 | 14 | 4 | 35 | 119 | 10 | 0 | 3 | 34 | 64 | 0 | 13 | 24 | 18 | 4 | 487 |
| 8:00 AM | 40 | 89 | 16 | 4 | 23 | 93 | 8 | 0 | 6 | 44 | 26 | 0 | 17 | 33 | 19 | 7 | 425 |
| 8:15 AM | 53 | 101 | 15 | 5 | 16 | 85 | 8 | 0 | 7 | 20 | 25 | 0 | 13 | 34 | 21 | 4 | 407 |
| 8:30 AM | 22 | 83 | 7 | 2 | 22 | 72 | 8 | 0 | 2 | 23 | 23 | 0 | 9 | 22 | 14 | 9 | 318 |
| 8:45 AM | 29 | 78 | 7 | 8 | 18 | 92 | 8 | 0 | 4 | 15 | 24 | 0 | 16 | 20 | 10 | 3 | 332 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 256 | 789 | 97 | 33 | 192 | 728 | 66 | 0 | 38 | 225 | 281 | 1 | 88 | 204 | 126 | 35 | 3159 |
| APPROACH %'s: PEAK HR: | 21.79% | 67.15% 07:30 AM - | 8.26% | 2.81% | 19.47% | 73.83% | 6.69% | 0.00% | 6.97% | 41.28% | 51.56% | 0.18% | 19.43% | 45.03% | 27.81% | 7.73% | TOTAL |
| PEAK HK : | 153 | 436 | 60 60 | 18 | 102 | 413 | 36 | 0 | 20 | 139 | 172 | 0 | 50 | 114 | 72 | 21 | 1806 |
| PEAK HR VOL : | 0.722 | 0.845 | 0.938 | 0.900 | 0.729 | 0.868 | 0.900 | 0.000 | 0.714 | 0.790 | 0.672 | 0.000 | 0.735 | 0.838 | 0.857 | 0.750 | 1000 |
| PEAK HK FACTOR : | 0.722 | 0.043 | | 0.900 | 0.729 | 0.84 | | 0.000 | 0.714 | 0.790 | | 0.000 | 0.733 | 0.84 | | 0.730 | 0.927 |
| | | 0151 | • | | | 0.0 | | | | 0102 | • | | | 0.0 | | | |
| | | NORTH | BOUND | | | SOUTHE | BOUND | | | EASTB | OUND | | | WESTB | OUND | | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 26 | 98 | 16 | 7 | 31 | 113 | 10 | 0 | 12 | 63 | 58 | 0 | 20 | 32 | 20 | 3 | 509 |
| 4:15 PM | 31 | 106 | 14 | 10 | 26 | 118 | 8 | 0 | 15 | 45 | 30 | 0 | 12 | 32 | 18 | 2 | 467 |
| 4:30 PM | 31 | 116 | 12 | 6 | 24 | 102 | 4 | 0 | 21 | 52 | 72 | 0 | 13 | 35 | 23 | 2 | 513 |
| 4:45 PM | 35 | 121 | 7 | 6 | 17 | 91 | 2 | 0 | 14 | 36 | 36 | 0 | 23 | 29 | 24 | 3 | 444 |
| 5:00 PM | 31 | 102 | 15 | 4 | 14 | 142 | 3 | 0 | 17 | 52 | 53 | 0 | 19 | 30 | 21 | 3 | 506 |
| 5:15 PM | 36 | 119 | 10 | 2 | 12 | 113 | 4 | 0 | 6 | 34 | 31 | 0 | 17 | 27 | 11 | 3 | 425 |
| 5:30 PM | 34 | 99 | 12 | 4 | 18 | 114 | 4 | 0 | 7 | 38 | 27 | 0 | 14 | 28 | 17 | 6 | 422 |
| 5:45 PM | 19 | 89 | 6 | 4 | 25 | 120 | 2 | 0 | 5 | 23 | 26 | 0 | 16 | 16 | 14 | 4 | 369 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 243 | 850 | 92 | 43 | 167 | 913 | 37 | 0 | 97 | 343 | 333 | 0 | 134 | 229 | 148 | 26 | 3655 |
| APPROACH %'s: | 19.79% | 69.22% | 7.49% | 3.50% | 14.95% | 81.74% | 3.31% | 0.00% | 12.55% | 44.37% | 43.08% | 0.00% | 24.95% | 42.64% | 27.56% | 4.84% | |
| PEAK HR : | | 04:00 PM - | | 20 | 00 | 424 | 24 | • | 63 | 100 | 100 | | 60 | 120 | 05 | 10 | TOTAL |
| PEAK HR VOL : | 123 | 441 | 49 | 29 | 98 | 424 | 24 | 0 | 62 | 196 | 196 | 0 | 68 | 128 | 85 | 10 | 1933 |
| PEAK HR FACTOR : | 0.879 | 0.911 | 0.766 | 0.725 | 0.790 | 0.898 | 0.600 | 0.000 | 0.738 | 0.778 | 0.681 | 0.000 | 0.739 | 0.914 | 0.885 | 0.833 | 0.942 |
| | | 0.95 | U | | | 0.88 | D | | | | | | | 0.92 | 1. | | |

Location: CR J19/Rd 80/N Plaza Dr & W Goshen Ave City: Visalia Control: Signalized

| _ | | | | | | | | Data | - HT | | | | | | | | |
|------------------|--------|------------|--------------|-------|--------|-----------|-------------|-------|--------|--------|-------------|-------|--------|--------|-------------|-------|-------|
| NS/EW Streets: | CR | J19/Rd 80 |)/N Plaza Dr | | CR | 319/Rd 80 | /N Plaza Dr | | | W Gosh | en Ave | | | W Gosh | en Ave | | |
| | | NORTH | BOUND | | | SOUTH | BOUND | | | EASTB | OUND | | | WESTE | BOUND | | |
| AM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 7:00 AM | 4 | 22 | 4 | 1 | 4 | 10 | 3 | 0 | 0 | 1 | 4 | 0 | 1 | 3 | 2 | 0 | 59 |
| 7:15 AM | 1 | 5 | 5 | 0 | 4 | 12 | 0 | 0 | 2 | 0 | 3 | 0 | 2 | 1 | 4 | 0 | 39 |
| 7:30 AM | 2 | 11 | 1 | 0 | 1 | 10 | 1 | 0 | 0 | 1 | 2 | 0 | 1 | 2 | 5 | 0 | 37 |
| 7:45 AM | 3 | 14 | 0 | 0 | 1 | 7 | 0 | 0 | 2 | | 4 | 0 | 3 | 1 | 2 | 0 | 44 |
| 8:00 AM | 2 | 21 | 3 | 0 | 3 | 11 | 3 | 0 | 2 | 2 | 3 | 0 | 0 | 1 | 2 | 0 | 53 |
| 8:15 AM | 2 | 13 | 0 | 0 | 4 | 7 | 1 | 0 | 2 | 2 | 2 | 0 | 3 | 3 | 5 | 0 | 44 |
| 8:30 AM | 2 | 14 | 1 | 0 | 0 | 13 15 | 5 | 0 | 1 | 3 | 5 3 | 0 | 6 | 2 | 4 | 0 | 53 |
| 8:45 AM | 1 | 12 | 2 | 0 | 3 | 15 | 5 | U | 2 | 3 | 3 | 0 | 2 | 1 | 2 | 0 | 51 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 17 | 112 | 16 | 1 | 20 | 85 | 14 | 0 | 11 | 20 | 26 | 0 | 18 | 14 | 26 | 0 | 380 |
| APPROACH %'s: | 11.64% | 76.71% | 10.96% | 0.68% | 16.81% | 71.43% | 11.76% | 0.00% | 19.30% | 35.09% | 45.61% | 0.00% | 31.03% | 24.14% | 44.83% | 0.00% | |
| PEAK HR : | | 7:30 AM - | | | | | | | | | | | | | | | TOTAL |
| PEAK HR VOL : | 9 | 59 | 4 | 0 | 9 | 35 | 5 | 0 | 6 | 12 | 11 | 0 | 7 | 7 | 14 | 0 | 178 |
| PEAK HR FACTOR : | 0.750 | 0.702 | 0.333 | 0.000 | 0.563 | 0.795 | 0.417 | 0.000 | 0.750 | 0.429 | 0.688 | 0.000 | 0.583 | 0.583 | 0.700 | 0.000 | 0.840 |
| | | 0.69 | 92 | | | 0.72 | 21 | | | 0.5 | 58 | | | 0.6 | 36 | | 0.010 |
| | | NORTH | BOLIND | | | SOUTH | ROLIND | | | EASTB | OUND | | | WESTE | ROLIND | | |
| PM | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | 1 | 2 | 1 | 0 | |
| 1 101 | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| 4:00 PM | 3 | 18 | 3 | 0 | 2 | 11 | 2 | 0 | 2 | 3 | 5 | 0 | 2 | 4 | 3 | 0 | 58 |
| 4:15 PM | 1 | 16 | 2 | 0 | 4 | 14 | 2 | 0 | 2 | 5 | 6 | 0 | 1 | 2 | 6 | 0 | 61 |
| 4:30 PM | 1 | 8 | 1 | 0 | 5 | 9 | 2 | 0 | 1 | 5 | 3 | 0 | 3 | 1 | 2 | 0 | 41 |
| 4:45 PM | 3 | 11 | 2 | 0 | 2 | 15 | 0 | 0 | 3 | 2 | 1 | 0 | 1 | 2 | 3 | 0 | 45 |
| 5:00 PM | 2 | 15 | 2 | 0 | 3 | 5 | 3 | 0 | 4 | 0 | 2 | 0 | 3 | 4 | 1 | 0 | 44 |
| 5:15 PM | 1 | 10 | 1 | 0 | 2 | 11 | 3 | 0 | 1 | 2 | 1 | 0 | 0 | 3 | 0 | 0 | 35 |
| 5:30 PM | 3 | 9 | 4 | 0 | 3 | 5 | 2 | 0 | 2 | 1 | 0 | 0 | 0 | 1 | 3 | 0 | 33 |
| 5:45 PM | 2 | 9 | 1 | 0 | 4 | 4 | 1 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 4 | 0 | 28 |
| | NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : | 16 | 96 | 16 | 0 | 25 | 74 | 15 | 0 | 16 | 18 | 19 | 0 | 11 | 17 | 22 | 0 | 345 |
| APPROACH %'s: | 12.50% | 75.00% | 12.50% | 0.00% | 21.93% | 64.91% | 13.16% | 0.00% | 30.19% | 33.96% | 35.85% | 0.00% | 22.00% | 34.00% | 44.00% | 0.00% | TOTAL |
| PEAK HR : | | 14:00 PM - | | _ | 42 | 40 | _ | | 0 | | | | - | ^ | | | TOTAL |
| PEAK HR VOL : | 8 | 53 | 8 | 0 | 13 | 49 | 6 | 0 | 8 | 15 | 15 | 0 | 7 | 9 | 14 | 0 | 205 |
| PEAK HR FACTOR : | 0.667 | 0.736 | 0.667 19 | 0.000 | 0.650 | 0.817 | 0.750 50 | 0.000 | 0.667 | 0.750 | 0.625 31 | 0.000 | 0.583 | 0.563 | 0.583 33 | 0.000 | 0.840 |

Location: CR J19/Rd 80/N Plaza Dr & W Goshen Ave City: Visalia Control: Signalized

| _ | | | | | | | | Data - | Bikes | | | | | | | | |
|--|-------------|--------------------------|------------------------|-------------|-------------|------------------|------------------|-------------|------------------|--------------------|------------------|------------------|-------------|-----------------|------------------|-------------|-------------|
| NS/EW Streets: | С | R J19/Rd 80 |)/N Plaza Dr | | CF | R J19/Rd 80 |)/N Plaza Di | , | | W Gosh | en Ave | | | W Gosł | nen Ave | | |
| AM | 1 NL | NORTH 2 NT | BOUND 1 NR | 0 NU | 1 SL | SOUTH 2 ST | BOUND 1 SR | 0 SU | 1 EL | EASTE 2 ET | OUND 1 ER | 0 EU | 1 WL | WEST 2 WT | BOUND 1 WR | 0 WU | TOTAL |
| 7:00 AM 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 0 |
| 7:30 AM 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM 8:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30 AM 8:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| TOTAL VOLUMES : APPROACH %'s : | NL 0 | NT 0 | NR 0 | NU 0 | SL 0 | ST 0 | SR 0 | SU 0 | EL 0 0.00% | ET 1 100.00% | ER 0 0.00% | EU 0 0.00% | WL 0 | WT 0 | WR 0 | WU 0 | TOTAL 1 |
| PEAK HR : PEAK HR VOL : PEAK HR FACTOR : | 0,000 | 07:30 AM - 0 0.000 | 0 0 0,000 | 0 0.000 | 0 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | 0 0.000 | TOTAL 0 |
| | | | | | | | | | | | | | | | | | |
| PM | 1 NL | NORTH 2 NT | BOUND 1 NR | 0 NU | 1 SL | SOUTH 2 ST | BOUND 1 SR | 0 SU | 1 EL | EASTE 2 ET | OUND 1 ER | 0 EU | 1 WL | WEST 2 WT | BOUND 1 WR | 0 WU | TOTAL |
| 4:00 PM 4:15 PM | 0 | 0 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 0 | 0 0 | 0 | 0 | 0 |
| 4:30 PM 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 3 |
| 5:00 PM 5:15 PM 5:30 PM 5:45 PM | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 | 0 0 0 |
| 3.43 FM | NL NL | NT | NR | NU | SL | ST | SR | SU | EL | ET | ER | EU | WL | WT | WR | WU | TOTAL |
| TOTAL VOLUMES : APPROACH %'s : | 0 0.00% | 0.00% | 1 100.00% | 0 0.00% | 1 33.33% | 1 33.33% | 0 0.00% | 1 33.33% | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| PEAK HR : PEAK HR VOL : PEAK HR FACTOR : | 0 | 04:00 PM - 0 0.000 | 05:00 PM 1 0.250 | 0 | 1 0.250 | 1 0.250 | 0 | 1 0.250 | 0 0.000 | 0 | 0 | 0 0.000 | 0 0.000 | 0 0.000 | 0 | 0 0.000 | TOTAL 4 |
| PEAK HR FACIUR : | 0.000 | 0.000 | | 0.000 | 0.230 | 0.250 | | 0.230 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.333 |

National Data & Surveying Services Intersection Turning

Location: CR J19/Rd 80/N Plaza Dr & W Goshen Ave

Movement Count
Project ID: 22-090052-005
Date: 4/21/2022

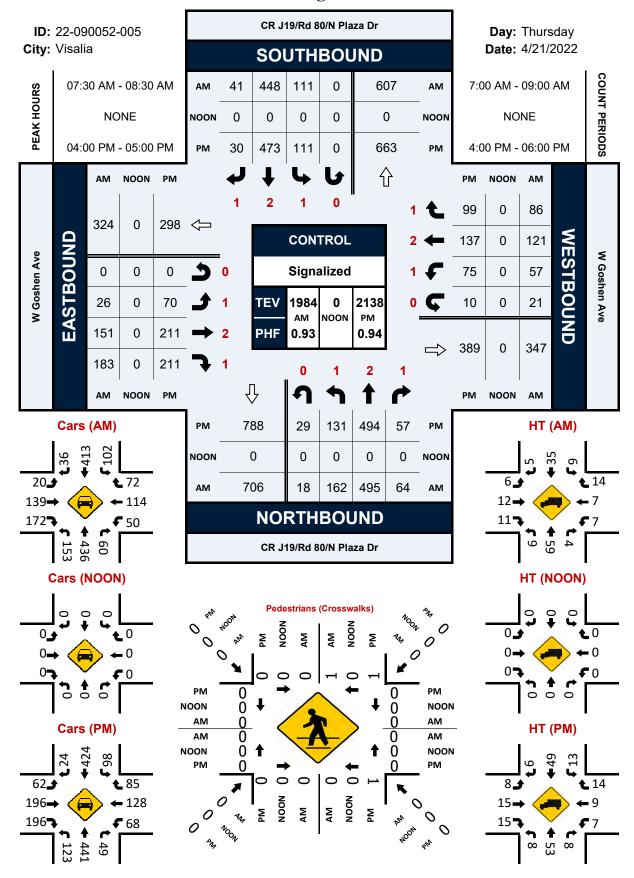
Data - Pedestrians (Crosswalks)

| NS/EW Streets: | CR J19/Rd | 80/N Plaza Dr | CR J19/Rd | 80/N Plaza Dr | W Gosh | ien Ave | W Gosh | nen Ave | |
|-----------------|------------------|---------------|-----------|---------------|---------|---------|--------|---------|-------|
| AM | NOR ⁻ | TH LEG | SOU | TH LEG | EAST | LEG | WES | Γ LEG | |
| Alvi | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:45 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45 AM | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 3 |
| APPROACH %'s: | 0.00% | 100.00% | 0.00% | 100.00% | 100.00% | 0.00% | | | |
| PEAK HR: | 07:30 AM | - 08:30 AM | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| PEAK HR FACTOR: | | 0.250 | | | | | | | 0.250 |
| | 0. | 250 | | | | | | | 0.250 |

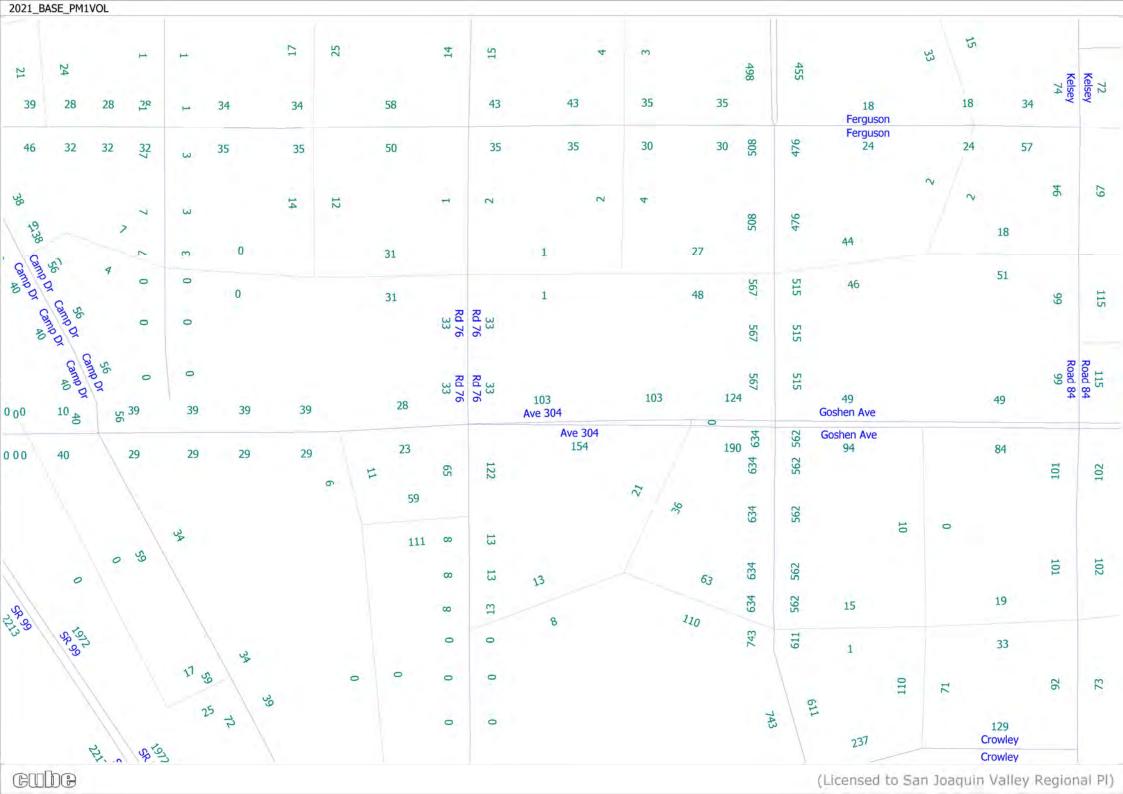
| PM | NORT | H LEG | SOUT | TH LEG | EAST | LEG | WEST | Γ LEG | |
|-----------------|----------|------------|-------|---------|---------|-------|------|-------|-------|
| PIVI | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| 4:00 PM | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 |
| 5:30 PM | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | | | | |
| | EB | WB | EB | WB | NB | SB | NB | SB | TOTAL |
| TOTAL VOLUMES: | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 5 |
| APPROACH %'s: | 66.67% | 33.33% | 0.00% | 100.00% | 100.00% | 0.00% | | | |
| PEAK HR: | 04:00 PM | - 05:00 PM | | | | | | | TOTAL |
| PEAK HR VOL: | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| PEAK HR FACTOR: | | 0.250 | | 0.250 | | | | | 0.250 |
| | 0.2 | 250 | 0. | 250 | | | | | 0.250 |

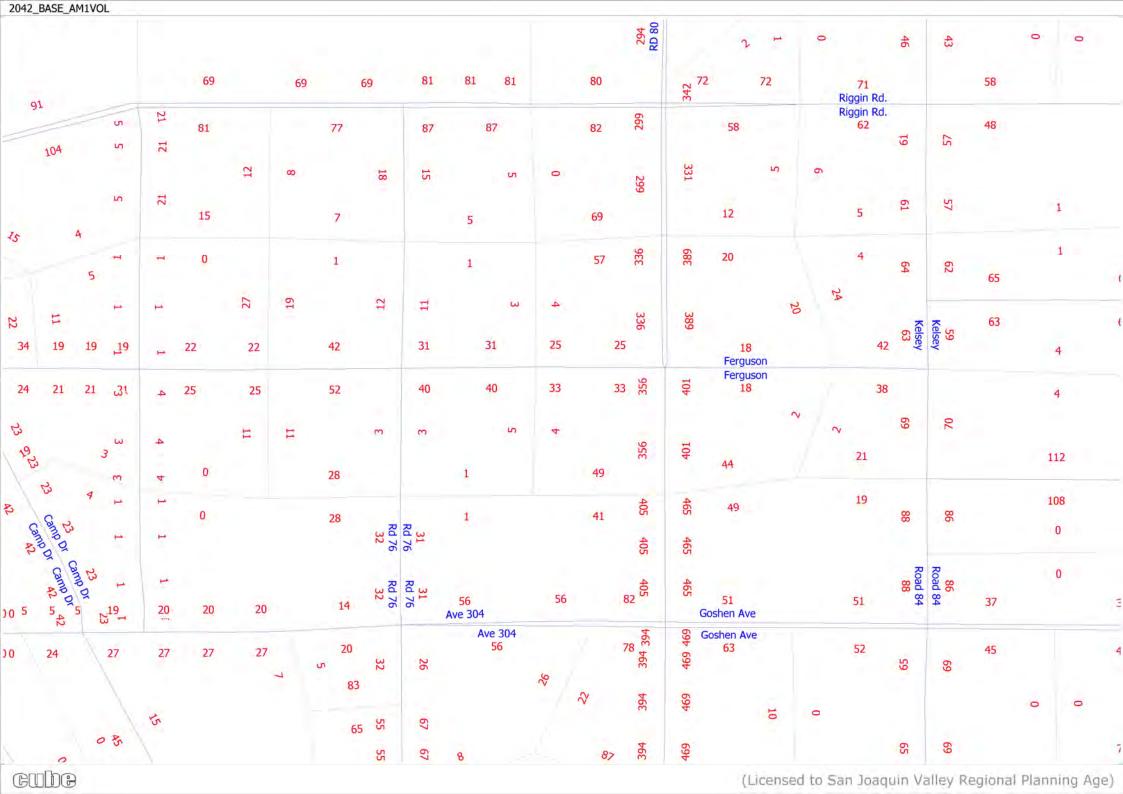
CR J19/Rd 80/N Plaza Dr & W Goshen Ave

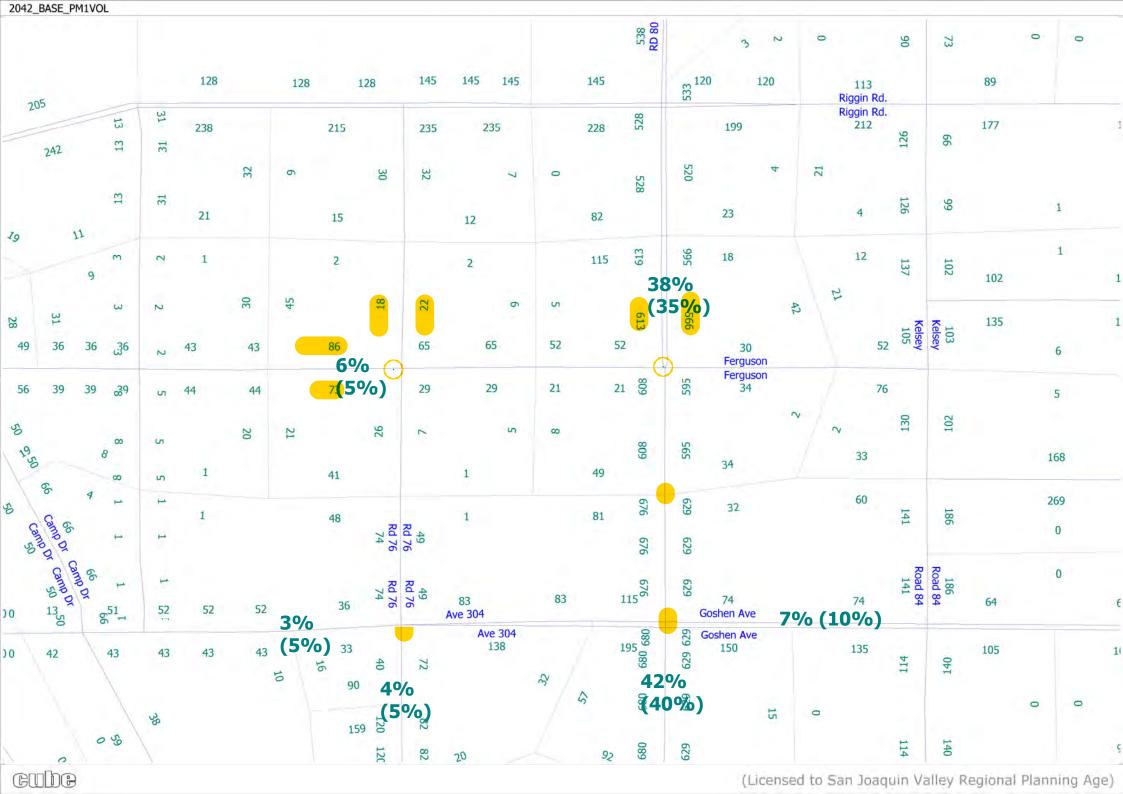
Peak Hour Turning Movement Count



| 2021_BA | ASE_A | M1V | OL | | | | | | | | | | | | | | | | | | | | |
|----------------|---------|-----------|----|---------|-----|----|----|---|----------|---|----------|-------|-------------|---------------|------|----|-------------|-------------|----------------------|----------|--------------------------|---------------|---------------|
| 15 28 | σ 15 | | 15 | 0 | 0 | 17 | , | | S | = | 28 | 80 | 20 | 20 | N 17 | 17 | 267 | 310 | 12 | ¥ 12 | | Kelsey 44 | 43 Kelsey |
| 20 | 17 | | 17 | 17 27 | 0 | 20 | | | 20 | | 35 | | 26 | 26 | 22 | 22 | | 318 | Ferguson Ferguson 12 | 12 | | | |
| 20 0200 | | | 2 | 2 | 4 | | Ō | | 7 | 7 | 17 | Ţ | - | m 1 | 2 | 27 | 279 | 318 | 45 | 2 2 | 19 | 48 | 20 |
| Camp Dr Carras | Campo | | 4 | 0 0 | 0 0 | | 0 | | | | 20 | Rd 76 | 19 Rd 76 | ì | | 21 | 320 320 | 370 370 | 51 | | 18 | 8 | 8 |
| 0 00 4 | Cal. 36 | Camp Dr 4 | | o 15 | 15 | | 15 | | 15 | | 11 | Rd 76 | 19 Rd 76 | 81 Ave 304 | 81 | 0 | 320 97 | 370 | 34 Goshen Ave | | 34 | Road 84 63 | 63 Road 84 |
| 000 | 22 | | | 22 | 22 | | 22 | | 22 | ō | 16 -> | 94 | 75 | Ave 304 75 | 4 | 15 | 346 346 346 | 414 414 414 | Goshen Ave 44 | | 36 | 28 | 63 |
| | | 0 | 0 | 22 | TA | | | | | | 47 | 7 7 2 | 5 5 | S | | 62 | 346 346 3 | 414 414 4 | 7 | 0 | 17 | 58 | 63 |
| TA S | Spor | 1652 | | | n | B | 4 | | | 0 | 0 | 0 0 | 0 | 1 | | 48 | 393 | 469 | 1 8 | 99 | 14 | 4 | 53 |
| | | 2 | | \$ | | 14 | 8 | 2 | | | | 0 | 0. | | | | 395 | | 113 | | 61 Crowley Crowley | | |
| GUI | he | | | | | | | | | | | | | | | | | | (Licensed to Sa | n Joaqui | n Valley | Region | al PI) |



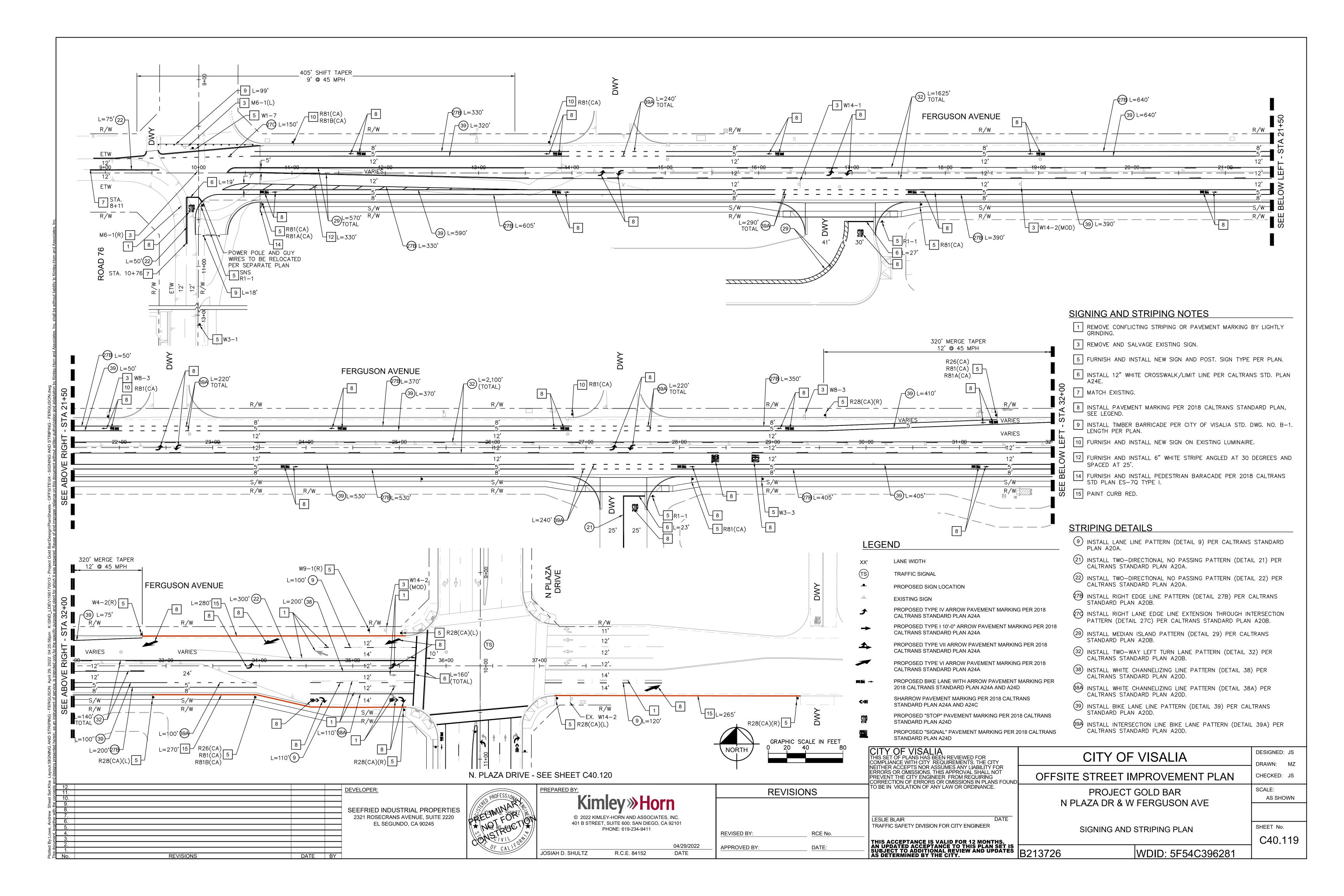


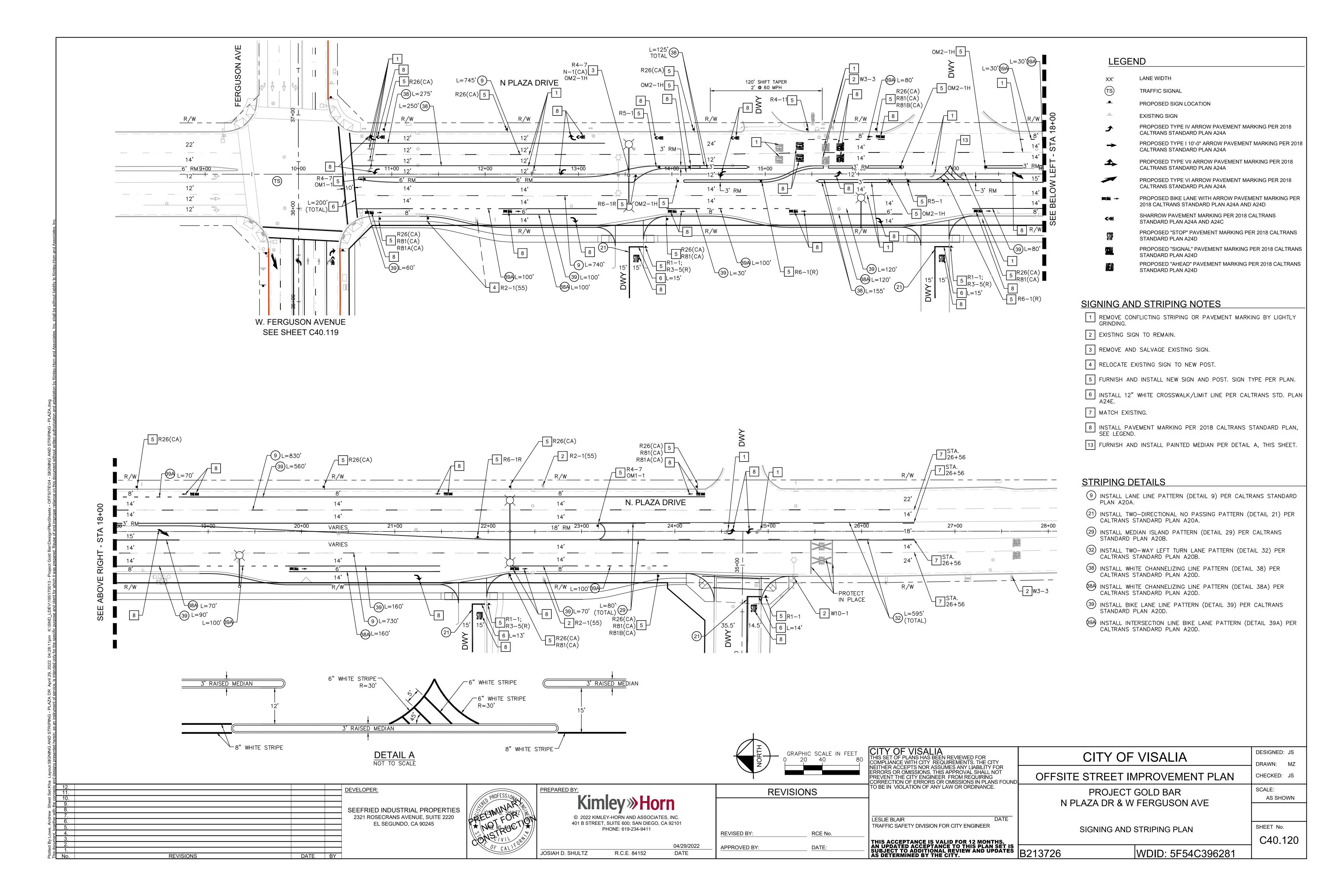


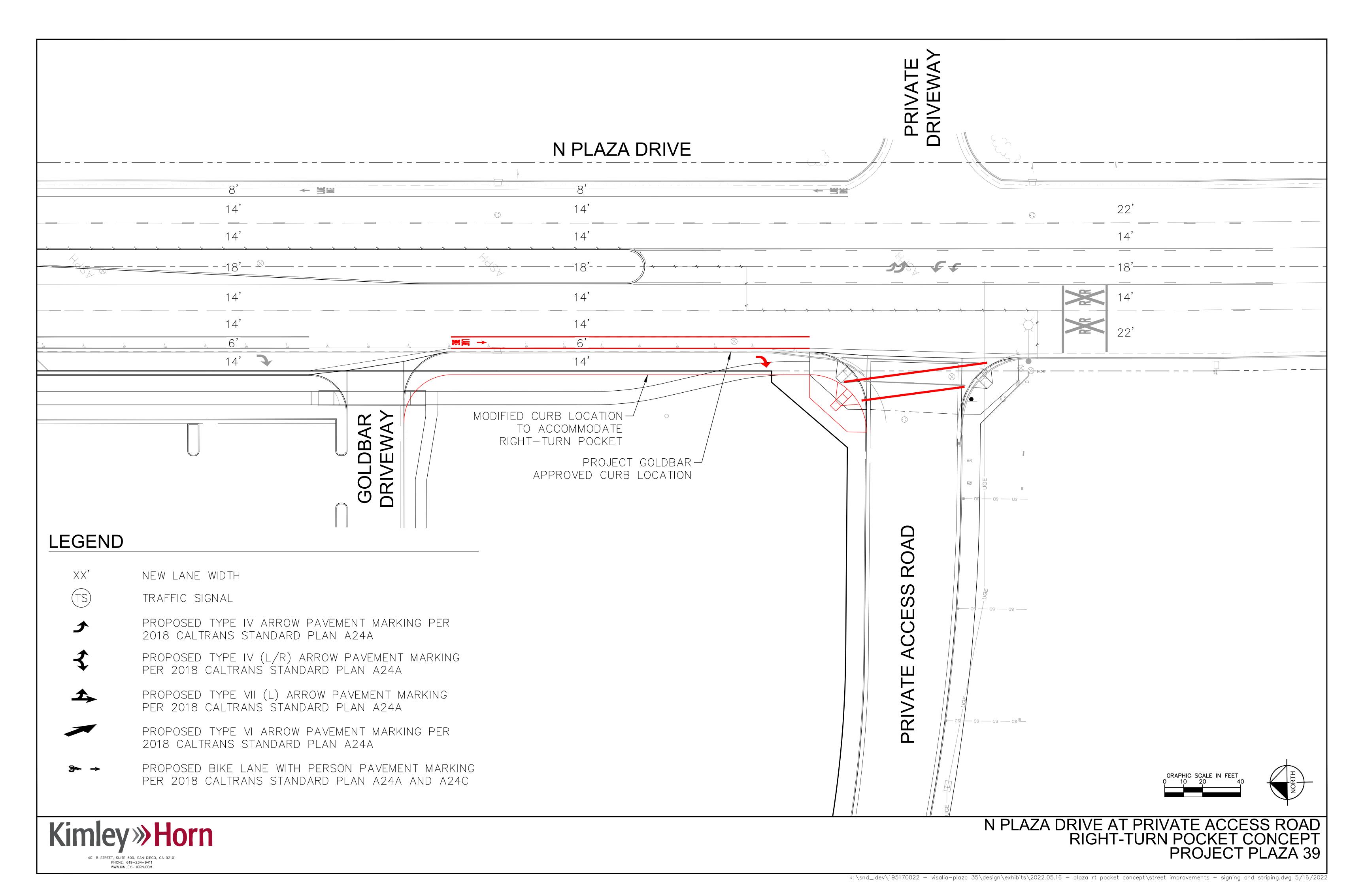
Project Distribution - 2042 BASE PM1VOL

| Roadway | Vol | % Distribution | % Adjusted |
|-------------------|------|----------------|------------|
| Ferguson | | | |
| West of Rd 76 | 159 | 5% | 5% |
| Road 76 | | | |
| North of Ferguson | 40 | 1% | 0% |
| South of Ave 304 | 112 | 4% | 5% |
| Ave 304 | | | |
| West of Rd 76 | 69 | 2% | 5% |
| Goshen Ave | | | |
| East of Plaza Rd | 224 | 7% | 10% |
| Plaza Rd | | | |
| South of Goshen | 1309 | 42% | 40% |
| North of Ferguson | 1179 | 38% | 35% |
| Total | 3092 | 100% | 100% |

C – Project Gold Bar Street Improvements and Modifications







D – Level of Service Calculation Sheets & Vehicle Queuing Calculation Sheets

| Intersection | | | | | | |
|------------------------|----------|-------|--------|----------|----------|-------|
| Int Delay, s/veh | 3 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| | | EDK | WDL | | | NDK |
| Lane Configurations | } | 440 | 40 | € | Y | 40 |
| Traffic Vol, veh/h | 26 | 148 | 10 | 12 | 66 | 10 |
| Future Vol, veh/h | 26 | 148 | 10 | 12 | 66 | 10 |
| Conflicting Peds, #/hr | _ 0 | 0 | _ 0 | _ 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storag | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 31 | 174 | 12 | 14 | 78 | 12 |
| | | | | | | |
| Majay/Misay | Maiaut | | Maia#0 | | Aire and | |
| Major/Minor | Major1 | | Major2 | | Minor1 | 440 |
| Conflicting Flow All | 0 | 0 | 205 | 0 | 156 | 118 |
| Stage 1 | - | - | - | - | 118 | - |
| Stage 2 | - | - | - | - | 38 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1366 | - | 835 | 934 |
| Stage 1 | - | - | - | - | 907 | - |
| Stage 2 | - | - | - | - | 984 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | _ | _ | 1366 | _ | 827 | 934 |
| Mov Cap-2 Maneuver | | _ | _ | _ | 827 | _ |
| Stage 1 | _ | - | _ | _ | 907 | _ |
| Stage 2 | _ | _ | _ | _ | 975 | _ |
| Olugo Z | | | | | 310 | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.5 | | 9.8 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| | | UDL 4 | EST | ED.5 | 14/5: | MACT |
| Minor Lane/Major Mvr | nt l | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 840 | - | | 1366 | - |
| HCM Lane V/C Ratio | | 0.106 | - | - | 0.009 | - |
| HCM Control Delay (s | | 9.8 | - | - | | 0 |
| HCM Lane LOS | | Α | - | - | Α | Α |
| HCM 95th %tile Q(veh | 1) | 0.4 | - | - | 0 | - |
| | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|---------|-------------|------|--------|-------------|----------|--------|------|-------|---------|------|------|
| Int Delay, s/veh | 6.7 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ች | † \$ | | | † \$ | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 1 | 116 | 14 | 37 | 158 | 91 | 8 | 6 | 19 | 193 | 19 | 0 |
| Future Vol, veh/h | 1 | 116 | 14 | 37 | 158 | 91 | 8 | 6 | 19 | 193 | 19 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 190 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, | # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 130 | 16 | 42 | 178 | 102 | 9 | 7 | 21 | 217 | 21 | 0 |
| | | | | | | | | | | | | |
| Major/Minor N | /lajor1 | | | Major2 | | <u> </u> | Minor1 | | N | /linor2 | | |
| Conflicting Flow All | 280 | 0 | 0 | 146 | 0 | 0 | 324 | 504 | 73 | 384 | 461 | 140 |
| Stage 1 | - | - | - | - | - | - | 140 | 140 | - | 313 | 313 | - |
| Stage 2 | - | - | - | - | - | - | 184 | 364 | - | 71 | 148 | - |
| Critical Hdwy | 4.14 | - | - | 4.14 | - | - | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Follow-up Hdwy | 2.22 | - | - | 2.22 | - | - | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap-1 Maneuver | 1280 | - | - | 1434 | - | - | 605 | 469 | 974 | 549 | 496 | 882 |
| Stage 1 | - | - | - | - | - | - | 849 | 780 | - | 672 | 656 | - |
| Stage 2 | - | - | - | - | - | - | 800 | 622 | - | 931 | 774 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1280 | - | - | 1434 | - | - | 571 | 455 | 974 | 519 | 481 | 882 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 571 | 455 | - | 519 | 481 | - |
| Stage 1 | - | - | - | - | - | - | 848 | 779 | - | 671 | 637 | - |
| Stage 2 | - | - | - | - | - | - | 751 | 604 | - | 902 | 773 | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.1 | | | 1 | | | 10.4 | | | 17.9 | | |
| HCM LOS | | | | | | | В | | | С | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR | SBLn1 | | | |
| Capacity (veh/h) | | | 1280 | | | 1434 | - | - | | | | |
| HCM Lane V/C Ratio | | 0.052 | | - | | 0.029 | _ | | 0.463 | | | |
| HCM Control Delay (s) | | 10.4 | 7.8 | - | _ | 7.6 | _ | - | 17.9 | | | |
| HCM Lane LOS | | В | A | - | - | A | - | _ | C | | | |
| HCM 95th %tile Q(veh) | | 0.2 | 0 | - | - | 0.1 | - | - | 2.4 | | | |
| | | | | | | | | | | | | |

| | ۶ | \rightarrow | • | 4 | † | ~ | > | ļ | 4 |
|-------------------------|------|---------------|------|------|----------|------|-------------|------|------|
| Lane Group | EBL | EBR | WBL | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 16 | 57 | 8 | 94 | 549 | 8 | 7 | 649 | 30 |
| v/c Ratio | 0.09 | 0.14 | 0.06 | 0.68 | 0.19 | 0.01 | 0.05 | 0.28 | 0.03 |
| Control Delay | 25.1 | 0.7 | 29.6 | 56.8 | 3.9 | 0.0 | 29.3 | 6.3 | 0.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 25.1 | 0.7 | 29.6 | 56.8 | 3.9 | 0.0 | 29.3 | 6.3 | 0.0 |
| Queue Length 50th (ft) | 6 | 0 | 3 | 35 | 20 | 0 | 2 | 52 | 0 |
| Queue Length 95th (ft) | 20 | 0 | 15 | #113 | 93 | 0 | 14 | 111 | 0 |
| Internal Link Dist (ft) | | | | | 1413 | | | 2950 | |
| Turn Bay Length (ft) | 200 | 110 | 120 | 250 | | 275 | 305 | | 110 |
| Base Capacity (vph) | 188 | 942 | 138 | 138 | 2866 | 1304 | 138 | 2336 | 1085 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.06 | 0.06 | 0.68 | 0.19 | 0.01 | 0.05 | 0.28 | 0.03 |
| | | | | | | | | | |

Intersection Summary

Synchro 11 Report Kimley-Horn Page 3 Queues

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

| | ۶ | → | • | • | ← | 4 | 1 | † | ~ | / | | ✓ |
|------------------------------|------|----------|------|------|----------|------|-------------|----------|------|----------|--------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 | 7 | ^↑ | 7 |
| Traffic Volume (veh/h) | 14 | 0 | 51 | 7 | 0 | 0 | 84 | 489 | 7 | 6 | 578 | 27 |
| Future Volume (veh/h) | 14 | 0 | 51 | 7 | 0 | 0 | 84 | 489 | 7 | 6 | 578 | 27 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 16 | 0 | 57 | 8 | 0 | 0 | 94 | 549 | 8 | 7 | 649 | 30 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 34 | 202 | 90 | 18 | 171 | 76 | 120 | 2276 | 1015 | 16 | 2068 | 922 |
| Arrive On Green | 0.02 | 0.00 | 0.06 | 0.01 | 0.00 | 0.00 | 0.07 | 0.64 | 0.64 | 0.01 | 0.58 | 0.58 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 16 | 0 | 57 | 8 | 0 | 0 | 94 | 549 | 8 | 7 | 649 | 30 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 0.6 | 0.0 | 2.2 | 0.3 | 0.0 | 0.0 | 3.3 | 4.2 | 0.1 | 0.2 | 5.9 | 0.5 |
| Cycle Q Clear(g_c), s | 0.6 | 0.0 | 2.2 | 0.3 | 0.0 | 0.0 | 3.3 | 4.2 | 0.1 | 0.2 | 5.9 | 0.5 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 34 | 202 | 90 | 18 | 171 | 76 | 120 | 2276 | 1015 | 16 | 2068 | 922 |
| V/C Ratio(X) | 0.46 | 0.00 | 0.63 | 0.43 | 0.00 | 0.00 | 0.78 | 0.24 | 0.01 | 0.43 | 0.31 | 0.03 |
| Avail Cap(c_a), veh/h | 140 | 1750 | 780 | 140 | 1789 | 798 | 140 | 2276 | 1015 | 140 | 2068 | 922 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 30.8 | 0.0 | 29.3 | 31.3 | 0.0 | 0.0 | 29.2 | 4.9 | 4.1 | 31.3 | 6.8 | 5.7 |
| Incr Delay (d2), s/veh | 9.4 | 0.0 | 7.1 | 15.2 | 0.0 | 0.0 | 21.3 | 0.3 | 0.0 | 16.9 | 0.4 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.3 | 0.0 | 1.0 | 0.2 | 0.0 | 0.0 | 1.9 | 0.8 | 0.0 | 0.2 | 1.4 | 0.2 |
| Unsig. Movement Delay, s/veh | | 0.0 | 00.4 | 40.5 | 0.0 | 0.0 | 50.4 | - 4 | | 40.0 | | |
| LnGrp Delay(d),s/veh | 40.2 | 0.0 | 36.4 | 46.5 | 0.0 | 0.0 | 50.4 | 5.1 | 4.1 | 48.2 | 7.2 | 5.7 |
| LnGrp LOS | D | A | D | D | A | A | D | Α | Α | D | A | A |
| Approach Vol, veh/h | | 73 | | | 8 | | | 651 | | | 686 | |
| Approach Delay, s/veh | | 37.2 | | | 46.5 | | | 11.6 | | | 7.5 | |
| Approach LOS | | D | | | D | | | В | | | Α | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 5.1 | 45.2 | 5.2 | 8.1 | 8.8 | 41.5 | 5.7 | 7.6 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 37.0 | 5.0 | 31.3 | 5.0 | 37.0 | 5.0 | 32.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.2 | 6.2 | 2.3 | 4.2 | 5.3 | 7.9 | 2.6 | 0.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.3 | 0.0 | 0.1 | 0.0 | 4.1 | 0.0 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 11.2 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|----------|------|--------|---------|----------|--------|----------|------|----------|----------|------|
| Int Delay, s/veh | 0.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | 1 | | | 4 | | ሻ | † | | <u> </u> | † | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 594 | 19 | 5 | 638 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 594 | 19 | 5 | 638 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | 150 | - | - | 150 | - | - |
| Veh in Median Storage | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 691 | 22 | 6 | 742 | 0 |
| | | | | | | | | | | | | |
| Major/Minor N | Minor2 | | | Minor1 | | <u> </u> | Major1 | | N | Major2 | | |
| Conflicting Flow All | 1100 | 1467 | 371 | 1085 | 1456 | 357 | 742 | 0 | 0 | 713 | 0 | 0 |
| Stage 1 | 754 | 754 | - | 702 | 702 | - | - | - | - | - | - | - |
| Stage 2 | 346 | 713 | - | 383 | 754 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 | 4.14 | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 | 2.22 | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | 167 | 127 | 626 | 171 | 129 | 639 | 861 | - | - | 883 | - | - |
| Stage 1 | 367 | 415 | - | 395 | 439 | - | - | - | - | - | - | - |
| Stage 2 | 643 | 434 | - | 611 | 415 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 166 | 126 | 626 | 170 | 128 | 639 | 861 | - | - | 883 | - | - |
| Mov Cap-2 Maneuver | 166 | 126 | - | 170 | 128 | - | - | - | - | - | - | - |
| Stage 1 | 367 | 412 | - | 395 | 439 | - | - | - | - | - | - | - |
| Stage 2 | 642 | 434 | - | 607 | 412 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0 | | | 18.5 | | | 0 | | | 0.1 | | |
| HCM LOS | Α | | | С | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBL | NBT | NBR I | EBLn1 I | EBLn2V | VBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 861 | - | - | - | - | 269 | 883 | - | - | | |
| HCM Lane V/C Ratio | | - | - | - | - | - | 0.009 | | - | - | | |
| HCM Control Delay (s) | | 0 | - | - | 0 | 0 | 18.5 | 9.1 | - | - | | |
| HCM Lane LOS | | Α | - | - | Α | Α | С | Α | - | - | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | - | - | 0 | 0 | - | - | | |
| | | | | | | | | | | | | |

| | ၨ | - | • | • | • | • | • | † | ~ | - | ļ | 4 |
|-------------------------|------|------|------|------|------|------|-------|----------|------|------|------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 29 | 168 | 202 | 86 | 134 | 96 | 199 | 548 | 71 | 123 | 496 | 45 |
| v/c Ratio | 0.27 | 0.42 | 0.56 | 0.80 | 0.21 | 0.26 | 1.09 | 0.31 | 0.08 | 0.67 | 0.28 | 0.05 |
| Control Delay | 44.5 | 37.1 | 11.9 | 88.1 | 31.0 | 8.4 | 131.5 | 12.9 | 1.4 | 55.4 | 12.6 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 44.5 | 37.1 | 11.9 | 88.1 | 31.0 | 8.4 | 131.5 | 12.9 | 1.4 | 55.4 | 12.6 | 0.1 |
| Queue Length 50th (ft) | 15 | 43 | 0 | 45 | 29 | 0 | ~117 | 82 | 0 | 62 | 73 | 0 |
| Queue Length 95th (ft) | 42 | 73 | 59 | #131 | 60 | 38 | #256 | 125 | 11 | #145 | 113 | 0 |
| Internal Link Dist (ft) | | 2572 | | | 1230 | | | 2364 | | | 1021 | |
| Turn Bay Length (ft) | 250 | | 110 | 250 | | 90 | 330 | | 105 | 170 | | 140 |
| Base Capacity (vph) | 107 | 1588 | 821 | 107 | 1588 | 768 | 182 | 1778 | 847 | 184 | 1782 | 848 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.27 | 0.11 | 0.25 | 0.80 | 0.08 | 0.13 | 1.09 | 0.31 | 0.08 | 0.67 | 0.28 | 0.05 |

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

| | ۶ | → | • | • | — | • | 1 | † | ~ | / | + | ✓ |
|------------------------------|------|----------|------|------|----------|------|-------|----------|------|--------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 | 7 | ^↑ | 7 |
| Traffic Volume (veh/h) | 27 | 156 | 188 | 80 | 125 | 89 | 185 | 510 | 66 | 114 | 461 | 42 |
| Future Volume (veh/h) | 27 | 156 | 188 | 80 | 125 | 89 | 185 | 510 | 66 | 114 | 461 | 42 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 29 | 168 | 202 | 86 | 134 | 96 | 199 | 548 | 71 | 123 | 496 | 45 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 52 | 578 | 258 | 102 | 679 | 303 | 174 | 1731 | 772 | 154 | 1691 | 754 |
| Arrive On Green | 0.03 | 0.16 | 0.16 | 0.06 | 0.19 | 0.19 | 0.10 | 0.49 | 0.49 | 0.09 | 0.48 | 0.48 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 29 | 168 | 202 | 86 | 134 | 96 | 199 | 548 | 71 | 123 | 496 | 45 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 1.4 | 3.6 | 10.7 | 4.2 | 2.8 | 4.5 | 8.5 | 8.2 | 2.1 | 5.9 | 7.4 | 1.3 |
| Cycle Q Clear(g_c), s | 1.4 | 3.6 | 10.7 | 4.2 | 2.8 | 4.5 | 8.5 | 8.2 | 2.1 | 5.9 | 7.4 | 1.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 52 | 578 | 258 | 102 | 679 | 303 | 174 | 1731 | 772 | 154 | 1691 | 754 |
| V/C Ratio(X) | 0.56 | 0.29 | 0.78 | 0.84 | 0.20 | 0.32 | 1.15 | 0.32 | 0.09 | 0.80 | 0.29 | 0.06 |
| Avail Cap(c_a), veh/h | 102 | 1508 | 673 | 102 | 1508 | 673 | 174 | 1731 | 772 | 176 | 1691 | 754 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.8 | 32.1 | 35.0 | 40.7 | 29.6 | 30.4 | 39.3 | 13.6 | 12.0 | 39.1 | 13.9 | 12.3 |
| Incr Delay (d2), s/veh | 9.3 | 0.3 | 5.2 | 43.7 | 0.1 | 0.6 | 113.0 | 0.5 | 0.2 | 20.3 | 0.4 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.7 | 1.5 | 4.2 | 3.0 | 1.1 | 1.7 | 8.9 | 2.8 | 0.7 | 3.3 | 2.6 | 0.4 |
| Unsig. Movement Delay, s/veh | | 00.4 | 40.0 | 04.4 | 00.0 | 04.0 | 450.0 | 440 | 40.0 | 50. 4 | 44.4 | 40.5 |
| LnGrp Delay(d),s/veh | 51.1 | 32.4 | 40.2 | 84.4 | 29.8 | 31.0 | 152.3 | 14.0 | 12.2 | 59.4 | 14.4 | 12.5 |
| LnGrp LOS | D | C | D | F | C | С | F | В | В | <u>E</u> | В | В |
| Approach Vol, veh/h | | 399 | | | 316 | | | 818 | | | 664 | |
| Approach Delay, s/veh | | 37.7 | | | 45.0 | | | 47.5 | | | 22.6 | |
| Approach LOS | | D | | | D | | | D | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.0 | 47.0 | 9.5 | 18.7 | 13.0 | 46.0 | 7.0 | 21.2 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 8.6 | 41.4 | 5.0 | 37.0 | 8.5 | 41.5 | 5.0 | 37.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.9 | 10.2 | 6.2 | 12.7 | 10.5 | 9.4 | 3.4 | 6.5 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.5 | 0.0 | 1.5 | 0.0 | 3.1 | 0.0 | 1.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 37.8 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|--------|-------|--------|------|--------|-------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ₽ | | | स | ¥,F | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storag | e,# 0 | - | - | 0 | 0 | - |
| Grade, % | 0 | - | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |
| WWW.CT IOW | • | Ū | | | J | J |
| | | | | - | | |
| Major/Minor | Major1 | | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 2 | 1 |
| Stage 1 | - | - | - | - | 1 | - |
| Stage 2 | - | - | - | - | 1 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1622 | - | 1021 | 1084 |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 1022 | _ |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1622 | - | 1021 | 1084 |
| Mov Cap-2 Maneuver | | - | - | - | 1021 | - |
| Stage 1 | _ | _ | _ | _ | 1022 | _ |
| Stage 2 | _ | _ | _ | _ | 4000 | _ |
| otago 2 | | | | | 1022 | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvr | nt I | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 1622 | - |
| HCM Lane V/C Ratio | | - | _ | _ | 1022 | - |
| HCM Control Delay (s |) | 0 | | _ | 0 | - |
| HCM Lane LOS | 7 | A | _ | _ | A | _ |
| HCM 95th %tile Q(ver | n) | - | | _ | 0 | - |
| HOW JOHN JULIE Q(VEI | '/ | | | | U | |

| Intersection | | | | | | |
|------------------------|-----------|-------|--------|------|---------|-------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 1→ | LDIX | VVDL | 4 | NDL NDL | TIDIN |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | |
| Sign Control | Free - | Free | Free | Free | Stop | Stop |
| RT Channelized | | None | - | | - | None |
| Storage Length | - # 0 | - | - | - | 0 | - |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | |
| Major/Minor N | /lajor1 | N | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 2 | 1 |
| Stage 1 | - | - | - | - | 1 | - |
| Stage 2 | _ | _ | _ | _ | 1 | _ |
| Critical Hdwy | _ | _ | 4.12 | _ | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | <u>-</u> | _ | 7.12 | _ | 5.42 | 0.22 |
| Critical Hdwy Stg 2 | _ | | _ | | 5.42 | _ |
| Follow-up Hdwy | | _ | 2.218 | - | 3.518 | |
| Pot Cap-1 Maneuver | - | - | 1622 | _ | 1021 | 1084 |
| • | - | - | 1022 | - | 1021 | 1004 |
| Stage 1 | - | - | - | _ | | - |
| Stage 2 | - | - | - | - | 1022 | - |
| Platoon blocked, % | - | - | 4000 | - | 1001 | 4004 |
| Mov Cap-1 Maneuver | - | - | 1622 | - | 1021 | 1084 |
| Mov Cap-2 Maneuver | - | - | - | - | 1021 | - |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 1022 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | U | | U | | A | |
| TIOWI LOS | | | | | A | |
| | | | | | | |
| Minor Lane/Major Mvmt | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 1622 | - |
| HCM Lane V/C Ratio | | - | - | - | - | - |
| HCM Control Delay (s) | | 0 | - | - | 0 | - |
| HCM Lane LOS | | Α | - | - | Α | - |
| HCM 95th %tile Q(veh) | | - | - | - | 0 | - |
| | | | | | | |

| Intersection | | | | | | |
|-----------------------------|----------|-------|--------|------------|----------|--------------|
| Int Delay, s/veh | 5.3 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | \$ | LDIX | VVDL | ₩ <u>₩</u> | NDL W | TIDIX |
| Traffic Vol, veh/h | 15 | 86 | 10 | 23 | 130 | 10 |
| Future Vol, veh/h | 15 | 86 | 10 | 23 | 130 | 10 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | | |
| Sign Control RT Channelized | -ree | None | | | Stop | Stop None |
| | | | - | | - | None - |
| Storage Length | - # 0 | - | - | - | 0 | |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 16 | 93 | 11 | 25 | 141 | 11 |
| | | | | | | |
| Major/Minor N | Major1 | ı | Major2 | ı | Minor1 | |
| Conflicting Flow All | 0 | 0 | 109 | 0 | 110 | 63 |
| Stage 1 | - | | 100 | - | 63 | - |
| Stage 2 | <u>-</u> | _ | _ | _ | 47 | <u>-</u> |
| Critical Hdwy | _ | | 4.12 | _ | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | <u> </u> | _ | 4.12 | _ | 5.42 | 0.22 |
| | | - | _ | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | 2.218 | - | 3.518 | 2 210 |
| Follow-up Hdwy | - | - | | - | | |
| Pot Cap-1 Maneuver | - | - | 1481 | - | 887 | 1002 |
| Stage 1 | - | - | - | - | 960 | - |
| Stage 2 | - | - | - | - | 975 | - |
| Platoon blocked, % | - | - | 1101 | - | 000 | 4000 |
| Mov Cap-1 Maneuver | - | - | 1481 | - | 880 | 1002 |
| Mov Cap-2 Maneuver | - | - | - | - | 880 | - |
| Stage 1 | - | - | - | - | 960 | - |
| Stage 2 | - | - | - | - | 967 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| | 0 | | 2.3 | | 9.9 | |
| HCM Control Delay, s | U | | 2.3 | | | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvm | t 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 888 | - | | 1481 | - |
| HCM Lane V/C Ratio | | 0.171 | _ | | 0.007 | _ |
| HCM Control Delay (s) | | 9.9 | _ | _ | | 0 |
| HCM Lane LOS | | Α | _ | _ | Α | A |
| HCM 95th %tile Q(veh) | | 0.6 | _ | _ | 0 | - |
| 70.1170.110 3(1011) | | 0.0 | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------|------|--------|------------|------|--------|-------|-------|---------|------|------|
| Int Delay, s/veh | 5.7 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ħβ | | ř | ↑ ↑ | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 7 | 221 | 15 | 23 | 126 | 140 | 15 | 19 | 74 | 131 | 28 | 7 |
| Future Vol, veh/h | 7 | 221 | 15 | 23 | 126 | 140 | 15 | 19 | 74 | 131 | 28 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | _ | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 190 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | ,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 | 91 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 248 | 17 | 26 | 142 | 157 | 16 | 21 | 83 | 147 | 31 | 8 |
| | | | | | | | | | | | | |
| Major/Minor N | Major1 | | | Major2 | | | Minor1 | | N | /linor2 | | |
| Conflicting Flow All | 299 | 0 | 0 | 265 | 0 | 0 | 412 | 624 | 133 | 424 | 554 | 150 |
| Stage 1 | - | - | - | - | _ | _ | 273 | 273 | - | 273 | 273 | - |
| Stage 2 | _ | - | _ | _ | _ | _ | 139 | 351 | - | 151 | 281 | _ |
| Critical Hdwy | 4.14 | - | _ | 4.14 | _ | - | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 | | - | _ | | _ | _ | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Critical Hdwy Stg 2 | - | - | _ | _ | _ | _ | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Follow-up Hdwy | 2.22 | - | _ | 2.22 | _ | _ | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap-1 Maneuver | 1259 | - | - | 1296 | _ | _ | 524 | 400 | 892 | 514 | 439 | 870 |
| Stage 1 | - | - | - | - | - | - | 710 | 683 | - | 710 | 683 | - |
| Stage 2 | _ | _ | _ | - | - | _ | 850 | 631 | - | 836 | 677 | _ |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1259 | - | - | 1296 | - | - | 481 | 390 | 892 | 438 | 428 | 870 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 481 | 390 | - | 438 | 428 | - |
| Stage 1 | - | _ | - | - | - | - | 706 | 679 | - | 706 | 669 | - |
| Stage 2 | - | - | - | - | _ | - | 787 | 618 | - | 730 | 673 | - |
| 3 · | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.2 | | | 0.6 | | | 11.6 | | | 18.8 | | |
| HCM LOS | | | | | | | В | | | С | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR : | SBLn1 | | | |
| Capacity (veh/h) | | 664 | 1259 | - | - | 1296 | - | - | 446 | | | |
| HCM Lane V/C Ratio | | 0.182 | | _ | _ | 0.02 | _ | _ | 0.418 | | | |
| HCM Control Delay (s) | | 11.6 | 7.9 | _ | _ | 7.8 | _ | _ | 18.8 | | | |
| HCM Lane LOS | | В | A | _ | _ | A | - | - | С | | | |
| HCM 95th %tile Q(veh) | | 0.7 | 0 | - | _ | 0.1 | - | - | 2 | | | |
| 2000 2000 | | • • • | | | | | | | | | | |

| | • | - | \rightarrow | • | • | 4 | † | / | > | ļ | 4 | |
|-------------------------|------|------|---------------|------|------|------|----------|------|-------------|------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Group Flow (vph) | 29 | 1 | 65 | 30 | 9 | 48 | 624 | 18 | 4 | 524 | 11 | |
| v/c Ratio | 0.16 | 0.00 | 0.27 | 0.22 | 0.02 | 0.35 | 0.24 | 0.01 | 0.03 | 0.22 | 0.01 | |
| Control Delay | 29.7 | 30.0 | 4.6 | 34.3 | 0.1 | 37.9 | 5.1 | 0.0 | 30.8 | 6.8 | 0.0 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 29.7 | 30.0 | 4.6 | 34.3 | 0.1 | 37.9 | 5.1 | 0.0 | 30.8 | 6.8 | 0.0 | |
| Queue Length 50th (ft) | 10 | 0 | 0 | 11 | 0 | 17 | 23 | 0 | 1 | 40 | 0 | |
| Queue Length 95th (ft) | 36 | 2 | 11 | 37 | 0 | 52 | 110 | 0 | 10 | 91 | 0 | |
| Internal Link Dist (ft) | | 223 | | | | | 1413 | | | 2950 | | |
| Turn Bay Length (ft) | 200 | | 110 | 120 | 105 | 250 | | 275 | 305 | | 110 | |
| Base Capacity (vph) | 187 | 1753 | 843 | 137 | 921 | 137 | 2637 | 1209 | 137 | 2431 | 1124 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.16 | 0.00 | 0.08 | 0.22 | 0.01 | 0.35 | 0.24 | 0.01 | 0.03 | 0.22 | 0.01 | |
| Intersection Summary | | | | | | | | | | | | |

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|------------------------------|------|----------|------|------|----------|------|------|----------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 28 | 1 | 64 | 29 | 0 | 9 | 47 | 612 | 18 | 4 | 514 | 11 |
| Future Volume (veh/h) | 28 | 1 | 64 | 29 | 0 | 9 | 47 | 612 | 18 | 4 | 514 | 11 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 29 | 1 | 65 | 30 | 0 | 9 | 48 | 624 | 18 | 4 | 524 | 11 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 56 | 234 | 104 | 57 | 236 | 105 | 80 | 2189 | 977 | 10 | 2049 | 914 |
| Arrive On Green | 0.03 | 0.07 | 0.07 | 0.03 | 0.00 | 0.07 | 0.04 | 0.62 | 0.62 | 0.01 | 0.58 | 0.58 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 29 | 1 | 65 | 30 | 0 | 9 | 48 | 624 | 18 | 4 | 524 | 11 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 1.0 | 0.0 | 2.6 | 1.1 | 0.0 | 0.3 | 1.7 | 5.2 | 0.3 | 0.1 | 4.7 | 0.2 |
| Cycle Q Clear(g_c), s | 1.0 | 0.0 | 2.6 | 1.1 | 0.0 | 0.3 | 1.7 | 5.2 | 0.3 | 0.1 | 4.7 | 0.2 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 56 | 234 | 104 | 57 | 236 | 105 | 80 | 2189 | 977 | 10 | 2049 | 914 |
| V/C Ratio(X) | 0.52 | 0.00 | 0.62 | 0.52 | 0.00 | 0.09 | 0.60 | 0.29 | 0.02 | 0.42 | 0.26 | 0.01 |
| Avail Cap(c_a), veh/h | 139 | 1734 | 773 | 139 | 1772 | 791 | 139 | 2189 | 977 | 139 | 2049 | 914 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 30.6 | 28.0 | 29.2 | 30.6 | 0.0 | 28.1 | 30.1 | 5.7 | 4.8 | 31.8 | 6.7 | 5.8 |
| Incr Delay (d2), s/veh | 7.2 | 0.0 | 6.0 | 7.1 | 0.0 | 0.3 | 7.1 | 0.3 | 0.0 | 26.6 | 0.3 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.5 | 0.0 | 1.1 | 0.6 | 0.0 | 0.1 | 0.8 | 1.2 | 0.1 | 0.1 | 1.2 | 0.1 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 37.8 | 28.0 | 35.2 | 37.7 | 0.0 | 28.5 | 37.2 | 6.1 | 4.8 | 58.4 | 7.0 | 5.8 |
| LnGrp LOS | D | С | D | D | A | С | D | Α | A | E | A | A |
| Approach Vol, veh/h | | 95 | | | 39 | | | 690 | | | 539 | |
| Approach Delay, s/veh | | 35.9 | | | 35.6 | | | 8.2 | | | 7.4 | |
| Approach LOS | | D | | | D | | | Α | | | Α | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 4.8 | 44.0 | 6.6 | 8.7 | 7.4 | 41.5 | 6.5 | 8.8 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 37.0 | 5.0 | 31.3 | 5.0 | 37.0 | 5.0 | 32.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.1 | 7.2 | 3.1 | 4.6 | 3.7 | 6.7 | 3.0 | 2.3 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.9 | 0.0 | 0.2 | 0.0 | 3.2 | 0.0 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 10.6 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|----------|----------|------|--------|---------|----------|--------|----------|------|---------|----------|------|
| Int Delay, s/veh | 0.1 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | <u> </u> | 1 | | | 4 | | ሻ | † | | ሻ | † | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 6 | 0 | 3 | 0 | 651 | 3 | 1 | 683 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 6 | 0 | 3 | 0 | 651 | 3 | 1 | 683 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | 150 | - | - | 150 | - | - |
| Veh in Median Storage | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 6 | 0 | 3 | 0 | 671 | 3 | 1 | 704 | 0 |
| | | | | | | | | | | | | |
| Major/Minor N | /linor2 | | | Minor1 | | <u> </u> | Major1 | | N | //ajor2 | | |
| Conflicting Flow All | 1042 | 1380 | 352 | 1027 | 1379 | 337 | 704 | 0 | 0 | 674 | 0 | 0 |
| Stage 1 | 706 | 706 | - | 673 | 673 | - | - | - | - | - | - | - |
| Stage 2 | 336 | 674 | - | 354 | 706 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 | 4.14 | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 | 2.22 | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | 184 | 143 | 644 | 189 | 143 | 659 | 890 | - | - | 913 | - | - |
| Stage 1 | 393 | 437 | - | 411 | 452 | - | - | - | - | - | - | - |
| Stage 2 | 652 | 452 | - | 636 | 437 | - | - | - | - | - | - | - |
| Platoon blocked, % | | | | | | | | - | - | | - | - |
| Mov Cap-1 Maneuver | 183 | 143 | 644 | 189 | 143 | 659 | 890 | - | - | 913 | - | - |
| Mov Cap-2 Maneuver | 183 | 143 | - | 189 | 143 | - | - | - | - | - | - | - |
| Stage 1 | 393 | 437 | - | 411 | 452 | - | - | - | - | - | - | - |
| Stage 2 | 649 | 452 | - | 635 | 437 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0 | | | 20.1 | | | 0 | | | 0 | | |
| HCM LOS | Α | | | С | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBL | NBT | NBR I | EBLn1 l | EBLn2V | VBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 890 | - | - | - | - | 248 | 913 | - | - | | |
| HCM Lane V/C Ratio | | - | - | - | - | - | 0.037 | | - | - | | |
| HCM Control Delay (s) | | 0 | - | - | 0 | 0 | 20.1 | 8.9 | - | - | | |
| HCM Lane LOS | | Α | - | - | Α | Α | С | Α | - | - | | |
| HCM 95th %tile Q(veh) | | 0 | - | - | - | - | 0.1 | 0 | - | - | | |
| | | | | | | | | | | | | |

| | • | → | • | • | • | • | 4 | † | ~ | \ | ļ | 1 |
|-------------------------|------|----------|------|------|------|------|-------|----------|------|----------|------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 77 | 231 | 231 | 94 | 150 | 109 | 176 | 541 | 63 | 121 | 518 | 33 |
| v/c Ratio | 0.66 | 0.50 | 0.57 | 0.81 | 0.33 | 0.36 | 1.11 | 0.31 | 0.08 | 0.68 | 0.29 | 0.04 |
| Control Delay | 67.8 | 37.8 | 10.8 | 87.0 | 34.9 | 10.6 | 145.4 | 13.9 | 1.1 | 57.5 | 13.1 | 0.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 67.8 | 37.8 | 10.8 | 87.0 | 34.9 | 10.6 | 145.4 | 13.9 | 1.1 | 57.5 | 13.1 | 0.1 |
| Queue Length 50th (ft) | 40 | 60 | 0 | 50 | 38 | 0 | ~107 | 85 | 0 | 63 | 79 | 0 |
| Queue Length 95th (ft) | #113 | 95 | 61 | #140 | 66 | 43 | #242 | 131 | 8 | #147 | 122 | 0 |
| Internal Link Dist (ft) | | 2572 | | | 1230 | | | 2364 | | | 1021 | |
| Turn Bay Length (ft) | 250 | | 110 | 250 | | 90 | 330 | | 105 | 170 | | 140 |
| Base Capacity (vph) | 116 | 1560 | 827 | 116 | 1560 | 759 | 158 | 1729 | 826 | 179 | 1771 | 844 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.66 | 0.15 | 0.28 | 0.81 | 0.10 | 0.14 | 1.11 | 0.31 | 0.08 | 0.68 | 0.29 | 0.04 |

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

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|------------------------------|------|----------|------|------|----------|------|-------|----------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 | 7 | ^↑ | 7 |
| Traffic Volume (veh/h) | 72 | 217 | 217 | 88 | 141 | 102 | 165 | 509 | 59 | 114 | 487 | 31 |
| Future Volume (veh/h) | 72 | 217 | 217 | 88 | 141 | 102 | 165 | 509 | 59 | 114 | 487 | 31 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 77 | 231 | 231 | 94 | 150 | 109 | 176 | 541 | 63 | 121 | 518 | 33 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 99 | 653 | 291 | 110 | 674 | 301 | 149 | 1666 | 743 | 151 | 1669 | 744 |
| Arrive On Green | 0.06 | 0.18 | 0.18 | 0.06 | 0.19 | 0.19 | 0.08 | 0.47 | 0.47 | 0.08 | 0.47 | 0.47 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 77 | 231 | 231 | 94 | 150 | 109 | 176 | 541 | 63 | 121 | 518 | 33 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 3.8 | 5.1 | 12.5 | 4.7 | 3.2 | 5.4 | 7.5 | 8.5 | 2.0 | 6.0 | 8.1 | 1.0 |
| Cycle Q Clear(g_c), s | 3.8 | 5.1 | 12.5 | 4.7 | 3.2 | 5.4 | 7.5 | 8.5 | 2.0 | 6.0 | 8.1 | 1.0 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 99 | 653 | 291 | 110 | 674 | 301 | 149 | 1666 | 743 | 151 | 1669 | 744 |
| V/C Ratio(X) | 0.78 | 0.35 | 0.79 | 0.86 | 0.22 | 0.36 | 1.18 | 0.32 | 0.08 | 0.80 | 0.31 | 0.04 |
| Avail Cap(c_a), veh/h | 110 | 1470 | 656 | 110 | 1470 | 656 | 149 | 1666 | 743 | 169 | 1669 | 744 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.7 | 31.9 | 34.9 | 41.6 | 30.6 | 31.5 | 41.0 | 14.9 | 13.1 | 40.2 | 14.7 | 12.8 |
| Incr Delay (d2), s/veh | 27.1 | 0.3 | 4.9 | 45.2 | 0.2 | 0.7 | 129.5 | 0.5 | 0.2 | 21.4 | 0.5 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.3 | 2.1 | 4.9 | 3.3 | 1.3 | 2.0 | 8.4 | 3.1 | 0.7 | 3.3 | 2.9 | 0.3 |
| Unsig. Movement Delay, s/veh | | 00.0 | 00.7 | 00.0 | 00.0 | 00.0 | 470 5 | 45.4 | 40.4 | 04.0 | 45.0 | 40.0 |
| LnGrp Delay(d),s/veh | 68.8 | 32.2 | 39.7 | 86.8 | 30.8 | 32.3 | 170.5 | 15.4 | 13.4 | 61.6 | 15.2 | 13.0 |
| LnGrp LOS | E | C | D | F | C | С | F | В | В | E | В | B |
| Approach Vol, veh/h | | 539 | | | 353 | | | 780 | | | 672 | |
| Approach Delay, s/veh | | 40.7 | | | 46.2 | | | 50.2 | | | 23.4 | |
| Approach LOS | | D | | | D | | | D | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.1 | 46.4 | 10.0 | 20.9 | 12.0 | 46.5 | 9.5 | 21.5 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 8.5 | 41.0 | 5.5 | 37.0 | 7.5 | 42.0 | 5.5 | 37.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 8.0 | 10.5 | 6.7 | 14.5 | 9.5 | 10.1 | 5.8 | 7.4 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.4 | 0.0 | 2.0 | 0.0 | 3.2 | 0.0 | 1.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 39.7 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|----------|--------|------|--------|-------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | <u>₽</u> | | | 4 | ¥ | |
| Traffic Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | _ | - | _ | - | 0 | - |
| Veh in Median Storage | # 0 | _ | _ | 0 | 0 | _ |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |
| MINITIL FIOW | U | U | U | U | U | U |
| | | | | | | |
| Major/Minor N | /lajor1 | | Major2 | ا | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 2 | 1 |
| Stage 1 | - | - | - | - | 1 | - |
| Stage 2 | - | - | - | - | 1 | - |
| Critical Hdwy | _ | _ | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | _ | _ | - | _ | 5.42 | _ |
| Critical Hdwy Stg 2 | _ | _ | _ | _ | 5.42 | _ |
| Follow-up Hdwy | _ | _ | 2.218 | _ | 3.518 | 3 318 |
| Pot Cap-1 Maneuver | _ | _ | 1622 | _ | 1021 | 1084 |
| Stage 1 | _ | _ | - | _ | 1022 | - |
| Stage 2 | _ | _ | _ | _ | 1022 | _ |
| Platoon blocked, % | <u>-</u> | <u>-</u> | | _ | 1022 | |
| Mov Cap-1 Maneuver | | _ | 1622 | _ | 1021 | 1084 |
| Mov Cap-1 Maneuver | _ | _ | 1022 | _ | 1021 | 1004 |
| | | - | | | 1021 | |
| Stage 1 | - | - | - | - | | |
| Stage 2 | - | - | - | - | 1022 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | | | | | A | |
| | | | | | ,\ | |
| | | | | | | |
| Minor Lane/Major Mvm | t I | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | - | - | - | 1622 | - |
| HCM Lane V/C Ratio | | - | - | - | - | - |
| HCM Control Delay (s) | | 0 | - | - | 0 | - |
| HCM Lane LOS | | Α | - | - | Α | - |
| HCM 95th %tile Q(veh) | | - | - | - | 0 | - |
| , | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|--------------|-----------|-------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | | LDK | VVDL | | INDL W | INDIX |
| Traffic Vol, veh/h | ₽ | 0 | ٥ | વ | | ٥ |
| | 0 | | 0 | 0 | 0 | 0 |
| Future Vol, veh/h | | 0 | 0 | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | | - | None |
| Storage Length | - - | - | - | - | 0 | - |
| Veh in Median Storage | • | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | | | | |
| Major/Minor I | Major1 | ı | Major2 | | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 2 | 1 |
| Stage 1 | - | - | | - | 1 | |
| Stage 2 | - | _ | - | - | 1 | - |
| Critical Hdwy | | | 4.12 | | 6.42 | 6.22 |
| • | - | - | 4.12 | - | | 0.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1622 | - | 1021 | 1084 |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 1022 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1622 | - | 1021 | 1084 |
| Mov Cap-2 Maneuver | - | - | - | - | 1021 | - |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | _ | _ | - | _ | 1022 | _ |
| 5 to go _ | | | | | | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvm | + 1 | NBLn1 | EBT | EBR | WBL | WBT |
| | ı I | | | | | |
| Capacity (veh/h) | | - | - | - | | - |
| HCM Lane V/C Ratio | | - | - | - | - | - |
| HCM Control Delay (s) | | 0 | - | - | 0 | - |
| HCM Lane LOS | | Α | - | - | Α | - |
| HCM 95th %tile Q(veh) | | - | - | - | 0 | - |
| | | | | | | |

| Intersection | | | | | | |
|--|-------|-------|--------|------|--------|------|
| Int Delay, s/veh | 2.9 | | | | | |
| | | | | 14/5 | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | f) | | | 4 | ¥ | |
| Traffic Vol, veh/h | 44 | 148 | 10 | 15 | 66 | 10 |
| Future Vol, veh/h | 44 | 148 | 10 | 15 | 66 | 10 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 52 | 174 | 12 | 18 | 78 | 12 |
| | | | | | | |
| Major/Minor Ma | ajor1 | ı | Major2 | N | Minor1 | |
| | | | | | | 120 |
| Conflicting Flow All | 0 | 0 | 226 | 0 | 181 | 139 |
| Stage 1 | - | - | - | - | 139 | - |
| Stage 2 | - | - | - | - | 42 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | |
| Pot Cap-1 Maneuver | - | - | 1342 | - | 808 | 909 |
| Stage 1 | - | - | - | - | 888 | - |
| Stage 2 | - | - | - | - | 980 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1342 | - | 801 | 909 |
| Mov Cap-2 Maneuver | - | - | - | - | 801 | - |
| Stage 1 | - | - | - | - | 888 | - |
| Stage 2 | - | - | - | - | 971 | - |
| , and the second | | | | | | |
| Annacah | ED | | \A/D | | ND | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.1 | | 10 | |
| HCM LOS | | | | | В | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 814 | | | 1342 | _ |
| HCM Lane V/C Ratio | | 0.11 | _ | | 0.009 | _ |
| HCM Control Delay (s) | | 10 | _ | _ | | 0 |
| HCM Lane LOS | | В | _ | _ | Α. | A |
| HCM 95th %tile Q(veh) | | 0.4 | _ | _ | 0 | - |
| | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|-------------|----------|--------|------|-------|--------|-------|-------|---------|------|------|
| Int Delay, s/veh | 6.9 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ች | ∱ 1> | | ች | ħβ | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 1 | 134 | 14 | 40 | 161 | 91 | 8 | 6 | 37 | 193 | 19 | 0 |
| Future Vol, veh/h | 1 | 134 | 14 | 40 | 161 | 91 | 8 | 6 | 37 | 193 | 19 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 190 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 1 | 151 | 16 | 45 | 181 | 102 | 9 | 7 | 42 | 217 | 21 | 0 |
| | | | | | | | | | | | | |
| Major/Minor N | Major1 | | <u> </u> | Major2 | | | Minor1 | | N | /linor2 | | |
| Conflicting Flow All | 283 | 0 | 0 | 167 | 0 | 0 | 352 | 534 | 84 | 403 | 491 | 142 |
| Stage 1 | - | - | - | - | - | - | 161 | 161 | - | 322 | 322 | - |
| Stage 2 | - | - | - | - | - | - | 191 | 373 | - | 81 | 169 | - |
| Critical Hdwy | 4.14 | - | - | 4.14 | - | - | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Follow-up Hdwy | 2.22 | - | - | 2.22 | - | - | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap-1 Maneuver | 1276 | - | - | 1408 | - | - | 578 | 451 | 958 | 532 | 477 | 880 |
| Stage 1 | - | - | - | - | - | - | 825 | 764 | - | 664 | 650 | - |
| Stage 2 | - | - | - | - | - | - | 792 | 617 | - | 918 | 758 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1276 | - | - | 1408 | - | - | 544 | 436 | 958 | 491 | 461 | 880 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 544 | 436 | - | 491 | 461 | - |
| Stage 1 | - | - | - | - | - | - | 824 | 763 | - | 663 | 629 | - |
| Stage 2 | - | - | - | - | - | - | 741 | 597 | - | 870 | 757 | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.1 | | | 1 | | | 10.1 | | | 19.2 | | |
| HCM LOS | | | | | | | В | | | С | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t l | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR : | SBLn1 | | | |
| Capacity (veh/h) | | 760 | | | | 1408 | - | - | 488 | | | |
| HCM Lane V/C Ratio | | 0.075 | | _ | | 0.032 | _ | _ | 0.488 | | | |
| HCM Control Delay (s) | | 10.1 | 7.8 | _ | - | 7.6 | _ | _ | | | | |
| HCM Lane LOS | | В | A | _ | _ | A | - | - | C | | | |
| HCM 95th %tile Q(veh) | | 0.2 | 0 | - | - | 0.1 | - | - | 2.6 | | | |
| | | | | | | | | | | | | |

Page 3

3: N Plaza Drive & W Ferguson Ave

| | ۶ | • | • | 4 | † | / | > | ļ | 4 | |
|------------------------|------|------|------|------|----------|----------|-------------|------|------|--|
| Lane Group | EBL | EBR | WBL | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Group Flow (vph) | 16 | 78 | 8 | 98 | 570 | 8 | 7 | 788 | 30 | |
| v/c Ratio | 0.09 | 0.21 | 0.06 | 0.72 | 0.21 | 0.01 | 0.05 | 0.35 | 0.03 | |
| Control Delay | 25.1 | 1.2 | 29.6 | 60.8 | 4.2 | 0.0 | 29.3 | 7.3 | 0.0 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| otal Delay | 25.1 | 1.2 | 29.6 | 60.8 | 4.2 | 0.0 | 29.3 | 7.3 | 0.0 | |
| ueue Length 50th (ft) | 6 | 0 | 3 | 36 | 21 | 0 | 2 | 66 | 0 | |
| Queue Length 95th (ft) | 20 | 0 | 15 | #118 | 96 | 0 | 14 | 139 | 0 | |
| nternal Link Dist (ft) | | | | | 1413 | | | 2950 | | |
| urn Bay Length (ft) | 200 | 110 | 120 | 250 | | 275 | 305 | | 110 | |
| ase Capacity (vph) | 187 | 917 | 137 | 137 | 2709 | 1239 | 137 | 2236 | 1043 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| torage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.09 | 0.09 | 0.06 | 0.72 | 0.21 | 0.01 | 0.05 | 0.35 | 0.03 | |
| ntersection Summary | | | | | | | | | | |

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

Synchro 11 Report Kimley-Horn Queues

| | <u> </u> | | _ | | + | 4 | • | † | <i>▶</i> | _ | 1 | 7 |
|--|----------|------------|--------------|----------|----------|------|----------|----------|----------|--------------|----------|------|
| | | _ | * | * | | | , | ı | / | - | * | - |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \ | ↑ ↑ | 7 | <u> </u> | * | 7 | \ | ^ | Ť | * | ^ | 7 |
| Traffic Volume (veh/h) | 14 | 0 | 69 | 7 | 0 | 0 | 87 | 507 | 7 | 6 | 701 | 27 |
| Future Volume (veh/h) | 14 | 0 | 69 | 7 | 0 | 0 | 87 | 507 | 7 | 6 | 701 | 27 |
| Initial Q (Qb), veh | 1.00 | 0 | 0 | 0 | 0 | 1.00 | 1.00 | 0 | 0 | 1.00 | 0 | 1.00 |
| Ped-Bike Adj(A_pbT) | 1.00 | 1.00 | 1.00 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 1.00 | 1.00 | 1.00 |
| Parking Bus, Adj | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 | 1.00 | No | 1.00 |
| Work Zone On Approach | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Sat Flow, veh/h/ln | 1670 | | 78 | 8 | 1070 | 0 | 98 | 570 | 8 | | 788 | 30 |
| Adj Flow Rate, veh/h Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 7 0.89 | 0.89 | 0.89 |
| | 0.09 | 0.09 | 0.09 | 0.09 | 0.69 | 0.69 | 0.69 | 0.09 | 0.69 | 0.09 | 0.69 | 0.09 |
| Percent Heavy Veh, % Cap, veh/h | 34 | 239 | 106 | 18 | 207 | 92 | 125 | 2255 | 1006 | 16 | 2037 | 909 |
| Arrive On Green | 0.02 | 0.00 | 0.07 | 0.01 | 0.00 | 0.00 | 0.07 | 0.63 | 0.63 | 0.01 | 0.57 | 0.57 |
| | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Sat Flow, veh/h | | | | | | | | | | | | |
| Grp Volume(v), veh/h | 16 | 0 | 78 | 8 | 0 | 0 | 98 | 570 | 8 | 7 | 788 | 30 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 0.6 | 0.0 | 3.1 | 0.3 | 0.0 | 0.0 | 3.5 | 4.5 | 0.1 | 0.3 | 7.8 | 0.5 |
| Cycle Q Clear(g_c), s | 0.6 | 0.0 | 3.1 | 0.3 | 0.0 | 0.0 | 3.5 | 4.5 | 0.1 | 0.3 | 7.8 | 0.5 |
| Prop In Lane | 1.00 | 020 | 1.00 | 1.00 | 007 | 1.00 | 1.00 | 0055 | 1.00 | 1.00 | 0007 | 1.00 |
| Lane Grp Cap(c), veh/h | 34 | 239 | 106 | 18 | 207 | 92 | 125 | 2255 | 1006 | 16 | 2037 | 909 |
| V/C Ratio(X) | 0.46 | 0.00 | 0.73 | 0.43 | 0.00 | 0.00 | 0.78 | 0.25 | 0.01 | 0.43 | 0.39 | 0.03 |
| Avail Cap(c_a), veh/h | 138 | 1723 | 769 | 138 | 1762 | 786 | 138 | 2255 | 1006 | 138 | 2037 | 909 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 31.3 | 0.0 | 29.5 | 31.8 | 0.0 | 0.0 | 29.5 | 5.1 | 4.3 | 31.8 | 7.6 | 6.0 |
| Incr Delay (d2), s/veh | 9.4 | 0.0 | 9.3 | 15.3 | 0.0 | 0.0 | 22.7 | 0.3 | 0.0 | 16.9 | 0.6 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.3 | 0.0 | 1.4 | 0.2 | 0.0 | 0.0 | 2.1 | 0.9 | 0.0 | 0.2 | 2.0 | 0.2 |
| Unsig. Movement Delay, s/veh | | 0.0 | 20.0 | 47.0 | 0.0 | 0.0 | 52.2 | 5.4 | 4.3 | 48.7 | 8.1 | 6.1 |
| LnGrp Delay(d),s/veh | 40.8 | 0.0 | 38.8 | 47.0 | 0.0 | 0.0 | | | | | | |
| LnGrp LOS | D | A 0.4 | D | D | A | A | D | A 070 | A | D | A | A |
| Approach Vol, veh/h | | 94 | | | 8 | | | 676 | | | 825 | |
| Approach Delay, s/veh | | 39.2 | | | 47.0 | | | 12.2 | | | 8.4 | |
| Approach LOS | | D | | | D | | | В | | | Α | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 5.1 | 45.5 | 5.2 | 8.8 | 9.0 | 41.5 | 5.7 | 8.3 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 37.0 | 5.0 | 31.3 | 5.0 | 37.0 | 5.0 | 32.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.3 | 6.5 | 2.3 | 5.1 | 5.5 | 9.8 | 2.6 | 0.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.5 | 0.0 | 0.2 | 0.0 | 5.1 | 0.0 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 12.0 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|------------------------|-----------|-------|----------|-----------|-------|--------|-----------|----------|----------|---------|------|----------|
| Int Delay, s/veh | 3.6 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ĵ. | | | 4 | | | ħβ | | ሻ | ħβ | |
| Traffic Vol, veh/h | 20 | 0 | 31 | 1 | 0 | 1 | 211 | 594 | 19 | 5 | 638 | 140 |
| Future Vol, veh/h | 20 | 0 | 31 | 1 | 0 | 1 | 211 | 594 | 19 | 5 | 638 | 140 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | | None | - | - | None | - | - | None |
| Storage Length | 0 | - | - | - | - | - | 150 | - | _ | 150 | - | - |
| Veh in Median Storage | ,# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 | 86 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 23 | 0 | 36 | 1 | 0 | 1 | 245 | 691 | 22 | 6 | 742 | 163 |
| | | | | | | | | | | | | |
| Major/Minor N | Minor2 | | ı | Minor1 | | ı | Major1 | | N | //ajor2 | | |
| Conflicting Flow All | 1672 | 2039 | 453 | 1575 | 2109 | 357 | 905 | 0 | 0 | 713 | 0 | 0 |
| Stage 1 | 836 | 836 | - | 1192 | 1192 | - | - | - | - | - | - | - |
| Stage 2 | 836 | 1203 | <u>-</u> | 383 | 917 | _ | <u>-</u> | <u>-</u> | _ | _ | _ | <u>-</u> |
| Critical Hdwy | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 | 4.14 | _ | _ | 4.14 | _ | _ |
| Critical Hdwy Stg 1 | 6.54 | 5.54 | - | 6.54 | 5.54 | - 0.07 | - 1.17 | <u>-</u> | _ | | _ | <u>-</u> |
| Critical Hdwy Stg 2 | 6.54 | 5.54 | _ | 6.54 | 5.54 | _ | _ | _ | _ | _ | _ | _ |
| Follow-up Hdwy | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 | 2.22 | _ | _ | 2.22 | _ | _ |
| Pot Cap-1 Maneuver | 63 | 56 | 554 | 74 | 51 | 639 | 747 | _ | _ | 883 | _ | _ |
| Stage 1 | 328 | 381 | - | 199 | 259 | - | - | _ | _ | - | _ | _ |
| Stage 2 | 328 | 256 | _ | 611 | 349 | _ | _ | _ | _ | _ | _ | _ |
| Platoon blocked, % | 020 | 200 | | 011 | 0-10 | | | _ | <u>-</u> | | _ | <u>-</u> |
| Mov Cap-1 Maneuver | 47 | 37 | 554 | 51 | 34 | 639 | 747 | _ | _ | 883 | _ | _ |
| Mov Cap-1 Maneuver | 47 | 37 | - | 51 | 34 | - | - | _ | _ | - | _ | <u>-</u> |
| Stage 1 | 220 | 378 | _ | 134 | 174 | _ | _ | _ | _ | _ | _ | _ |
| Stage 2 | 220 | 172 | _ | 567 | 347 | - | _ | _ | _ | _ | - | _ |
| J. 10 2 | | | | 301 | 317 | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 62.6 | | | 44.3 | | | 3.1 | | | 0.1 | | |
| HCM LOS | 02.0 F | | | ++.5 E | | | J. 1 | | | J. 1 | | |
| TOW LOO | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBL | NBT | NBR I | EBLn1 | EBLn2V | VBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 747 | - | _ | 47 | 554 | 94 | 883 | - | - | | |
| HCM Lane V/C Ratio | | 0.328 | _ | _ | | 0.065 | | | _ | _ | | |
| HCM Control Delay (s) | | 12.2 | _ | | 141.1 | 12 | 44.3 | 9.1 | _ | _ | | |
| HCM Lane LOS | | В | _ | _ | F | В | ++.0 E | A | _ | _ | | |
| HCM 95th %tile Q(veh) | | 1.4 | _ | _ | 1.8 | 0.2 | 0.1 | 0 | _ | _ | | |
| | | 1.1 | | | 1.5 | J.L | J. 1 | | | | | |

| | ۶ | → | • | • | ← | • | 4 | † | / | > | ļ | 4 |
|-------------------------|------|----------|------|------|----------|------|-------|----------|------|-------------|------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 67 | 168 | 202 | 86 | 134 | 133 | 199 | 699 | 71 | 128 | 517 | 51 |
| v/c Ratio | 0.63 | 0.42 | 0.56 | 0.80 | 0.33 | 0.45 | 1.09 | 0.41 | 0.09 | 0.70 | 0.30 | 0.06 |
| Control Delay | 65.5 | 37.1 | 11.9 | 88.1 | 35.7 | 11.6 | 131.5 | 14.8 | 1.5 | 57.5 | 13.6 | 0.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 65.5 | 37.1 | 11.9 | 88.1 | 35.7 | 11.6 | 131.5 | 14.8 | 1.5 | 57.5 | 13.6 | 0.4 |
| Queue Length 50th (ft) | 34 | 43 | 0 | 45 | 34 | 0 | ~117 | 115 | 0 | 65 | 80 | 0 |
| Queue Length 95th (ft) | #99 | 73 | 59 | #131 | 60 | 48 | #256 | 170 | 12 | #153 | 123 | 3 |
| Internal Link Dist (ft) | | 2572 | | | 1230 | | | 2364 | | | 1021 | |
| Turn Bay Length (ft) | 250 | | 110 | 250 | | 90 | 330 | | 105 | 170 | | 140 |
| Base Capacity (vph) | 107 | 1588 | 821 | 107 | 1588 | 783 | 182 | 1713 | 820 | 184 | 1718 | 821 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.63 | 0.11 | 0.25 | 0.80 | 0.08 | 0.17 | 1.09 | 0.41 | 0.09 | 0.70 | 0.30 | 0.06 |

Intersection Summary

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

| | ٠ | → | • | • | ← | • | • | † | ~ | \ | + | √ |
|------------------------------|------|----------|------|------|----------|------|-------|----------|------|----------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ř | ^ | 7 | * | ^ | 7 | * | ^ | 7 | * | ^ | 7 |
| Traffic Volume (veh/h) | 62 | 156 | 188 | 80 | 125 | 124 | 185 | 650 | 66 | 119 | 481 | 47 |
| Future Volume (veh/h) | 62 | 156 | 188 | 80 | 125 | 124 | 185 | 650 | 66 | 119 | 481 | 47 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 67 | 168 | 202 | 86 | 134 | 133 | 199 | 699 | 71 | 128 | 517 | 51 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 86 | 578 | 258 | 102 | 611 | 272 | 174 | 1659 | 740 | 159 | 1630 | 727 |
| Arrive On Green | 0.05 | 0.16 | 0.16 | 0.06 | 0.17 | 0.17 | 0.10 | 0.47 | 0.47 | 0.09 | 0.46 | 0.46 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 67 | 168 | 202 | 86 | 134 | 133 | 199 | 699 | 71 | 128 | 517 | 51 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 3.2 | 3.6 | 10.7 | 4.2 | 2.8 | 6.6 | 8.5 | 11.4 | 2.2 | 6.1 | 8.0 | 1.6 |
| Cycle Q Clear(g_c), s | 3.2 | 3.6 | 10.7 | 4.2 | 2.8 | 6.6 | 8.5 | 11.4 | 2.2 | 6.1 | 8.0 | 1.6 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 86 | 578 | 258 | 102 | 611 | 272 | 174 | 1659 | 740 | 159 | 1630 | 727 |
| V/C Ratio(X) | 0.78 | 0.29 | 0.78 | 0.84 | 0.22 | 0.49 | 1.15 | 0.42 | 0.10 | 0.80 | 0.32 | 0.07 |
| Avail Cap(c_a), veh/h | 102 | 1508 | 673 | 102 | 1508 | 673 | 174 | 1659 | 740 | 176 | 1630 | 727 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.0 | 32.1 | 35.0 | 40.7 | 31.1 | 32.6 | 39.3 | 15.4 | 13.0 | 38.9 | 14.9 | 13.2 |
| Incr Delay (d2), s/veh | 26.8 | 0.3 | 5.2 | 43.7 | 0.2 | 1.4 | 113.0 | 0.8 | 0.3 | 21.4 | 0.5 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.0 | 1.5 | 4.2 | 3.0 | 1.2 | 2.5 | 8.9 | 4.1 | 0.7 | 3.4 | 2.9 | 0.5 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 67.8 | 32.4 | 40.2 | 84.4 | 31.3 | 34.0 | 152.3 | 16.2 | 13.2 | 60.4 | 15.5 | 13.4 |
| LnGrp LOS | Е | С | D | F | С | С | F | В | В | Е | В | В |
| Approach Vol, veh/h | | 437 | | | 353 | | | 969 | | | 696 | |
| Approach Delay, s/veh | | 41.4 | | | 45.2 | | | 43.9 | | | 23.6 | |
| Approach LOS | | D | | | D | | | D | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.3 | 46.7 | 9.5 | 18.7 | 13.0 | 46.0 | 8.7 | 19.5 | | | | |
| Change Period (Y+Rc), s | 4.5 | 6.0 | 4.5 | 4.5 | 4.5 | 6.0 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 8.6 | 39.9 | 5.0 | 37.0 | 8.5 | 40.0 | 5.0 | 37.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 8.1 | 13.4 | 6.2 | 12.7 | 10.5 | 10.0 | 5.2 | 8.6 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.5 | 0.0 | 1.5 | 0.0 | 3.2 | 0.0 | 1.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 37.9 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| Intersection | | | | | | |
|---|----------|--------|--------|------|--------|-------|
| Int Delay, s/veh | 7.6 | | | | | |
| | | EDD | WDI | WDT | NDI | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ₽ | 0 | 470 | र्न | À | 00 |
| Traffic Vol, veh/h | 0 | 0 | 176 | 0 | 0 | 26 |
| Future Vol, veh/h | 0 | 0 | 176 | 0 | 0 | 26 |
| Conflicting Peds, #/hr | _ 0 | _ 0 | _ 0 | _ 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 191 | 0 | 0 | 28 |
| | | | | | | |
| Major/Minor N | Noior1 | | Major2 | | Minor1 | |
| | //ajor1 | | | | | 1 |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 383 | 1 |
| Stage 1 | - | - | - | - | 1 | - |
| Stage 2 | - | - | - | - | 382 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1622 | - | 620 | 1084 |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 690 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1622 | - | 547 | 1084 |
| Mov Cap-2 Maneuver | - | _ | _ | _ | 547 | - |
| Stage 1 | _ | _ | _ | _ | 1022 | - |
| Stage 2 | _ | _ | - | _ | 609 | _ |
| J. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. | | | | | 300 | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 7.5 | | 8.4 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Long/Major Mund | | IDI -1 | EDT | EBR | WDI | WDT |
| Minor Lane/Major Mymt | . 1 | NBLn1 | EBT | | WBL | WBT |
| Capacity (veh/h) | | 1084 | - | | 1622 | - |
| HCM Lane V/C Ratio | | 0.026 | - | | 0.118 | - |
| HCM Control Delay (s) | | 8.4 | - | - | 7.5 | 0 |
| HCM Lane LOS | | A | - | - | A | Α |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 0.4 | - |
| | | | | | | |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|----------|--------|-------|
| Int Delay, s/veh | 3.8 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 1 | | | 4 | ¥ | |
| Traffic Vol, veh/h | 26 | 0 | 175 | 176 | 0 | 25 |
| Future Vol, veh/h | 26 | 0 | 175 | 176 | 0 | 25 |
| Conflicting Peds, #/hr | | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | _ | | _ | None | - | None |
| Storage Length | _ | - | - | - | 0 | - |
| Veh in Median Storag | ie,# 0 | _ | _ | 0 | 0 | - |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 28 | 0 | 190 | 191 | 0 | 27 |
| WWW.CT IOW | 20 | V | 100 | 101 | · · | 21 |
| | | | | _ | | |
| Major/Minor | Major1 | N | Major2 | <u> </u> | Minor1 | |
| Conflicting Flow All | 0 | 0 | 28 | 0 | 599 | 28 |
| Stage 1 | - | - | - | - | 28 | - |
| Stage 2 | - | - | - | - | 571 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1585 | - | 465 | 1047 |
| Stage 1 | - | - | - | - | 995 | - |
| Stage 2 | - | - | - | - | 565 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | _ | 1585 | - | 403 | 1047 |
| Mov Cap-2 Maneuver | | - | - | - | 403 | - |
| Stage 1 | _ | _ | - | - | 995 | _ |
| Stage 2 | _ | _ | _ | _ | 489 | _ |
| 5 ta gu = | | | | | | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.8 | | 8.5 | |
| HCM LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvi | mt I | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1047 | - | - | 1585 | - |
| HCM Lane V/C Ratio | | 0.026 | _ | _ | 0.12 | _ |
| HCM Control Delay (s | 3) | 8.5 | _ | _ | 7.6 | 0 |
| HCM Lane LOS | , | A | _ | _ | Α | A |
| HCM 95th %tile Q(vel | h) | 0.1 | - | - | 0.4 | - |
| | , | | | | | |

| Intersection | | | | | | |
|------------------------|------------|-------|--------|-------|---------|-------|
| Int Delay, s/veh | 5.1 | | | | | |
| | | EDD | \\/DI | \\/DT | NDL | NIDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | } | 00 | 40 | 4 | 420 | 40 |
| Traffic Vol, veh/h | 18 | 86 | 10 | 38 | 130 | 10 |
| Future Vol, veh/h | 18 | 86 | 10 | 38 | 130 | 10 |
| Conflicting Peds, #/hr | _ 0 | _ 0 | _ 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 20 | 93 | 11 | 41 | 141 | 11 |
| | | | | | | |
| Major/Minor | Mais =1 | | Mais 2 | | Mineral | |
| | Major1 | | Major2 | | Minor1 | ^- |
| Conflicting Flow All | 0 | 0 | 113 | 0 | 130 | 67 |
| Stage 1 | - | - | - | - | 67 | - |
| Stage 2 | - | - | - | - | 63 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1476 | - | 864 | 997 |
| Stage 1 | - | _ | - | - | 956 | - |
| Stage 2 | _ | - | - | _ | 960 | - |
| Platoon blocked, % | _ | _ | | _ | | |
| Mov Cap-1 Maneuver | _ | | 1476 | _ | 857 | 997 |
| Mov Cap-2 Maneuver | _ | | - | _ | 857 | - |
| | - | - | | | 956 | - |
| Stage 1 | | - | - | - | | |
| Stage 2 | - | - | - | - | 952 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 1.6 | | 10 | |
| HCM LOS | - 0 | | 1.0 | | В | |
| TOW LOO | | | | | U | |
| | | | | | | |
| Minor Lane/Major Mvm | <u>t 1</u> | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 866 | - | - | 1476 | - |
| HCM Lane V/C Ratio | | 0.176 | - | - | 0.007 | - |
| HCM Control Delay (s) | | 10 | - | - | 7.5 | 0 |
| HCM Lane LOS | | В | - | - | A | A |
| | | | | | | - |
| HCM 95th %tile Q(veh) |) | 0.6 | - | - | 0 | - |

| Intersection | | | | | | | | | | | | |
|------------------------|--------|------------|------|--------|------------|----------|--------|-------|-------------------|---------|------|------|
| Int Delay, s/veh | 6.2 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ħ | ↑ } | | ሻ | ↑ ↑ | | | 4 | | | 4 | |
| Traffic Vol, veh/h | 7 | 224 | 15 | 38 | 141 | 140 | 15 | 19 | 77 | 131 | 28 | 7 |
| Future Vol, veh/h | 7 | 224 | 15 | 38 | 141 | 140 | 15 | 19 | 77 | 131 | 28 | 7 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | ·- | - | None |
| Storage Length | 90 | - | - | 190 | - | - | - | - | - | - | - | - |
| Veh in Median Storage | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 | 91 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 8 | 252 | 17 | 43 | 158 | 157 | 16 | 21 | 87 | 147 | 31 | 8 |
| | | | | | | | | | | | | |
| Major/Minor N | Major1 | | | Major2 | | <u> </u> | Minor1 | | N | /linor2 | | |
| Conflicting Flow All | 315 | 0 | 0 | 269 | 0 | 0 | 458 | 678 | 135 | 476 | 608 | 158 |
| Stage 1 | - | - | - | - | - | - | 277 | 277 | - | 323 | 323 | - |
| Stage 2 | - | - | - | - | - | - | 181 | 401 | - | 153 | 285 | - |
| Critical Hdwy | 4.14 | - | - | 4.14 | - | - | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.54 | 5.54 | - | 6.54 | 5.54 | - |
| Follow-up Hdwy | 2.22 | - | - | 2.22 | - | - | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 |
| Pot Cap-1 Maneuver | 1242 | - | - | 1292 | - | - | 486 | 373 | 889 | 472 | 409 | 859 |
| Stage 1 | - | - | - | - | - | - | 706 | 680 | - | 663 | 649 | - |
| Stage 2 | - | - | - | - | - | - | 803 | 599 | - | 834 | 674 | - |
| Platoon blocked, % | | - | - | | - | - | | | | | | |
| Mov Cap-1 Maneuver | 1242 | - | - | 1292 | - | - | 438 | 358 | 889 | 395 | 393 | 859 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 438 | 358 | - | 395 | 393 | - |
| Stage 1 | - | - | - | - | - | - | 702 | 676 | - | 659 | 628 | - |
| Stage 2 | - | - | - | - | - | - | 731 | 579 | - | 724 | 670 | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 0.2 | | | 0.9 | | | 12 | | | 21.3 | | |
| HCM LOS | | | | | | | В | | | С | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t1 | NBLn1 | EBL | EBT | EBR | WBL | WBT | WBR : | SBL _{n1} | | | |
| Capacity (veh/h) | | 639 | 1242 | - | - | 1292 | - | - | 404 | | | |
| HCM Lane V/C Ratio | | 0.195 | | - | - | 0.033 | - | - | 0.462 | | | |
| HCM Control Delay (s) | | 12 | 7.9 | - | - | 7.9 | - | - | 21.3 | | | |
| HCM Lane LOS | | В | Α | - | - | Α | - | - | С | | | |
| HCM 95th %tile Q(veh) | | 0.7 | 0 | - | - | 0.1 | - | - | 2.4 | | | |
| | | | | | | | | | | | | |

Intersection Summary

| | ۶ | - | \rightarrow | • | • | 4 | † | / | \ | ↓ | 4 | |
|-------------------------|------|------|---------------|------|------|------|----------|------|----------|----------|------|--|
| Lane Group | EBL | EBT | EBR | WBL | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Group Flow (vph) | 29 | 1 | 68 | 30 | 9 | 63 | 733 | 18 | 4 | 543 | 11 | |
| v/c Ratio | 0.16 | 0.00 | 0.28 | 0.22 | 0.03 | 0.46 | 0.28 | 0.01 | 0.03 | 0.23 | 0.01 | |
| Control Delay | 29.7 | 30.0 | 5.0 | 34.3 | 0.1 | 42.7 | 5.3 | 0.0 | 30.8 | 7.4 | 0.0 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 29.7 | 30.0 | 5.0 | 34.3 | 0.1 | 42.7 | 5.3 | 0.0 | 30.8 | 7.4 | 0.0 | |
| Queue Length 50th (ft) | 10 | 0 | 0 | 11 | 0 | 23 | 28 | 0 | 1 | 42 | 0 | |
| Queue Length 95th (ft) | 36 | 2 | 13 | 37 | 0 | #73 | 132 | 0 | 10 | 95 | 0 | |
| Internal Link Dist (ft) | | 223 | | | | | 1413 | | | 2950 | | |
| Turn Bay Length (ft) | 200 | | 110 | 120 | 105 | 250 | | 275 | 305 | | 110 | |
| Base Capacity (vph) | 187 | 1757 | 845 | 137 | 906 | 137 | 2633 | 1208 | 137 | 2325 | 1080 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.16 | 0.00 | 0.08 | 0.22 | 0.01 | 0.46 | 0.28 | 0.01 | 0.03 | 0.23 | 0.01 | |

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Kimley-Horn Queues

Queue shown is maximum after two cycles.

| | <u> </u> | | _ | | — | 4 | • | + | | _ | ı | J |
|------------------------------|----------|----------|------|----------|------------|------|----------|------------|------|-------------|----------|------|
| | | - | * | • | | | 7 | I | 7 | _ | * | _ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \ | ^ | 7 | \ | ↑ ↑ | 7 | \ | ↑ ↑ | 7 | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 28 | 1 | 67 | 29 | 0 | 9 | 62 | 718 | 18 | 4 | 532 | 11 |
| Future Volume (veh/h) | 28 | 1 | 67 | 29 | 0 | 9 | 62 | 718 | 18 | 4 | 532 | 11 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | 4.00 | 1.00 | 1.00 | 4.00 | 1.00 | 1.00 | 4.00 | 1.00 | 1.00 | 4.00 | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | 4070 | No | 4070 | 4070 | No | 4070 | 4070 | No | 4070 | 4070 | No | 4070 |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 29 | 1 | 68 | 30 | 0 | 9 | 63 | 733 | 18 | 4 | 543 | 11 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 56 | 234 | 105 | 57 | 237 | 106 | 93 | 2198 | 980 | 10 | 2031 | 906 |
| Arrive On Green | 0.03 | 0.07 | 0.07 | 0.03 | 0.00 | 0.07 | 0.05 | 0.62 | 0.62 | 0.01 | 0.57 | 0.57 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 29 | 1 | 68 | 30 | 0 | 9 | 63 | 733 | 18 | 4 | 543 | 11 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 1.0 | 0.0 | 2.7 | 1.1 | 0.0 | 0.3 | 2.2 | 6.4 | 0.3 | 0.1 | 5.0 | 0.2 |
| Cycle Q Clear(g_c), s | 1.0 | 0.0 | 2.7 | 1.1 | 0.0 | 0.3 | 2.2 | 6.4 | 0.3 | 0.1 | 5.0 | 0.2 |
| Prop In Lane | 1.00 | 00.4 | 1.00 | 1.00 | 207 | 1.00 | 1.00 | 0.400 | 1.00 | 1.00 | 0004 | 1.00 |
| Lane Grp Cap(c), veh/h | 56 | 234 | 105 | 57 | 237 | 106 | 93 | 2198 | 980 | 10 | 2031 | 906 |
| V/C Ratio(X) | 0.52 | 0.00 | 0.65 | 0.52 | 0.00 | 0.09 | 0.68 | 0.33 | 0.02 | 0.42 | 0.27 | 0.01 |
| Avail Cap(c_a), veh/h | 138 | 1718 | 766 | 138 | 1756 | 783 | 138 | 2198 | 980 | 138 | 2031 | 906 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 30.9 | 28.3 | 29.5 | 30.8 | 0.0 | 28.4 | 30.1 | 5.9 | 4.8 | 32.1 | 7.0 | 6.0 |
| Incr Delay (d2), s/veh | 7.3 | 0.0 | 6.6 | 7.2 | 0.0 | 0.3 | 8.2 | 0.4 | 0.0 | 26.6 | 0.3 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.5 | 0.0 | 1.2 | 0.6 | 0.0 | 0.1 | 1.1 | 1.4 | 0.1 | 0.1 | 1.3 | 0.1 |
| Unsig. Movement Delay, s/veh | | 00.0 | 00.0 | 00.0 | 0.0 | 00.7 | 00.4 | 0.0 | 4.0 | 50.7 | 7.0 | 0.0 |
| LnGrp Delay(d),s/veh | 38.1 | 28.3 | 36.2 | 38.0 | 0.0 | 28.7 | 38.4 | 6.3 | 4.8 | 58.7 | 7.3 | 6.0 |
| LnGrp LOS | D | C | D | D | A | C | D | A | A | E | A | A |
| Approach Vol, veh/h | | 98 | | | 39 | | | 814 | | | 558 | |
| Approach Delay, s/veh | | 36.7 | | | 35.9 | | | 8.8 | | | 7.7 | |
| Approach LOS | | D | | | D | | | Α | | | Α | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 4.8 | 44.5 | 6.6 | 8.8 | 7.9 | 41.5 | 6.5 | 8.8 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 5.0 | 37.0 | 5.0 | 31.3 | 5.0 | 37.0 | 5.0 | 32.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 2.1 | 8.4 | 3.1 | 4.7 | 4.2 | 7.0 | 3.0 | 2.3 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.7 | 0.0 | 0.2 | 0.0 | 3.3 | 0.0 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 10.9 | | | | | | | | | |
| HCM 6th LOS | | | В | | | | | | | | | |

| Intersection | | | | | | | | | | | | |
|--------------------------------|------------|-----------|--------------|-----------|-------|--------|----------|--------------|--------------|-----------|------------|--------------|
| Int Delay, s/veh | 7.6 | | | | | | | | | | | |
| • * | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Movement Configurations | | | EDK | WDL | | WBR | | | NDK | | | SDR |
| Lane Configurations | 101 | f | 100 | c | - ♣ | 2 | <u>ነ</u> | ↑ } | 2 | <u> </u> | † | 20 |
| Traffic Vol, veh/h | 121 121 | 0 | 182 182 | 6 | 0 | 3 | 31 31 | 651 651 | 3 | 1 1 | 683 683 | 20 |
| Future Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 001 | 0 | 0 | 003 | 0 |
| Conflicting Peds, #/hr | | | | | | | | Free | Free | | Free | |
| Sign Control RT Channelized | Stop - | Stop - | Stop None | Stop - | Stop | Stop | Free | riee - | None | Free - | | Free None |
| Storage Length | 0 | - | NOHE | _ | _ | NOHE - | 150 | - | None - | 150 | - | NOHE |
| | | 0 | - | | 0 | - | 100 | 0 | - | 150 | 0 | |
| Veh in Median Storage Grade, % | , # - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 | 97 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 125 | 0 | 188 | 6 | 0 | 3 | 32 | 671 | 3 | 1 | 704 | 21 |
| WIVIIIL I IOW | 123 | U | 100 | U | U | J | 32 | 011 | J | | 704 | Z 1 |
| | | | | | | | | | | | | |
| | Minor2 | | | Minor1 | | | Major1 | | | Major2 | | |
| Conflicting Flow All | 1117 | 1455 | 363 | 1091 | 1464 | 337 | 725 | 0 | 0 | 674 | 0 | 0 |
| Stage 1 | 717 | 717 | - | 737 | 737 | - | - | - | - | - | - | - |
| Stage 2 | 400 | 738 | - | 354 | 727 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.54 | 6.54 | 6.94 | 7.54 | 6.54 | 6.94 | 4.14 | - | - | 4.14 | - | - |
| Critical Hdwy Stg 1 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | 6.54 | 5.54 | - | 6.54 | 5.54 | - | - | - | - | - | - | - |
| Follow-up Hdwy | 3.52 | 4.02 | 3.32 | 3.52 | 4.02 | 3.32 | 2.22 | - | - | 2.22 | - | - |
| Pot Cap-1 Maneuver | 162 | 129 | 634 | 169 | 127 | 659 | 874 | - | - | 913 | - | - |
| Stage 1 | 387 | 432 | - | 376 | 423 | - | - | - | - | - | - | - |
| Stage 2 | 597 | 422 | - | 636 | 427 | - | - | - | - | - | - | - |
| Platoon blocked, % | 157 | 101 | 60.4 | 110 | 100 | GEO. | 074 | - | - | 042 | - | - |
| Mov Cap-1 Maneuver | 157 | 124 | 634 | 116 | 122 | 659 | 874 | - | - | 913 | - | - |
| Mov Cap-2 Maneuver | 157 | 124 | - | 116 | 122 | - | - | - | - | - | - | - |
| Stage 1 | 373 | 432 | - | 362 | 407 | - | - | - | - | - | - | - |
| Stage 2 | 572 | 406 | - | 447 | 427 | - | - | - | - | - | - | - |
| | | | | | | | | | | | | |
| Approach | EB | | | WB | | | NB | | | SB | | |
| HCM Control Delay, s | 41.1 | | | 28.9 | | | 0.4 | | | 0 | | |
| HCM LOS | Е | | | D | | | | | | | | |
| | | | | | | | | | | | | |
| Minor Lane/Major Mvm | t | NBL | NBT | NBR I | EBLn1 | EBLn2V | VBLn1 | SBL | SBT | SBR | | |
| Capacity (veh/h) | | 874 | _ | - | 4 | 634 | 160 | 913 | _ | _ | | |
| HCM Lane V/C Ratio | | 0.037 | _ | | | 0.296 | 0.058 | 0.001 | _ | _ | | |
| HCM Control Delay (s) | | 9.3 | - | - | | 13 | 28.9 | 8.9 | - | - | | |
| HCM Lane LOS | | A | - | _ | F | В | D | A | _ | _ | | |
| HCM 95th %tile Q(veh) | | 0.1 | - | - | 5.1 | 1.2 | 0.2 | 0 | - | - | | |
| | | | | | | | | | | | | |

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|-------------------------|------|----------|------|------|----------|------|-------|----------|-------------|-------------|------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Group Flow (vph) | 82 | 231 | 231 | 94 | 150 | 114 | 176 | 563 | 63 | 153 | 647 | 65 |
| v/c Ratio | 0.71 | 0.50 | 0.57 | 0.81 | 0.33 | 0.38 | 1.11 | 0.33 | 0.08 | 0.85 | 0.37 | 0.08 |
| Control Delay | 72.4 | 37.8 | 10.8 | 87.0 | 34.9 | 10.6 | 145.4 | 14.0 | 1.1 | 78.2 | 13.9 | 1.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 72.4 | 37.8 | 10.8 | 87.0 | 34.9 | 10.6 | 145.4 | 14.0 | 1.1 | 78.2 | 13.9 | 1.2 |
| Queue Length 50th (ft) | 43 | 60 | 0 | 50 | 38 | 0 | ~107 | 90 | 0 | 80 | 103 | 0 |
| Queue Length 95th (ft) | #121 | 95 | 61 | #140 | 66 | 44 | #242 | 136 | 8 | #197 | 155 | 9 |
| Internal Link Dist (ft) | | 2572 | | | 1230 | | | 2364 | | | 1021 | |
| Turn Bay Length (ft) | 250 | | 110 | 250 | | 90 | 330 | | 105 | 170 | | 140 |
| Base Capacity (vph) | 116 | 1560 | 827 | 116 | 1560 | 762 | 158 | 1729 | 826 | 179 | 1771 | 844 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.71 | 0.15 | 0.28 | 0.81 | 0.10 | 0.15 | 1.11 | 0.33 | 80.0 | 0.85 | 0.37 | 0.08 |

Intersection Summary

Kimley-Horn Queues

Volume exceeds capacity, queue is theoretically infinite.

Queue shown is maximum after two cycles.

^{# 95}th percentile volume exceeds capacity, queue may be longer.

Queue shown is maximum after two cycles.

| | ۶ | → | • | • | — | • | 1 | † | ~ | / | + | ✓ |
|------------------------------|----------|-----------|------|------|----------|------|-------|----------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ^ | 7 | ሻ | ^ | 7 | ሻ | ^ | 7 | 7 | ^↑ | 7 |
| Traffic Volume (veh/h) | 77 | 217 | 217 | 88 | 141 | 107 | 165 | 529 | 59 | 144 | 608 | 61 |
| Future Volume (veh/h) | 77 | 217 | 217 | 88 | 141 | 107 | 165 | 529 | 59 | 144 | 608 | 61 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 82 | 231 | 231 | 94 | 150 | 114 | 176 | 563 | 63 | 153 | 647 | 65 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 105 | 653 | 291 | 110 | 662 | 295 | 149 | 1629 | 727 | 169 | 1669 | 744 |
| Arrive On Green | 0.06 | 0.18 | 0.18 | 0.06 | 0.19 | 0.19 | 0.08 | 0.46 | 0.46 | 0.10 | 0.47 | 0.47 |
| Sat Flow, veh/h | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 82 | 231 | 231 | 94 | 150 | 114 | 176 | 563 | 63 | 153 | 647 | 65 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 4.1 | 5.1 | 12.5 | 4.7 | 3.2 | 5.6 | 7.5 | 9.1 | 2.0 | 7.6 | 10.6 | 2.0 |
| Cycle Q Clear(g_c), s | 4.1 | 5.1 | 12.5 | 4.7 | 3.2 | 5.6 | 7.5 | 9.1 | 2.0 | 7.6 | 10.6 | 2.0 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 105 | 653 | 291 | 110 | 662 | 295 | 149 | 1629 | 727 | 169 | 1669 | 744 |
| V/C Ratio(X) | 0.78 | 0.35 | 0.79 | 0.86 | 0.23 | 0.39 | 1.18 | 0.35 | 0.09 | 0.90 | 0.39 | 0.09 |
| Avail Cap(c_a), veh/h | 110 | 1470 | 656 | 110 | 1470 | 656 | 149 | 1629 | 727 | 169 | 1669 | 744 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.5 | 31.9 | 34.9 | 41.6 | 30.9 | 31.9 | 41.0 | 15.6 | 13.7 | 40.1 | 15.4 | 13.1 |
| Incr Delay (d2), s/veh | 28.7 | 0.3 | 4.9 | 45.2 | 0.2 | 0.8 | 129.5 | 0.6 | 0.2 | 42.7 | 0.7 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 2.5 | 2.1 | 4.9 | 3.3 | 1.3 | 2.1 | 8.4 | 3.3 | 0.7 | 5.1 | 3.8 | 0.7 |
| Unsig. Movement Delay, s/veh | | 20.0 | 20.7 | 00.0 | 24.4 | 20.7 | 470 F | 40.0 | 40.0 | 00.7 | 10.1 | 40.0 |
| LnGrp Delay(d),s/veh | 70.2 | 32.2 C | 39.7 | 86.8 | 31.1 | 32.7 | 170.5 | 16.2 | 13.9 | 82.7 | 16.1 | 13.3 |
| LnGrp LOS | <u>E</u> | | D | F | CC | С | F | В | В | F | В | В |
| Approach Vol, veh/h | | 544 | | | 358 | | | 802 | | | 865 | |
| Approach Delay, s/veh | | 41.1 | | | 46.2 | | | 49.8 | | | 27.6 | |
| Approach LOS | | D | | | D | | | D | | | С | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 13.0 | 45.5 | 10.0 | 20.9 | 12.0 | 46.5 | 9.8 | 21.2 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | 4.5 | | | | |
| Max Green Setting (Gmax), s | 8.5 | 41.0 | 5.5 | 37.0 | 7.5 | 42.0 | 5.5 | 37.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 9.6 | 11.1 | 6.7 | 14.5 | 9.5 | 12.6 | 6.1 | 7.6 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.6 | 0.0 | 2.0 | 0.0 | 4.2 | 0.0 | 1.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 40.0 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

| Intersection | | | | | | |
|---|----------|-------|--------|------|--------|-------|
| Int Delay, s/veh | 8.6 | | | | | |
| | | EDD | WDI | WDT | NDI | NDD |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | ₽ | ^ | 00 | र्न | À | 450 |
| Traffic Vol, veh/h | 0 | 0 | 26 | 0 | 0 | 152 |
| Future Vol, veh/h | 0 | 0 | 26 | 0 | 0 | 152 |
| Conflicting Peds, #/hr | _ 0 | _ 0 | _ 0 | _ 0 | 0 | 0 |
| 3 | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, | | - | - | 0 | 0 | - |
| Grade, % | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 0 | 0 | 28 | 0 | 0 | 165 |
| | | | | | | |
| Major/Minor Major/Minor | ajor1 | ı | Major2 | ı | Minor1 | |
| Conflicting Flow All | 0 | 0 | 1 | 0 | 57 | 1 |
| Stage 1 | - | - | | - | 1 | _ |
| Stage 2 | | _ | _ | _ | 56 | _ |
| Critical Hdwy | _ | _ | 4.12 | _ | 6.42 | 6.22 |
| • | _ | - | 4.12 | - | 5.42 | 0.22 |
| Critical Hdwy Stg 1 Critical Hdwy Stg 2 | | - | - | | 5.42 | - |
| , , | - | - | 0.040 | - | | |
| Follow-up Hdwy | - | | 2.218 | - | | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1622 | - | 950 | 1084 |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 967 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | - | - | 1622 | - | 934 | 1084 |
| Mov Cap-2 Maneuver | - | - | - | - | 934 | - |
| Stage 1 | - | - | - | - | 1022 | - |
| Stage 2 | - | - | - | - | 951 | - |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 7.3 | | 8.9 | |
| HCM LOS | U | | 1.3 | | | |
| HCIVI LOS | | | | | Α | |
| | | | | | | |
| Minor Lane/Major Mvmt | 1 | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 1084 | - | - | 1622 | - |
| HCM Lane V/C Ratio | | 0.152 | - | - | 0.017 | - |
| HCM Control Delay (s) | | 8.9 | - | - | 7.3 | 0 |
| HCM Lane LOS | | Α | - | - | Α | Α |
| | | | | | | |
| HCM 95th %tile Q(veh) | | 0.5 | - | - | 0.1 | - |

| Intersection | | | | | | |
|------------------------|----------|-------|--------|----------|--------|----------|
| Int Delay, s/veh | 4.8 | | | | | |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | <u> </u> | | | 4 | ¥ | |
| Traffic Vol, veh/h | 152 | 0 | 25 | 26 | 0 | 151 |
| Future Vol, veh/h | 152 | 0 | 25 | 26 | 0 | 151 |
| Conflicting Peds, #/hr | | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | | - | | - | None |
| Storage Length | _ | - | _ | - | 0 | - |
| Veh in Median Storag | ie.# 0 | _ | _ | 0 | 0 | _ |
| Grade, % | 0 | _ | _ | 0 | 0 | _ |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 2 | 2 | 2 | 2 | 2 | 2 |
| Mymt Flow | 165 | 0 | 27 | 28 | 0 | 164 |
| WWIIICI IOW | 100 | U | 21 | 20 | U | 104 |
| | | | | | | |
| Major/Minor | Major1 | I | Major2 | <u> </u> | Minor1 | |
| Conflicting Flow All | 0 | 0 | 165 | 0 | 247 | 165 |
| Stage 1 | - | - | - | - | 165 | - |
| Stage 2 | - | - | - | - | 82 | - |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | - | - | 1413 | - | 741 | 879 |
| Stage 1 | - | - | - | - | 864 | - |
| Stage 2 | - | - | - | - | 941 | - |
| Platoon blocked, % | - | - | | - | | |
| Mov Cap-1 Maneuver | r - | - | 1413 | - | 727 | 879 |
| Mov Cap-2 Maneuver | | - | - | - | 727 | - |
| Stage 1 | _ | - | - | - | 864 | _ |
| Stage 2 | _ | _ | _ | _ | 923 | _ |
| olago 2 | | | | | 020 | |
| | | | | | | |
| Approach | EB | | WB | | NB | |
| HCM Control Delay, s | 0 | | 3.7 | | 10 | |
| HCM LOS | | | | | В | |
| | | | | | | |
| Minor Lane/Major Mvi | mt I | NBLn1 | EBT | EBR | WBL | WBT |
| Capacity (veh/h) | | 879 | | | | - |
| HCM Lane V/C Ratio | | 0.187 | _ | | 0.019 | <u>-</u> |
| HCM Control Delay (s | | 10 | _ | _ | 7.6 | 0 |
| HCM Lane LOS | | В | _ | _ | Α. | A |
| HCM 95th %tile Q(vel | h) | 0.7 | _ | _ | 0.1 | - |
| | , | 3.1 | | | J. 1 | |

4: N Plaza Drive & Private Access Road

| | ۶ | → | ← | 4 | † | \ | ļ | ✓ | |
|-------------------------|------|----------|----------|------|----------|----------|------|------|--|
| Lane Group | EBL | EBT | WBT | NBL | NBT | SBL | SBT | SBR | |
| Lane Group Flow (vph) | 23 | 36 | 2 | 245 | 713 | 6 | 742 | 163 | |
| v/c Ratio | 0.09 | 0.07 | 0.01 | 0.51 | 0.26 | 0.03 | 0.51 | 0.22 | |
| Control Delay | 23.4 | 0.3 | 0.0 | 21.3 | 4.0 | 24.2 | 13.8 | 3.5 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 23.4 | 0.3 | 0.0 | 21.3 | 4.0 | 24.2 | 13.8 | 3.5 | |
| Queue Length 50th (ft) | 6 | 0 | 0 | 62 | 30 | 2 | 94 | 0 | |
| Queue Length 95th (ft) | 24 | 0 | 0 | 135 | 97 | 11 | 144 | 27 | |
| Internal Link Dist (ft) | | 1103 | 226 | | 1021 | | 1413 | | |
| Turn Bay Length (ft) | 150 | | | 150 | | 150 | | 190 | |
| Base Capacity (vph) | 841 | 896 | 715 | 604 | 3124 | 409 | 2949 | 1346 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.03 | 0.04 | 0.00 | 0.41 | 0.23 | 0.01 | 0.25 | 0.12 | |
| Intersection Summary | | | | | | | | | |

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| | ۶ | → | * | • | — | • | 1 | † | ~ | / | + | ✓ |
|------------------------------|------|----------|------|------|----------|------|------|------------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ₽ | | | 4 | | ሻ | ∱ β | | 7 | ^↑ | 7 |
| Traffic Volume (veh/h) | 20 | 0 | 31 | 1 | 0 | 1 | 211 | 594 | 19 | 5 | 638 | 140 |
| Future Volume (veh/h) | 20 | 0 | 31 | 1 | 0 | 1 | 211 | 594 | 19 | 5 | 638 | 140 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 23 | 0 | 36 | 1 | 0 | 1 | 245 | 691 | 22 | 6 | 742 | 163 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 | 0.86 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 302 | 0 | 101 | 183 | 4 | 35 | 323 | 1922 | 61 | 14 | 1328 | 592 |
| Arrive On Green | 0.06 | 0.00 | 0.06 | 0.06 | 0.00 | 0.06 | 0.18 | 0.55 | 0.55 | 0.01 | 0.37 | 0.37 |
| Sat Flow, veh/h | 1416 | 0 | 1585 | 484 | 58 | 542 | 1781 | 3515 | 112 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 23 | 0 | 36 | 2 | 0 | 0 | 245 | 349 | 364 | 6 | 742 | 163 |
| Grp Sat Flow(s),veh/h/ln | 1416 | 0 | 1585 | 1084 | 0 | 0 | 1781 | 1777 | 1850 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 | 0.0 | 4.6 | 3.9 | 3.9 | 0.1 | 5.9 | 2.5 |
| Cycle Q Clear(g_c), s | 0.4 | 0.0 | 0.8 | 0.8 | 0.0 | 0.0 | 4.6 | 3.9 | 3.9 | 0.1 | 5.9 | 2.5 |
| Prop In Lane | 1.00 | | 1.00 | 0.50 | | 0.50 | 1.00 | | 0.06 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 302 | 0 | 101 | 222 | 0 | 0 | 323 | 972 | 1012 | 14 | 1328 | 592 |
| V/C Ratio(X) | 0.08 | 0.00 | 0.36 | 0.01 | 0.00 | 0.00 | 0.76 | 0.36 | 0.36 | 0.42 | 0.56 | 0.28 |
| Avail Cap(c_a), veh/h | 1031 | 0 | 918 | 980 | 0 | 0 | 780 | 2283 | 2378 | 528 | 4065 | 1813 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 15.7 | 0.0 | 15.9 | 15.5 | 0.0 | 0.0 | 13.8 | 4.5 | 4.5 | 17.5 | 8.8 | 7.7 |
| Incr Delay (d2), s/veh | 0.1 | 0.0 | 2.1 | 0.0 | 0.0 | 0.0 | 3.7 | 0.2 | 0.2 | 18.0 | 0.4 | 0.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.2 | 0.0 | 0.3 | 0.0 | 0.0 | 0.0 | 1.5 | 0.3 | 0.3 | 0.1 | 1.1 | 0.4 |
| Unsig. Movement Delay, s/veh | | 0.0 | 40.0 | 45.0 | 0.0 | 0.0 | 47.4 | 4-7 | | 05.5 | 0.4 | 0.0 |
| LnGrp Delay(d),s/veh | 15.8 | 0.0 | 18.0 | 15.6 | 0.0 | 0.0 | 17.4 | 4.7 | 4.7 | 35.5 | 9.1 | 8.0 |
| LnGrp LOS | В | A | В | В | A | A | В | A | A | D | A | A |
| Approach Vol, veh/h | | 59 | | | 2 | | | 958 | | | 911 | |
| Approach Delay, s/veh | | 17.2 | | | 15.6 | | | 8.0 | | | 9.1 | |
| Approach LOS | | В | | | В | | | Α | | | Α | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 4.8 | 23.9 | | 6.8 | 10.9 | 17.7 | | 6.8 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | 10.5 | 45.5 | | 20.5 | 15.5 | 40.5 | | 20.5 | | | | |
| Max Q Clear Time (g_c+l1), s | 2.1 | 5.9 | | 2.8 | 6.6 | 7.9 | | 2.8 | | | | |
| Green Ext Time (p_c), s | 0.0 | 4.0 | | 0.2 | 0.4 | 5.4 | | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 8.8 | | | | | | | | | |
| HCM 6th LOS | | | А | | | | | | | | | |

4: N Plaza Drive & Private Access Road

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|-------------------------|------|----------|----------|------|----------|----------|------|------|--|
| | EDI | EDT | MDT | NDI | NDT | ODI | 007 | 000 | |
| Lane Group | EBL | EBT | WBT | NBL | NBT | SBL | SBT | SBR | |
| Lane Group Flow (vph) | 125 | 188 | 9 | 32 | 674 | 1 | 704 | 21 | |
| v/c Ratio | 0.37 | 0.29 | 0.02 | 0.11 | 0.40 | 0.00 | 0.47 | 0.03 | |
| Control Delay | 18.4 | 1.1 | 0.1 | 20.3 | 8.5 | 23.0 | 11.3 | 0.1 | |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | |
| Total Delay | 18.4 | 1.1 | 0.1 | 20.3 | 8.5 | 23.0 | 11.3 | 0.1 | |
| Queue Length 50th (ft) | 15 | 0 | 0 | 4 | 35 | 0 | 36 | 0 | |
| Queue Length 95th (ft) | 78 | 0 | 0 | 32 | 128 | 4 | 146 | 0 | |
| Internal Link Dist (ft) | | 1103 | 226 | | 1021 | | 1413 | | |
| Turn Bay Length (ft) | 150 | | | 150 | | 150 | | 190 | |
| Base Capacity (vph) | 774 | 1027 | 856 | 740 | 3288 | 501 | 3163 | 1428 | |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Reduced v/c Ratio | 0.16 | 0.18 | 0.01 | 0.04 | 0.20 | 0.00 | 0.22 | 0.01 | |
| Intersection Summary | | | | | | | | | |
| intersection Summary | | | | | | | | | |

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| | ၨ | → | * | • | ← | 4 | 1 | † | ~ | / | | 4 |
|------------------------------|------|----------|------|------|----------|------|------|------------|------|----------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | f. | | | 4 | | 7 | ∱ β | | ሻ | ^ | 7 |
| Traffic Volume (veh/h) | 121 | 0 | 182 | 6 | 0 | 3 | 31 | 651 | 3 | 1 | 683 | 20 |
| Future Volume (veh/h) | 121 | 0 | 182 | 6 | 0 | 3 | 31 | 651 | 3 | 1 | 683 | 20 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 |
| Adj Flow Rate, veh/h | 125 | 0 | 188 | 6 | 0 | 3 | 32 | 671 | 3 | 1 | 704 | 21 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 536 | 0 | 312 | 258 | 35 | 56 | 69 | 1430 | 6 | 5 | 1268 | 566 |
| Arrive On Green | 0.20 | 0.00 | 0.20 | 0.20 | 0.00 | 0.20 | 0.04 | 0.39 | 0.39 | 0.00 | 0.36 | 0.36 |
| Sat Flow, veh/h | 1414 | 0 | 1585 | 392 | 175 | 284 | 1781 | 3628 | 16 | 1781 | 3554 | 1585 |
| Grp Volume(v), veh/h | 125 | 0 | 188 | 9 | 0 | 0 | 32 | 329 | 345 | 1 | 704 | 21 |
| Grp Sat Flow(s),veh/h/ln | 1414 | 0 | 1585 | 851 | 0 | 0 | 1781 | 1777 | 1867 | 1781 | 1777 | 1585 |
| Q Serve(g_s), s | 0.0 | 0.0 | 3.6 | 0.0 | 0.0 | 0.0 | 0.6 | 4.6 | 4.6 | 0.0 | 5.3 | 0.3 |
| Cycle Q Clear(g_c), s | 2.0 | 0.0 | 3.6 | 3.6 | 0.0 | 0.0 | 0.6 | 4.6 | 4.6 | 0.0 | 5.3 | 0.3 |
| Prop In Lane | 1.00 | | 1.00 | 0.67 | | 0.33 | 1.00 | | 0.01 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 536 | 0 | 312 | 349 | 0 | 0 | 69 | 700 | 736 | 5 | 1268 | 566 |
| V/C Ratio(X) | 0.23 | 0.00 | 0.60 | 0.03 | 0.00 | 0.00 | 0.47 | 0.47 | 0.47 | 0.19 | 0.56 | 0.04 |
| Avail Cap(c_a), veh/h | 1132 | 0 | 981 | 898 | 0 | 0 | 834 | 2441 | 2566 | 565 | 4346 | 1938 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 11.5 | 0.0 | 12.1 | 10.8 | 0.0 | 0.0 | 15.6 | 7.5 | 7.5 | 16.5 | 8.5 | 6.9 |
| Incr Delay (d2), s/veh | 0.2 | 0.0 | 1.9 | 0.0 | 0.0 | 0.0 | 4.9 | 0.5 | 0.5 | 15.8 | 0.4 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 0.6 | 0.0 | 1.1 | 0.0 | 0.0 | 0.0 | 0.2 | 0.7 | 0.7 | 0.0 | 0.9 | 0.0 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 11.7 | 0.0 | 14.0 | 10.9 | 0.0 | 0.0 | 20.4 | 7.9 | 7.9 | 32.3 | 8.9 | 7.0 |
| LnGrp LOS | В | Α | В | В | Α | Α | С | Α | Α | С | Α | <u>A</u> |
| Approach Vol, veh/h | | 313 | | | 9 | | | 706 | | | 726 | |
| Approach Delay, s/veh | | 13.1 | | | 10.9 | | | 8.5 | | | 8.9 | |
| Approach LOS | | В | | | В | | | Α | | | Α | |
| Timer - Assigned Phs | 1 | 2 | | 4 | 5 | 6 | | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 4.5 | 17.5 | | 11.0 | 5.8 | 16.3 | | 11.0 | | | | |
| Change Period (Y+Rc), s | 4.5 | 4.5 | | 4.5 | 4.5 | 4.5 | | 4.5 | | | | |
| Max Green Setting (Gmax), s | 10.5 | 45.5 | | 20.5 | 15.5 | 40.5 | | 20.5 | | | | |
| Max Q Clear Time (g_c+l1), s | 2.0 | 6.6 | | 5.6 | 2.6 | 7.3 | | 5.6 | | | | |
| Green Ext Time (p_c), s | 0.0 | 3.7 | | 1.3 | 0.0 | 4.6 | | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 9.5 | | | | | | | | | |
| HCM 6th LOS | | | Α | | | | | | | | | |

E – ITE Trip Generation Excerpts

Land Use: 110 General Light Industrial

Description

A light industrial facility is a free-standing facility devoted to a single use. The facility has an emphasis on activities other than manufacturing and typically has minimal office space. Typical light industrial activities include printing, material testing, and assembly of data processing equipment. Industrial park (Land Use 130) and manufacturing (Land Use 140) are related uses.

Additional Data

The technical appendices provide supporting information on time-of-day distributions for this land use. The appendices can be accessed through either the ITETripGen web app or the trip generation resource page on the ITE website (https://www.ite.org/technical-resources/topics/trip-and-parking-generation/).

The sites were surveyed in the 1980s, the 2000s, and the 2010s in Colorado, Connecticut, Indiana, New Jersey, New York, Oregon, Pennsylvania, and Texas.

Source Numbers

106, 157, 174, 177, 179, 184, 191, 251, 253, 286, 300, 611, 874, 875, 912



Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday

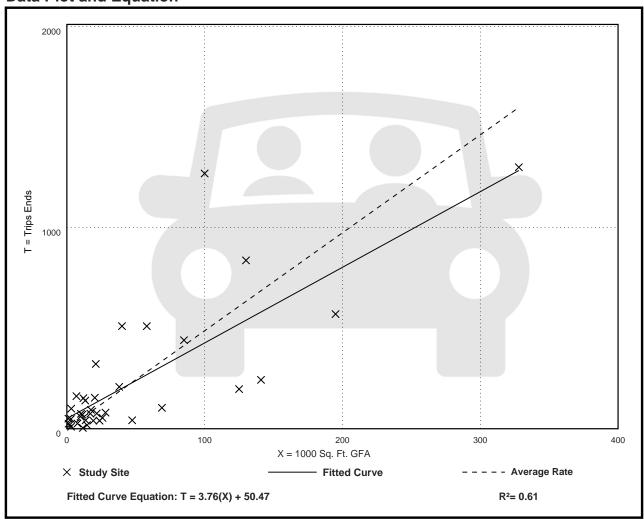
Setting/Location: General Urban/Suburban

Number of Studies: 37 Avg. 1000 Sq. Ft. GFA: 45

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 4.87 | 0.34 - 43.86 | 4.08 |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

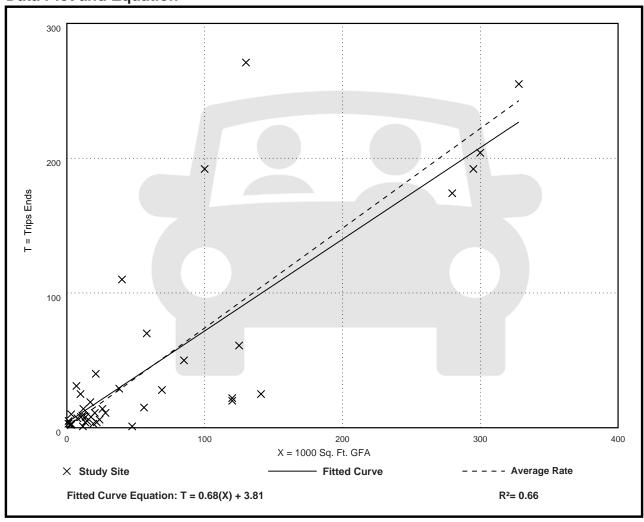
Setting/Location: General Urban/Suburban

Number of Studies: 41 Avg. 1000 Sq. Ft. GFA: 65

Directional Distribution: 88% entering, 12% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.74 | 0.02 - 4.46 | 0.61 |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

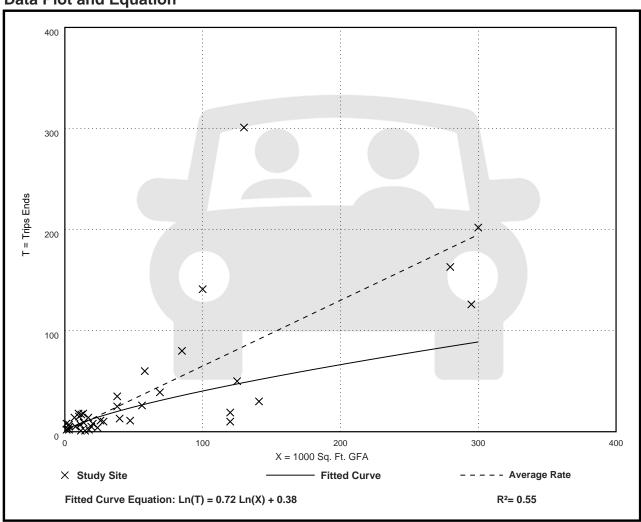
Setting/Location: General Urban/Suburban

Number of Studies: 40 Avg. 1000 Sq. Ft. GFA: 58

Directional Distribution: 14% entering, 86% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.65 | 0.07 - 7.02 | 0.56 |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Weekday,

AM Peak Hour of Generator

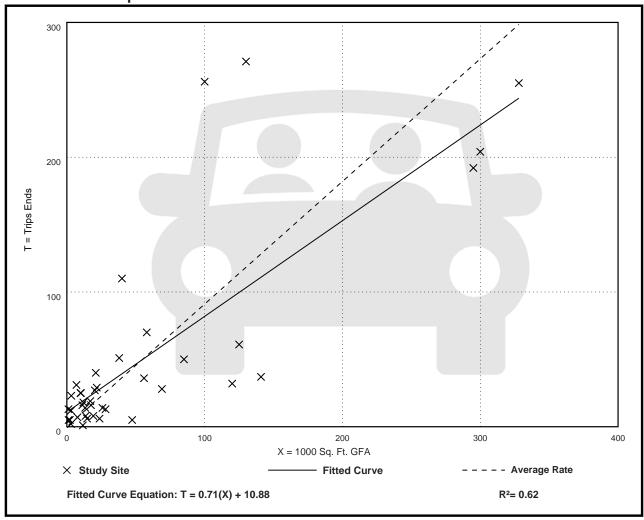
Setting/Location: General Urban/Suburban

Number of Studies: 40 Avg. 1000 Sq. Ft. GFA: 56

Directional Distribution: 87% entering, 13% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.91 | 0.09 - 11.40 | 0.78 |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,

PM Peak Hour of Generator

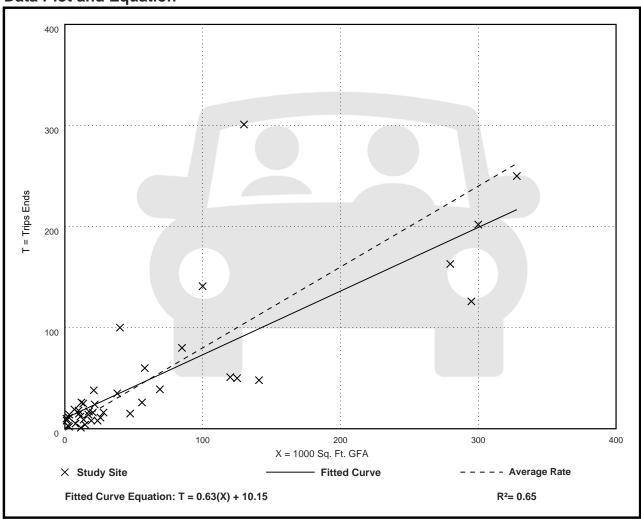
Setting/Location: General Urban/Suburban

Number of Studies: 41 Avg. 1000 Sq. Ft. GFA: 62

Directional Distribution: 18% entering, 82% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| | Average Rate | Range of Rates | Standard Deviation |
|---|--------------|----------------|--------------------|
| ſ | 0.80 | 0.09 - 8.77 | 0.61 |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Saturday

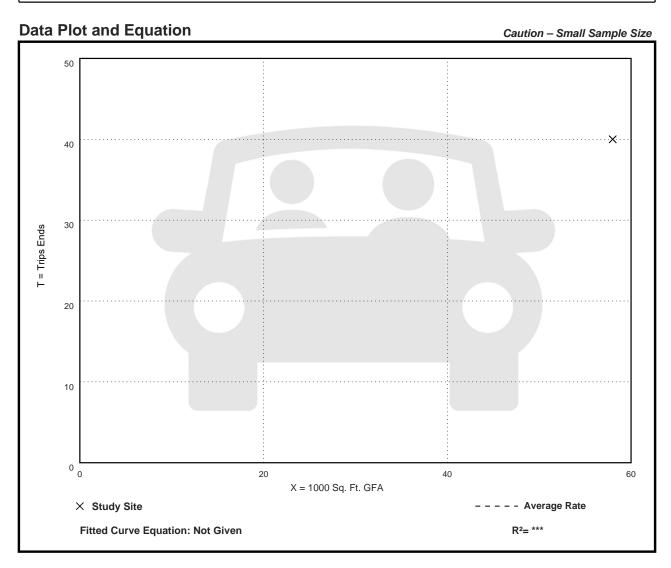
Setting/Location: General Urban/Suburban

Number of Studies: 1 Avg. 1000 Sq. Ft. GFA: 58

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.69 | 0.69 - 0.69 | *** |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Sunday

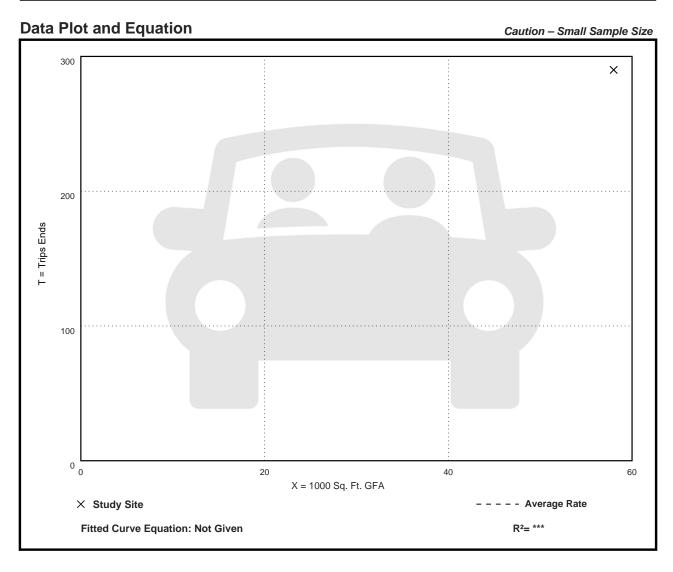
Setting/Location: General Urban/Suburban

Number of Studies: 1 Avg. 1000 Sq. Ft. GFA: 58

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 5.00 | 5.00 - 5.00 | *** |





Vehicle Trip Ends vs: 1000 Sq. Ft. GFA

On a: Sunday, Peak Hour of Generator

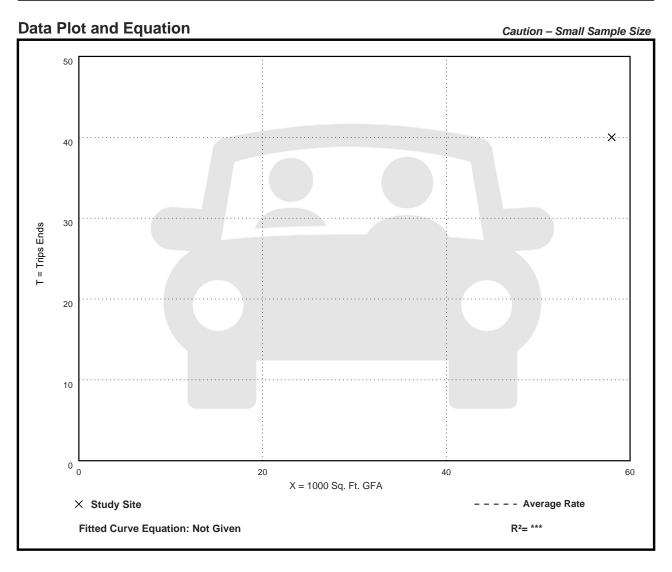
Setting/Location: General Urban/Suburban

Number of Studies: 1 Avg. 1000 Sq. Ft. GFA: 58

Directional Distribution: 48% entering, 52% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.69 | 0.69 - 0.69 | *** |





Vehicle Trip Ends vs: Employees
On a: Weekday

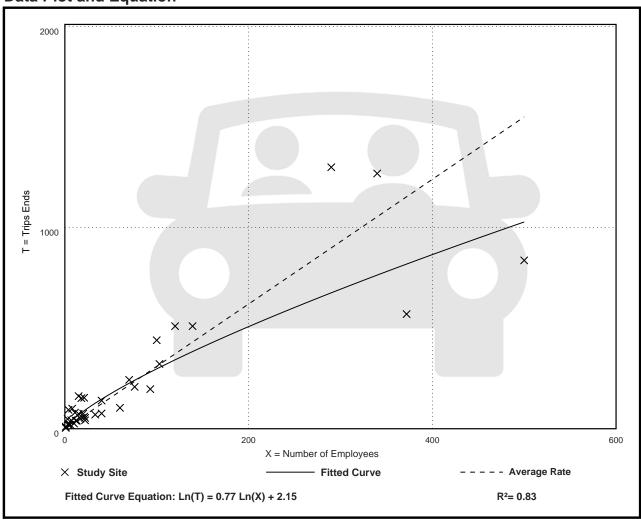
Setting/Location: General Urban/Suburban

Number of Studies: 37 Avg. Num. of Employees: 71

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 3.10 | 1.53 - 23.50 | 1.81 |





Vehicle Trip Ends vs: Employees

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 7 and 9 a.m.

Setting/Location: General Urban/Suburban

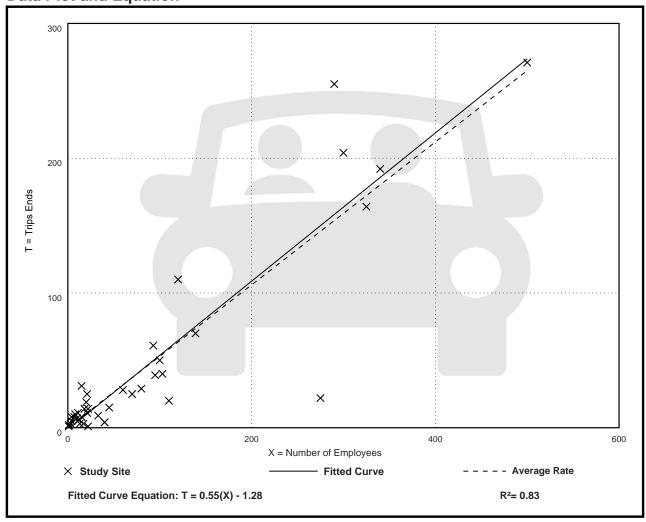
Number of Studies: 41 Avg. Num. of Employees: 83

Directional Distribution: 83% entering, 17% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.53 | 0.05 - 2.07 | 0.27 |

Data Plot and Equation





40

Vehicle Trip Ends vs: Employees

On a: Weekday,

Peak Hour of Adjacent Street Traffic,

One Hour Between 4 and 6 p.m.

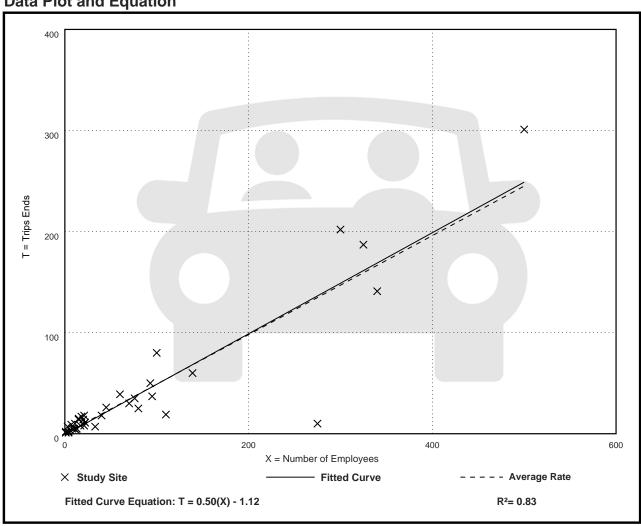
Setting/Location: General Urban/Suburban

Number of Studies: 39 Avg. Num. of Employees: 75

Directional Distribution: 22% entering, 78% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.49 | 0.04 - 2.33 | 0.22 |





Vehicle Trip Ends vs: Employees On a: Weekday, **AM Peak Hour of Generator**

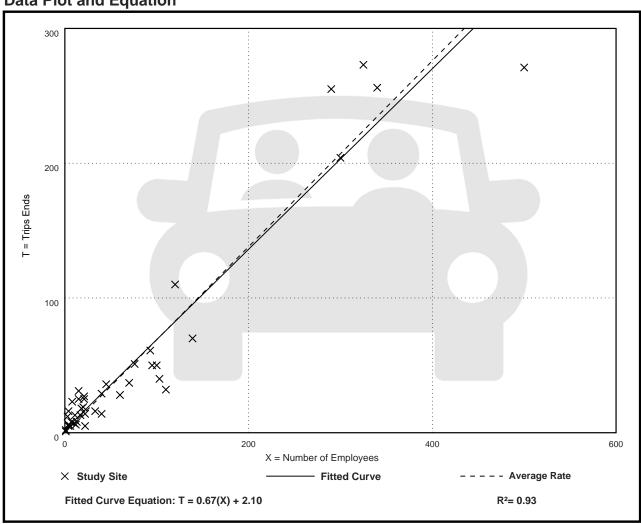
Setting/Location: General Urban/Suburban

Number of Studies: 41 Avg. Num. of Employees: 76

Directional Distribution: 85% entering, 15% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.69 | 0.23 - 4.00 | 0.30 |





Vehicle Trip Ends vs: Employees On a: Weekday, **PM Peak Hour of Generator**

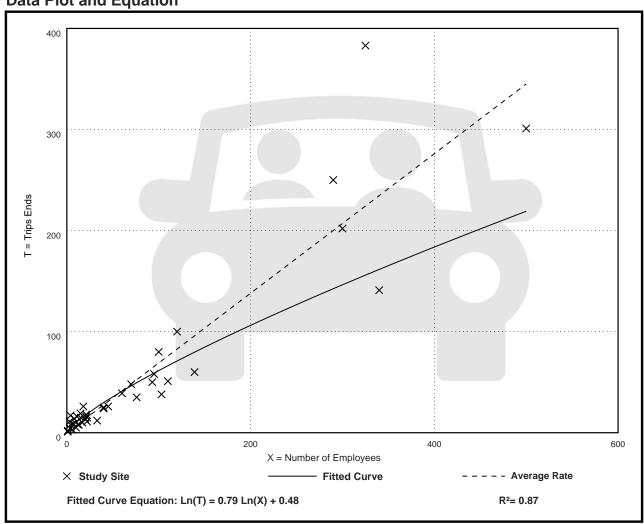
Setting/Location: General Urban/Suburban

Number of Studies: 41 Avg. Num. of Employees: 76

Directional Distribution: 31% entering, 69% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.69 | 0.36 - 4.25 | 0.30 |





Vehicle Trip Ends vs: Employees On a: Saturday

Setting/Location: General Urban/Suburban

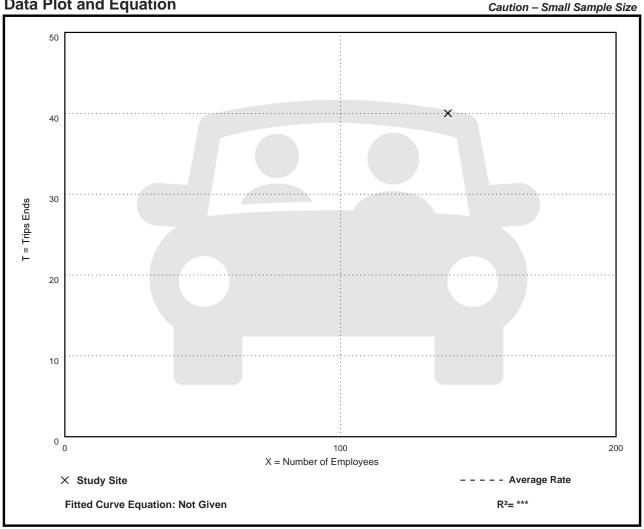
Number of Studies: 1 Avg. Num. of Employees: 139

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.29 | 0.29 - 0.29 | *** |







Vehicle Trip Ends vs: Employees On a: Sunday

Setting/Location: General Urban/Suburban

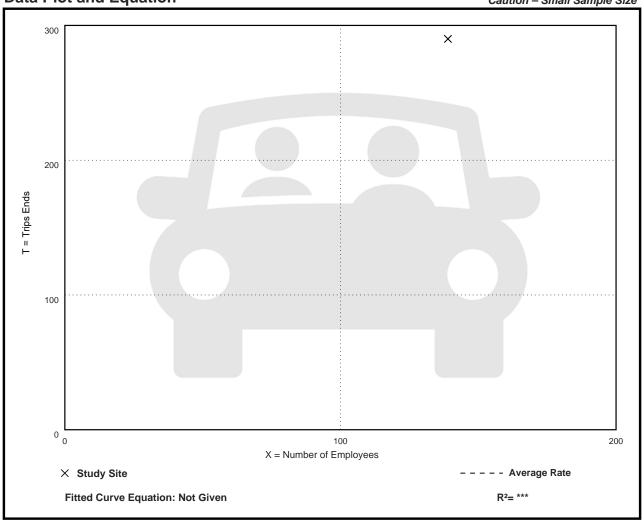
Number of Studies: 1 Avg. Num. of Employees: 139

Directional Distribution: 50% entering, 50% exiting

Vehicle Trip Generation per Employee

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 2.09 | 2.09 - 2.09 | *** |







Vehicle Trip Ends vs: Employees

On a: Sunday, Peak Hour of Generator

Setting/Location: General Urban/Suburban

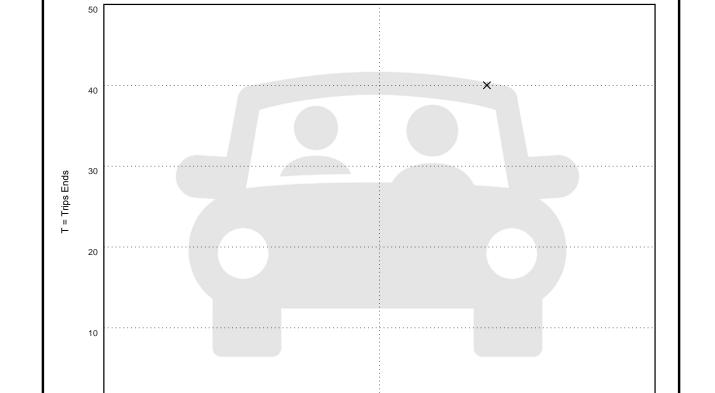
Number of Studies: 1 Avg. Num. of Employees: 139

Directional Distribution: 48% entering, 52% exiting

Vehicle Trip Generation per Employee

Data Plot and Equation

| Average Rate | Range of Rates | Standard Deviation |
|--------------|----------------|--------------------|
| 0.29 | 0.29 - 0.29 | *** |



X = Number of Employees



200

– - Average Rate

R2= ***

Caution - Small Sample Size

46

× Study Site

Fitted Curve Equation: Not Given

| Hourly Distribu | tion of Entering an | d Exiting Vehicle Tri | ns by Land Use | | | | | | | | |
|------------------|---------------------|--------------------------|----------------|--|--|--|--|--|--|--|--|
| · | | ion Manual , 11th Edit | • | | | | | | | | |
| | | , | | | | | | | | | |
| Land Use Code | | 110 | | | | | | | | | |
| Land Use | | General Light Industrial | | | | | | | | | |
| Setting | | General Urban/Suburba | | | | | | | | | |
| Time Period | | Weekday | | | | | | | | | |
| # Data Sites | | 27 | | | | | | | | | |
| | % | of 24-Hour Vehicle Tr | ips | | | | | | | | |
| Time | Total | Entering | Exiting | | | | | | | | |
| 12:00 - 1:00 AM | 0.0% | 0.0% | 0.0% | | | | | | | | |
| 1:00 - 2:00 AM | 0.0% | 0.0% | 0.1% | | | | | | | | |
| 2:00 - 3:00 AM | 0.0% | 0.0% | 0.1% | | | | | | | | |
| 3:00 - 4:00 AM | 0.0% | 0.1% | 0.0% | | | | | | | | |
| 4:00 - 5:00 AM | 0.3% | 0.6% | 0.0% | | | | | | | | |
| 5:00 - 6:00 AM | 2.9% | 5.4% | 0.4% | | | | | | | | |
| 6:00 - 7:00 AM | 3.9% | 7.2% | 0.7% | | | | | | | | |
| 7:00 - 8:00 AM | 10.1% | 18.0% | 2.3% | | | | | | | | |
| 8:00 - 9:00 AM | 7.7% | 10.8% | 4.6% | | | | | | | | |
| 9:00 - 10:00 AM | 7.3% | 7.3% | 7.3% | | | | | | | | |
| 10:00 - 11:00 AM | 7.7% | 7.7% | 7.8% | | | | | | | | |
| 11:00 - 12:00 PM | 7.5% | 6.5% | 8.5% | | | | | | | | |
| 12:00 - 1:00 PM | 9.9% | 9.0% | 10.8% | | | | | | | | |
| 1:00 - 2:00 PM | 7.9% | 8.5% | 7.3% | | | | | | | | |
| 2:00 - 3:00 PM | 8.1% | 7.3% | 8.9% | | | | | | | | |
| 3:00 - 4:00 PM | 8.7% | 6.0% | 11.3% | | | | | | | | |
| 4:00 - 5:00 PM | 7.5% | 4.1% | 10.8% | | | | | | | | |
| 5:00 - 6:00 PM | 9.0% | 1.2% | 16.7% | | | | | | | | |
| 6:00 - 7:00 PM | 1.2% | 0.1% | 2.4% | | | | | | | | |
| 7:00 - 8:00 PM | 0.0% | 0.0% | 0.1% | | | | | | | | |
| 8:00 - 9:00 PM | 0.0% | 0.0% | 0.0% | | | | | | | | |
| 9:00 - 10:00 PM | 0.0% | 0.0% | 0.0% | | | | | | | | |
| 10:00 - 11:00 PM | 0.0% | 0.0% | 0.0% | | | | | | | | |
| 11:00 - 12:00 AM | 0.0% | 0.0% | 0.0% | | | | | | | | |

F – CA MUTCD Traffic Signal Warrants

| Warrant | Title | | | Standard |
|---------|---------------------------|--------|--------|---|
| 1 | Eight-Hour Volume | | | The need for a traffic control signal shall be considered if an engineering study finds that 1 of the following conditions exist for each of any 8 hours of an average day. In applying each condition the major-street and minor-street volumes shall be for the same 8 hours. On the minor street, the higher volume shall not be required to be on the same approach during each of these 8 hours. |
| - | Condition A | Part 1 | Part 2 | A. The vehicles per hour given in both of the 100%/80% columns of Condition A in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection, or |
| - | Condition B | Part 1 | Part 2 | A. The vehicles per hour given in both of the 100%/80% columns of Condition B in Table 4C-1 exist on the major-street and the higher-volume minor-street approaches, respectively, to the intersection. |
| 2 | Four-Hour Volume | | | See Figure 4C-1 or 4C-2 in MUTCD. |
| 3 | Peak Hour Volume | | | This signal warrant shall be applied only in unusual cases, such as office complexes, manufacturing plants, industrial complexes, or high-occupancy vehicle facilities that attract or discharge large numbers of vehicles over a short time. The need for a traffic control signal shall be considered if an engineering study finds that the criteria in either of the following 2 categories are met: A. If all 3 of the following conditions exist for the same 1 hour of an average day: 1. The total stopped time delay experience by the traffic on 1 minor-street approach (1 direction only) controlled by a STOP sign equals or exceeds: 4 vehicle-hours for a 1-lane approach; or 5 vehicle-hours for a 2-lane approach, and 2. The volume on the same minor-street approach (1 direction only) equals or exceeds 100 vph for 1 moving lane of traffic or 150 vph for 2 moving lanes, and 3. The total entering volume serviced during the hour equals or exceeds 650 vph for intersections with 3 approaches or 800 vph for intersections with 4 or more approaches. B. See Figure 4C-3 or 4C-4 in MUTCD. |
| 4 | Pedestrian Volume | | | See Page 4C-5 in MUTCD |
| 5 | School Crossing | | | See Page 4C-5 in MUTCD |
| 6 | Coordinated Signal System | | | See Page 4C-6 in MUTCD |
| 7 | Crash Experience | | | The need for a traffic control signal shall be considered if an engineering study finds that all of the following criteria are met: A. Adequate trial of alternatives with satisfactory observance and enforcement has falled to reduce the crash frequency; and B. 5 or more reported crashes, of types susceptible to correction by a traffic control signal, have occurred within a 12-month period, each crash involving personal injury or property damage apparently exceeding the applicable requirements for a reportable crash; and C. For each of any 8 hours of an average day, the vph given in both the 80% columns of Condition A in Table 4C-1, or the vph in both of the 80% columns of Condition B in Table 4C-1 exists on the major-street and the higher-volume minor-street approach, respectively, to the intersection, or the volume of pedestrian traffic is not less than 80% of the requirements specified in the Pedestrian Volume warrant. These major-street and minor-street volumes shall be for the same 8 hours. On the minor street, the higher volume shall not be required to be on the same approach during each of the 8 hours. |
| 8 | Roadway Network | | | See page 4C-7 in MUTCD |

| | | | 111110 | 1 272 | | 1 272 | | 2 744 | | ſ | Hourly Dietributi | ion of En | toring and | Eviting | | | | | |
|------------|----------|----------|---------|----------------|--------------|---------------|---------|--------------|-------|----------|--|-------------|--------------|-------------|--|--|--|--|--|
| | | | LU 110 | 1,372 ering | Evit | 1,372 ting | To | 2,744 tal | | | Hourly Distribution of Entering and Exiting Vehicle Trips by Land Use | | | | | | | | |
| | | | % Daily | Trips | % Daily | Trip | % Daily | Trip | | | Source: ITE Trip Generation Manual, 11th Edition | | | | | | | | |
| 6:00 | to | 7:00 | 7.20% | 99 | 0.70% | 10 | 3.90% | 107 | | | Jource. TIE Trip Ger | ieration iv | nunuur, 110 | .ii Edition | | | | | |
| 7:00 | to | 8:00 | 18.00% | 247 | 2.30% | 32 | 10.10% | 277 | | | Land Use Code | | 110 | | | | | | |
| 8:00 | to | 9:00 | 10.80% | 148 | 4.60% | 63 | 7.70% | 211 | | | Land Use | Gener | al Light Ind | lustrial | | | | | |
| 9:00 | to | 10:00 | 7.30% | 100 | 7.30% | 100 | 7.70% | 200 | | | Setting | | al Urban/Su | | | | | | |
| 10:00 | to | 11:00 | 7.70% | 106 | 7.80% | 107 | 7.70% | 211 | | | Time Period | Genera | Weekday | barbari | | | | | |
| 11:00 | to | 12:00 | 6.50% | 89 | 8.50% | 117 | 7.50% | 206 | | | # Data Sites | | 27 | | | | | | |
| 12:00 | to | 13:00 | 9.00% | 123 | 10.80% | 148 | 9.90% | 272 | | | # Data Sites | % of 24 | -Hour Vehi | cle Trips | | | | | |
| 13:00 | to | 14:00 | 8.50% | 117 | 7.30% | 100 | 7.90% | 217 | | | Time | Total | Entering | Exiting | | | | | |
| 14:00 | to | 15:00 | 7.30% | 100 | 8.90% | 122 | 8.10% | 222 | | | 12:00 - 1:00 AM | 0.00% | 0.00% | 0.00% | | | | | |
| 15:00 | to | 16:00 | 6.00% | 82 | 11.30% | 155 | 8.70% | 239 | | | 1:00 - 2:00 AM | 0.00% | 0.00% | 0.10% | | | | | |
| 16:00 | to | 17:00 | 4.10% | 56 | 10.80% | 148 | 7.50% | 206 | | | 2:00 - 3:00 AM | 0.00% | 0.00% | 0.10% | | | | | |
| 17:00 | to | 18:00 | 1.20% | 16 | 16.70% | 229 | 9.00% | 247 | | | 3:00 - 4:00 AM | 0.00% | 0.10% | 0.00% | | | | | |
| | | | | | | | | | | | 4:00 - 5:00 AM | 0.30% | 0.60% | 0.00% | | | | | |
| #3 Plaza 8 | & Privat | e Access | Road | | | | | | | F | 5:00 - 6:00 AM | 2.90% | 5.40% | 0.40% | | | | | |
| | | | | | | | | | | F | 6:00 - 7:00 AM | 3.90% | 7.20% | 0.70% | | | | | |
| | | | | Existing | Intersection | n Counts | | | | F | 7:00 - 8:00 AM | 10.10% | 18.00% | 2.30% | | | | | |
| | | | | | | | Major | Minor | | - | | | | | | | | | |
| | | | NB | SB | EB | WB | Total | Total | Total | | 8:00 - 9:00 AM | 7.70% | 10.80% | 4.60% | | | | | |
| 6:00 | to | 7:00 | 535 | 398 | 0 | 1 | 933 | 1 | 934 | - | 9:00 - 10:00 AM | 7.70% | 7.30% | 7.30% | | | | | |
| 7:00 | to | 8:00 | 581 | 587 | 0 | 1 | 1168 | 1 | 1169 | F | 10:00 - 11:00 AM | 7.70% | 7.70% | 7.80% | | | | | |
| 8:00 | to | 9:00 | 494 | 508 | 0 | 1 | 1002 | 1 | 1003 | F | 11:00 - 12:00 PM | 7.50% | 6.50% | 8.50% | | | | | |
| 9:00 | to | 10:00 | 370 | 543 | 0 | 5 | 913 | 5 | 918 | F | 12:00 - 1:00 PM | 9.90% | 9.00% | 10.80% | | | | | |
| 10:00 | to | 11:00 | 423 | 444 | 0 | 2 | 867 | 2 | 869 | F | 1:00 - 2:00 PM | 7.90% | 8.50% | 7.30% | | | | | |
| 11:00 | to | 12:00 | 423 | 538 | 0 | 14 | 961 | 14 | 975 | F | 2:00 - 3:00 PM | 8.10% | 7.30% | 8.90% | | | | | |
| 12:00 | to | 13:00 | 461 | 397 | 0 | 4 | 858 | 4 | 862 | - | 3:00 - 4:00 PM | 8.70% | 6.00% | 11.30% | | | | | |
| 13:00 | to | 14:00 | 533 | 619 | 0 | 7 | 1152 | 7 | 1159 | - | 4:00 - 5:00 PM | 7.50% | 4.10% | 10.80% | | | | | |
| 14:00 | to | 15:00 | 484 | 581 | 0 | 3 | 1065 | 3 | 1068 | - | 5:00 - 6:00 PM | 9.00% | 1.20% | 16.70% | | | | | |
| 15:00 | to | 16:00 | 484 | 639 | 0 | 3 | 1123 | 3 | 1126 | - | 6:00 - 7:00 PM | 1.20% | 0.10% | 2.40% | | | | | |
| 16:00 | to | 17:00 | 664 | 592 | 0 | 12 | 1256 | 12 | 1268 | F | 7:00 - 8:00 PM | 0.00% | 0.00% | 0.10% | | | | | |
| 17:00 | to | 18:00 | 568 | 593 | 0 | 12 | 1161 | 12 | 1173 | F | 8:00 - 9:00 PM | 0.00% | 0.00% | 0.00% | | | | | |
| | | | | | | | | | | F | 9:00 - 10:00 PM | 0.00% | 0.00% | 0.00% | | | | | |
| | | | | | | | | | | F | 10:00 - 11:00 PM | 0.00% | 0.00% | 0.00% | | | | | |
| | | | | Projec | t Trip Assig | nment | | | | - | 11:00 - 12:00 AM | 0.00% | 0.00% | 0.00% | | | | | |
| | | | | - | | | Major | Minor | | <u> </u> | | | | | | | | | |
| | | | NB | SB | EB | WB | Total | Total | Total | | | | | | | | | | |
| | | | 60% | 40% | 100% | 0% | | | | | | | | | | | | | |
| 6:00 | to | 7:00 | 59 | 40 | 10 | 0 | 99 | 10 | 109 | | | | | | | | | | |
| 7:00 | to | 8:00 | 148 | 99 | 32 | 0 | 247 | 32 | 279 | | | | | | | | | | |
| 8:00 | to | 9:00 | 89 | 59 | 63 | 0 | 148 | 63 | 211 | | | | | | | | | | |
| 9:00 | to | 10:00 | 60 | 40 | 100 | 0 | 100 | 100 | 200 | | | | | | | | | | |
| 10:00 | to | 11:00 | 64 | 42 | 107 | 0 | 106 | 107 | 213 | | | | | | | | | | |
| 11:00 | to | 12:00 | 53 | 36 | 117 | 0 | 89 | 117 | 206 | | | | | | | | | | |
| 12:00 | to | 13:00 | 74 | 49 | 148 | 0 | 123 | 148 | 271 | | | | | | | | | | |
| 13:00 | to | 14:00 | 70 | 47 | 100 | 0 | 117 | 100 | 217 | | | | | | | | | | |
| 14:00 | to | 15:00 | 60 | 40 | 122 | 0 | 100 | 122 | 222 | | | | | | | | | | |
| 15:00 | to | 16:00 | 49 | 33 | 155 | 0 | 82 | 155 | 237 | | | | | | | | | | |
| 16:00 | to | 17:00 | 34 | 22 | 148 | 0 | 56 | 148 | 204 | | | | | | | | | | |
| 17:00 | to | 18:00 | 10 | 6 | 229 | 0 | 16 | 229 | 245 | | | | | | | | | | |
| | | | - | | | | | | | | | | | | | | | | |

Growth =

Minor

Total

Major

Total

0.03

Total

Total Intersection Volumes

ЕВ

WB

NB

6:00

7:00

8:00

9:00

10:00

11:00

12:00

13:00

14:00

15:00

16:00

17:00

to

7:00

8:00

9:00

10:00

11:00

12:00

13:00

14:00

15:00

16:00

17:00

18:00

SB

TRAFFIC SIGNAL VOLUME WARRANT ANALYSIS (2014 MUTCD, REV. 6)

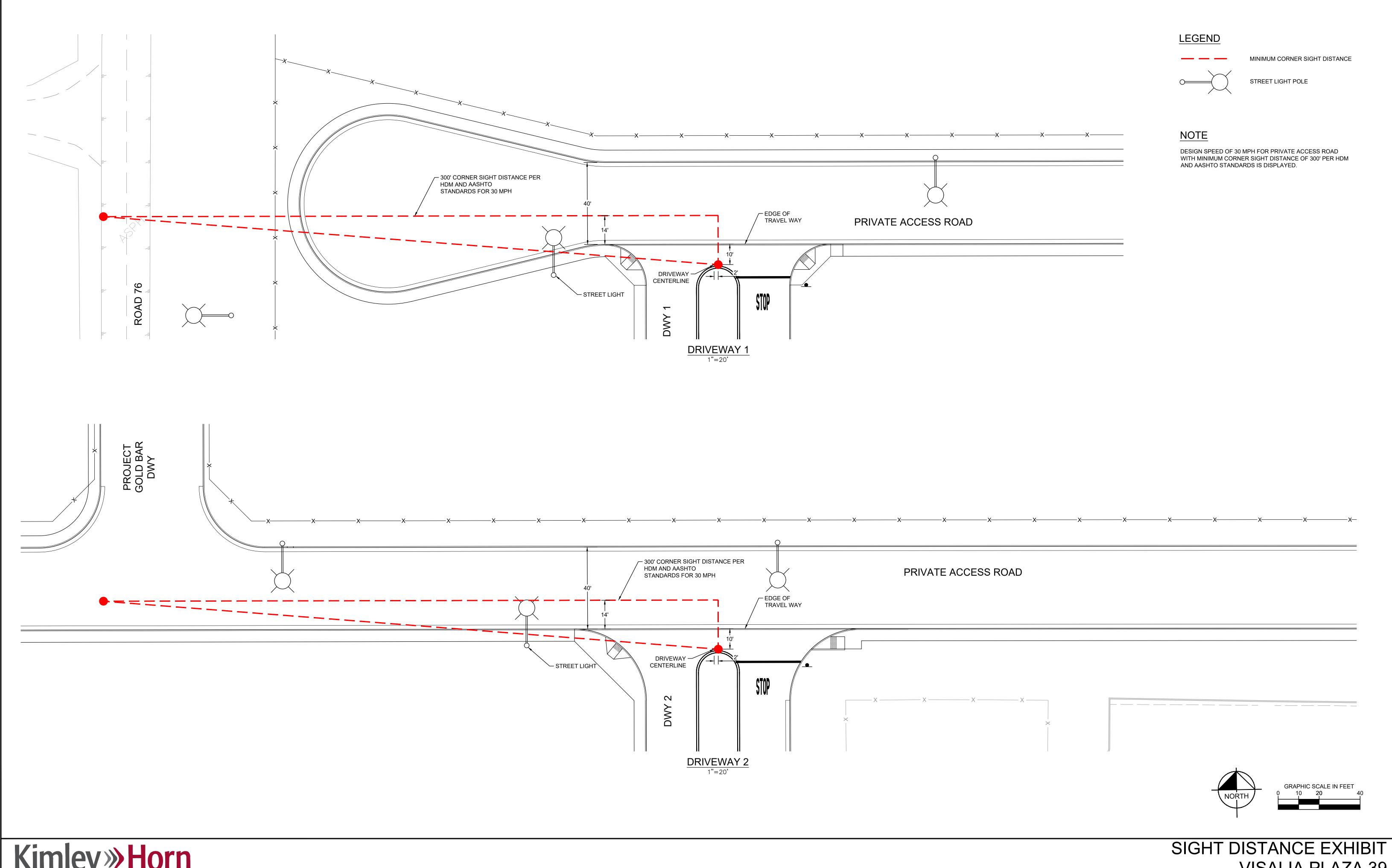
| MAJOR STREET: | N Plaza Drive | NB | SB | # OF APPROACH LANES: | 2 |
|-----------------|--------------------------------------|---------------|----|----------------------|---|
| MINOR STREET: | Private Access Road | ЕВ | WB | # OF APPROACH LANES: | 1 |
| CITY, STATE: | Visalia, California | | | | |
| COMMENTS: | Opening Year Plus Project Traffic C | onditions | | | |
| ICOLATED COMMUN | UTV MUTIL DODLII ATION I ECC THAN 40 | 000 (V OD N): | | | |

ISOLATED COMMUNITY WITH POPULATION LESS THAN 10,000 (Y OR N): 85TH PERCENTILE SPEED GREATER THAN 40 MPH ON MAJOR STREET (Y OR N):

| N |
|---|
| Y |

| | | | MAJOR ST | MINOR ST | Ped Count | WARRAN [*] | Γ1 - Conditi | on A, Part 1 | WARRAN | T 1 - Condition | on B, Part 1 | WARRAN [*] | T 1 - Conditi | on A, Part 2 | WARRAN [*] | Γ1 - Conditi | on B, Part 2 | WARRANT 2 | WARRANT 3 | WAR | RANT 4 |
|-----------|--------|----------|--------------------|----------------------|----------------------|---------------------|----------------|--------------|-----------|-----------------|--------------|---|----------------|--------------|---------------------|----------------|--------------|------------------|--------------|---------------------------|---------------------------|
| | | | TWO-WAY TRAFFIC | TRAFFIC HEAVY LEG | CROSSING MAJOR ST | MAIN LINE | SIDE STREET | ВОТН МЕТ | MAIN LINE | SIDE STREET | ВОТН МЕТ | MAIN LINE | SIDE STREET | вотн мет | MAIN LINE | SIDE STREET | ВОТН МЕТ | Four-Hour | Peak Hour | Ped Volume (Four-hour) | Ped Volume (Peak-hour) |
| THRESHOLD | VALUES | 3 | | — | | 420 | 105 | | 630 | 53 | | 336 | 84 | | 504 | 42 | | 60 | 75 | 100 | 190 |
| 06:00 AM | TO | 07:00 AM | 1,060 | 11 | | Y | | | Υ | | | Y | | | Y | | | | | | |
| 07:00 AM | TO | MA 00:80 | 1,450 | 33 | | Y | | | Υ | | | Υ | | | Y | | | | | | |
| 08:00 AM | TO | 09:00 AM | 1,180 | 64 | | Υ | | | Υ | Υ | Y | Υ | | | Y | Υ | Y | Y | | | |
| 09:00 AM | TO | 10:00 AM | 1,040 | 105 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 10:00 AM | TO | 11:00 AM | 999 | 109 | | Υ | Υ | Y | Υ | Υ | Y | Υ | Y | Υ | Y | Υ | Y | Y | | | |
| 11:00 AM | TO | 12:00 PM | 1,079 | 131 | | Υ | Υ | Y | Υ | Υ | Y | Υ | Y | Υ | Y | Υ | Y | Y | Υ | | |
| 12:00 PM | TO | 01:00 PM | 1,007 | 152 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 01:00 PM | TO | 02:00 PM | 1,304 | 107 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 02:00 PM | TO | 03:00 PM | 1,197 | 125 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 03:00 PM | TO | 04:00 PM | 1,239 | 158 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 04:00 PM | TO | 05:00 PM | 1,350 | 160 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 05:00 PM | TO | 06:00 PM | 1,212 | 241 | | Y | Y | Y | Υ | Y | Y | Υ | Y | Y | Y | Y | Y | Υ | Y | | |
| 06:00 PM | TO | 07:00 PM | | | | | | | | | | | | | | | | | | | |
| 07:00 PM | TO | 08:00 PM | | | | | | | | | | | | | | | | | | | |
| 08:00 PM | TO | 09:00 PM | | | | | | | | | | | | | | | | | | | |
| 09:00 PM | TO | 10:00 PM | | | | | | | | | | | | | | | | | | | |
| | | | 14,117 | 1,396 | | 12 | 9 | 9 | 12 | 10 | 10 | 12 | 9 | 9 | 12 | 10 | 10 | 10 | 8 | 0 | 0 |
| | | | | | | 8 H | OURS NEE | DED | 8 H | OURS NEE | DED | 8 HOURS NEEDED for both Condition A & B | | | | 4 HRS NEEDED | 1 HR NEEDED | 4 HRS NEEDED | 1 HR NEEDE | | |
| | | | | | | | SATISFIED |) | | SATISFIED |) | SATISFIED | | | | SATISFIED | SATISFIED | NOT SATISFIED | NOT SATISFII | | |

05/19/22 Kimley-Horn and Associates G – Sight Distance Assessment



401 B STREET, SUITE 600, SAN DIEGO, CA 92101 PHONE: 619—234—9411 WWW.KIMLEY—HORN.COM

k:\snd_ldev\195170022 - visalia-plaza 35\design\exhibits\2022.05.19 - sight distance exhibit\2022.05.19 - sight distance exhibit.dwg 5/19/2022

- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -- Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting am & Eve Vilalia Project/Business Name: 05/13/2022 Project Description: GENERAL PROJECT INFORMATION Site Plan Review Resubmittal: If Resubmittal, Previous Site Plan Review Number: Property Owner: Capital. Applicant(s) Name: Management Croup LB Inc dba Adam & Eve Project Address/Location: Mooney Blud, Visalia CA 93277 Assessor Parcel Number: Parcel Size (Acreage or Square Feet): Building or Suite Square Footage: Are There Any Proposed Building Modifications: - THIS AREA FOR CITY STAFF USE ONLY ---05/13/2022 Estimated Cost of Modifications to Building: Date Received: 05/25/2022 Describe All Proposed Building Modifications: SPR Agenda: Item No. 22-053 SPR No. **Historic District:** Yes (Flood Zone: AE (X/AE (- - A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS - -Existing/Prior Building Use: Retail Proposed Building Use: Retail 1 Proposed Hours of Operation: 11:00 AM- 10:00 PM OPERATIONS & TRAFFIC INFORMATION Days of Week In Operation (Circle): Su M T W Th F Sa Number of Employees Per Day: Existing 1-2 Proposed Number of Customers Per Day (Estimated): Existing 10 Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: none Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees (Provide Separate Attachment if Necessary): Describe Any Special Events Planned for the Facility: none Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS | | |
|---------------------------|--|--|--|
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies | | |
| S | | | |
| JENT | not accepted). | | |
| REN | ⇒ Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. | | |
| SITE PLAN REQUIREMENTS | ⇒ Site plan shall provide for and indicate all of the following: North arrow Existing & proposed structures All existing & proposed site features Site dimensions, including building Existing and proposed fencing at site Public improvements (curbs, sidewalks, utility poles, hydrants, street lights, etc.) Existing & proposed structures Accessible path of travel from ADA stall Location and width of drive approaches to site Tentative maps shall adhere to requirements of Visalia Municipal Code Section 16 | | |
| | Applicant Information (Final comments will be mailed to the name and address provided below) | | |
| REQUIRED SIGNATURE | Name: LM Capital ILC Signature of Owner or Authorized Agent* Address: 9441 Charleville Blvd, #500 City, State, Zip Bewerly Hills CA 90212 Phone: (310) 405-9778 Email: Michael@fmgae.com Authorized Agent* Date * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. | | |
| l.s. | AGENCY AUTHORIZATION | | |
| | OWNER: I,, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): | | |
| IRM | AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to | | |
| ON F | relative to the property mentioned herein. | | |
| ZATI | I declare under penalty of perjury the foregoing is true and correct. | | |
| AGENCY AUTHORIZATION FORM | Executed this day of, 20 | | |
| ICY A | OWNER Signatures AGENT | | |
| AGEN | | | |
| | Signature of Agent Signature of Agent | | |
| | 9401 Charleville Blvd, #500 Owner Mailing Address Agent Mailing Address | | |
| | Owner Mailing Address Beverly Hills CA 90212 | | |
| | Owper Phone Number Agent Phone Number Agent Phone Number | | |
| 75 | | | |

Page 2 of 2

Proposed Location: 1312 S Mooney Blvd, Visalia CA 93277

Proposed Square Footage: 1,550 Square Feet

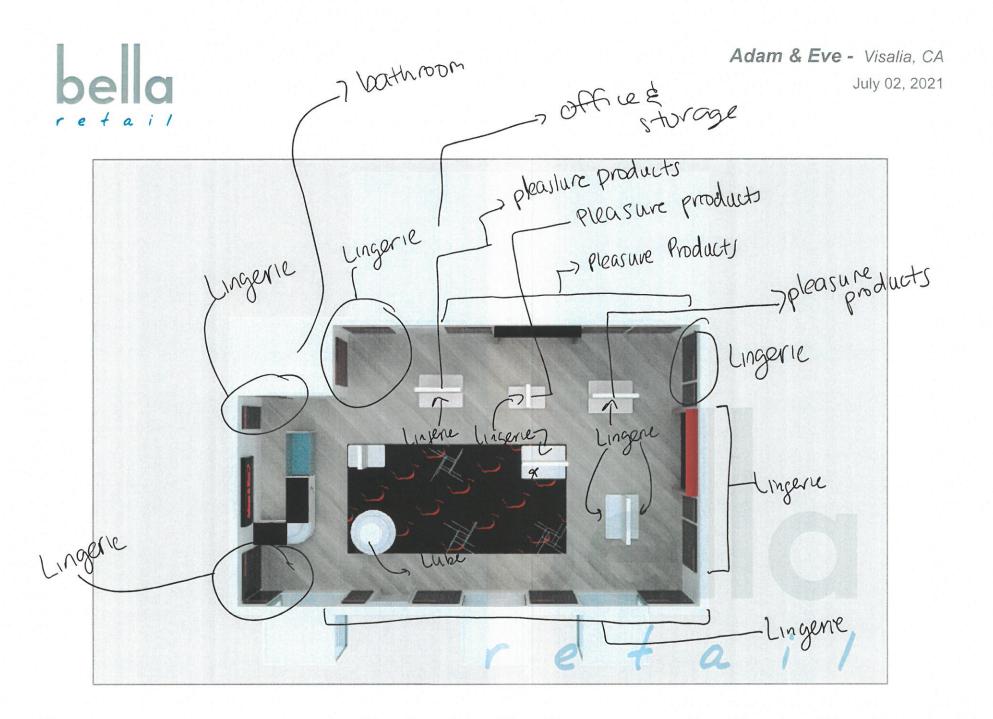
Store Description: We are opening an up-scale retail boutique. Our retail store provides an area for women and couples to come and shop in person versus online. We provide a wide variety of items for all people such as, apparel, lingerie, hosiery, shoes, games, apparel, pleasure products, massage oils, and lotions. We provide customers a comfortable, safe, and friendly retail shopping experience.

Products by Category & Percentage of Display:

- Women's Apparel 5%
- Lingerie (regular & plus size) 55%
- Hosiery, Shoes, and Boots 2.5%
- Men's Apparel 2.5%
- Lotions (edible & non-edible) 2.5%
- Oils (edible & non-edible) 10%
- Candles (edible & non-edible) − 2.5%
- Pleasure Products (Adult Toys) 20%

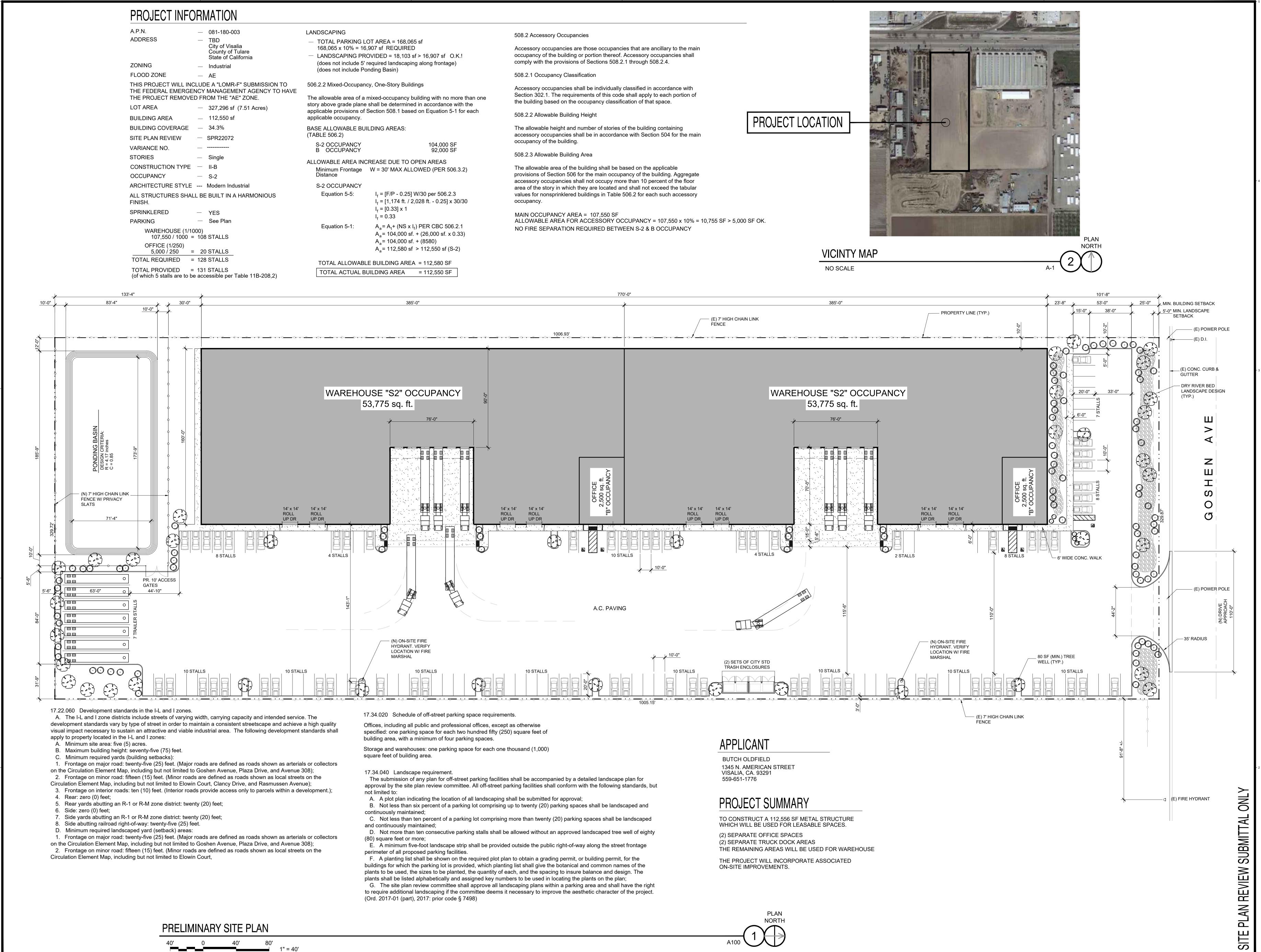
Products by Category & Percentage of Sales:

- Women's Apparel 10%
- Lingerie (regular & plus size) 35%
- Hosiery, Shoes, and Boots 5%
- Men's Apparel 5%
- Lotions (edible & non-edible) 10%
- Oils (edible & non-edible) 15%
- Candles (edible & non-edible) 5%
- Pleasure Products (Adult Toys) 15%



| | CITY OF VISALIA SITE PLAN REVIEW APPLICATION |
|-----------------------------|---|
| | - Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440- |
| | This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda. |
| | - Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present - |
| | - Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting - |
| | Project/Business Name: GA INDUSTRING COMPLEX Date: 5/19/27 Project Description: NEW 112, 550 54 A. BUILDING AND LOADING DOCKS. |
| NOL | Project Description: NEW 112, 550 54 H. BUILDING AND LOADING DOCKS. |
| RMA | Site Plan Review Resubmittal: Yes No If Resubmittal, Previous Site Plan Review Number: 5712 72 |
| GENERAL PROJECT INFORMATION | Property Owner: AMERICAN INC |
| | Applicant(s) Name: COLWYN "BUTCH" OLDFIELD |
| L B | Project Address/Location: GOSHEN AVE GOOFT WEST OF CLANCY ST |
| NE. | Assessor Parcel Number: 001-180-003 |
| 8 | Parcel Size (Acreage or Square Feet): 327, 29 6 59. ft. Building or Suite Square Footage: |
| | Are There Any Proposed Building Modifications: Yes No THIS AREA FOR CITY STAFF USE ONLY |
| | Estimated Cost of Modifications to Building: \$ 8 MILLION Date Received: |
| | Describe All Proposed Building Modifications: NEい METAL BUILDING SPR Agenda: Item No |
| | W LOADING DOCKS Zone: SPR No. |
| | Historic District: Yes No |
| | Flood Zone: X AE X/AE |
| | A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS |
| | Existing/Prior Building Use: N/A |
| | Proposed Building Use: WA 化さけついん |
| | Proposed Hours of Operation: 6Am - 6PM |
| FIC INFORMATION | Days of Week In Operation (Circle): Su M to M to Sa |
| NR. | Number of Employees Per Day: Existing \(\bar{\bar{\bar{\bar{\Bar{\Bar{\Bar{\Bar{\Bar{\Bar{\Bar{\B |
| N. | Number of Customers Per Day (Estimated): Existing Proposed Proposed |
| | Predicted Peak Operating Hour: N/A |
| OPERATIONS & TRA | Describe Any Truck Delivery Schedule & Operations: |
| RATIO | Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees |
| OPE | (Provide Separate Attachment if Necessary): |
| | |
| | Describe Any Special Events Planned for the Facility: |
| | |
| | Page 1 of 2 - Application continues on back of this page |

| | SITE PLAN MINIMUM REQUIREMENTS |
|-------------------|---|
| Jon. | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies |
| 2 | not accepted). |
| LAIN NEGOINEMENTS | Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. |
| 3 | Site plan shall provide for and indicate all of the following: |
| | - North arrow - Existing & proposed structures - Loading/unloading areas |
| | - All existing & proposed site features - Adjacent street names - Accessible path of travel from right of way |
| | Site dimensions, including building Refuse enclosures & containers Accessible path of travel from ADA stall |
| , | - Existing and proposed fencing at site - Valley oak trees (show drip line) - Location and width of drive approaches to site |
| | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| 1000 | Applicant Information (Final comments will be mailed to the name and address provided below) |
| | Name: Conwyn OLDFIELT Signature of Owner or Authorized Agent* |
| | Address: 1345 M. Amarian St. |
| | |
| | City, State, Zip V-SALVII CA 132-1 |
| ı | Phone: 559-730-6910 |
| 1 | Email: BOLP FIELD @ A MINIL. COM Authorized Agent* Date |
| - | * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | individual by an additionable agent, the Agenty Additionable information below into the completed for this application to be considered acceptable. |
| | I,, declare as follows; I am the owner of certain real property bearing assessor's |
| | parcel number (APN): |
| | AGENT: |
| | AGENT: I designate |
| | AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to |
| | AGENT: I designate |
| | AGENT: I designate |
| | AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to |
| | AGENT: I designate |
| | AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to relative to the property mentioned herein. I declare under penalty of perjury the foregoing is true and correct. |
| | AGENT: I designate |





□

PROJECT NO: XX OF 40 SHEET NO. A100

- Additional information and help in filling out this application can be found at the City of Visalia website (www.ci.visalia.ca.us) or by calling (559) 713-4440-

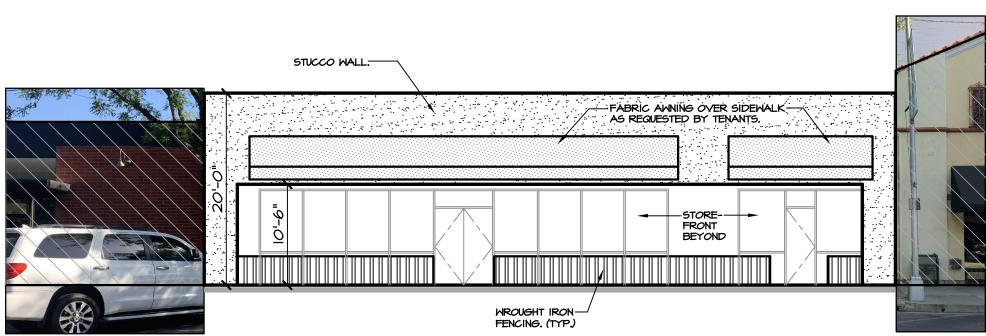


This application MUST be filled out in its entirety and submitted with an acceptable site plan (see details below). Failure to provide all requested information may result in your application being rejected for additional information and excluded from the Site Plan Review agenda

- All plans to be considered on the next available agenda must be submitted by 4:00 p.m. on the Thursday prior to the meeting -- Site plan review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant or representative must be present -Alejandra's and Jimmy John's Date: 5-18-22 Project/Business Name: Rebuild of existing restaurants and retail building. Project Description: Yes O No 💢 Site Plan Review Resubmittal: If Resubmittal, Previous Site Plan Review Number: Property Owner: 312-316 West Main St., LLC Applicant(s) Name: Dave Francy Project Address/Location: 312, 314 and 316 W Main St, Visalia, CA 93291 094 322 004 Assessor Parcel Number: Parcel Size (Acreage or Square Feet): 8,406 sf Building or Suite Square Footage: 8,406 sf Yes X No (--- THIS AREA FOR CITY STAFF USE ONLY ---Are There Any Proposed Building Modifications: Date Received: 05/18/2022 \$ tbd Estimated Cost of Modifications to Building: SPR Agenda: 05/25/2022 Item No. Describe All Proposed Building Modifications: Zone: D-MU SPR No. 22-085 Rebuild of existing restaurants and retail building. Yes No X Historic District: AE(X) X/AE() Flood Zone: -- A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS --Restaurants and Retail Existing/Prior Building Use: Restaurants and Retail Proposed Building Use: Proposed Hours of Operation: 10:00 am - 10:00 pm Days of Week In Operation (Circle): Su M T W Th F Sa 10 Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existina Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees (Provide Separate Attachment if Necessary): Describe Any Special Events Planned for the Facility: Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS |
|------------------------|--|
| | Plan(s) must be clear, legible, and on a sheet size appropriate to easily convey all necessary project information. Suggested minimum |
| SITE PLAN REQUIREMENTS | sheet size for site plans is 11"x17" (Excludes tentative parcel and final maps) |
| ME | ⇒ Site plan shall provide for and indicate all of the following: |
| UIR | - North arrow - Existing & proposed structures - Loading/unloading areas |
| EQ | - All existing & proposed site features - Adjacent street names - Accessible path of travel from right of way |
| N | - Site dimensions, including building - Refuse enclosures & containers - Accessible path of travel from ADA stall |
| PL | - Existing and proposed fencing at site - Valley oak trees (show drip line) - Location and width of drive approaches to site |
| SITE | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| | Submit 20 copies of the site plan with this application, folded to a legal size of 9" x 12" with the print on the outside (no rolled plans) |
| | Applicant Information (Final comments will be mailed to the name and address provided below) |
| Æ | Circulations of Communication of Assets and Assets |
| T D | |
| GN | Address: 121 N. Eucha St. Owner Date Date |
| D SI | City, State, Zip 115AIN C1293291 |
| 188 | Phone: 559 3044100 |
| REQUIRED SIGNATURE | Email: Francys @ Lyno, con Authorized Agent* Date |
| | * If signed by an authorized agent , the "Agency Authorization" information below must be completed for this application to be considered complete |
| - | |
| | AGENCY AUTHORIZATION |
| | OW: ER: |
| | declare as followed lamitha approximated managing accessed |
| | declare as follows; I am the owner of certain real property bearing assessor parcel number (A, N): |
| | parcer number (AACV). |
| | |
| ē. | AGENT: |
| | I designate |
| | an application for, and obtain a permit to |
| FORM | relative to the property mentioned herein. |
| S | |
| | I declare under penalty of perjury the foregoing is true and correct. |
| AGENCY AUTHORIZATION | Executed this day of |
| 일 | |
| A | OWNER AGENT |
| ١٢ | <u>ASENI</u> |
| AGE | |
| | Signature of Owner (Notary Required) Signature of Agent |
| | Owner Mailing Address Agent Mailing Address |
| | Agent Maning Address |
| | |
| | Owner Phone Number Agent Phone Number |
| | |
| Ē | Approve by City of Visalia: |
| | |
| | Date: |
| | Page 2 of 2 |

NORTH



SOUTH ELEVATION

REFERENCE ONLY APPROX. |" = 10'

SITE NOTES

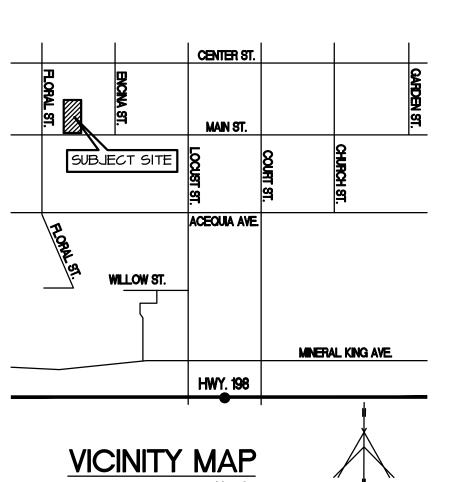
- EXISTING UNDERGROUND UTILITIES, PIPING, CONDUITS, IMPROVEMENTS OR OTHER UNDERGROUND ENCUMBERANCES FOR THIS EXISTING SITE ARE NOT SHOWN ON THESE PLANS. NO ATTEMPT HAS BEEN MADE BY COLLINS ENGINEERING TO LOCATE, VERIFY OR SHOW ANY NEW OR EXISTING UNDERGROUND UTILITIES, PIPING, CONDUITS, TANKS, IMPROVEMENTS OR OTHER UNDERGROUND ENCUMBERANCES FOR THIS EXISTING SITE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR FIELD LOCATING AND VERIFYING ALL UNDERGROUND UTILITIES, PIPING, CONDUITS, TANKS, IMPROVEMENTS AND SIMILAR UNDERGROUND ENCUMBERANCES AND TAKE ALL NECESSARY PRECAUTIONS AND PREVENTATIVE MEASURES TO INSURE THAT SUCH EXISTING UTILITIES ARE NOT DAMAGED OR DISRUPTED DURING CONSTRUCTION. OWNER AND ENGINEER SHALL BE NOTIFIED OF ANY UTILITIES, PIPING, ETC. THAT IS UNCOVERED PRIOR TO OR DURING CONSTRUCTION WHICH MAY INTERFERE WITH OR BE AFFECTED BY THE PROPOSED CONSTRUCTION SO CONDITIONS AND ALTERNATIVES CAN BE REVIEWED PRIOR TO PROCEEDING WITH CONSTRUCTION.
- 2. ALL PROPERTY LINE DIMENSIONS, LOCATIONS, DETAILS, EASEMENTS, ETC. ARE BASED ON AVAILABLE COUNTY ASSESSOR'S MAP INFORMATION AND SHALL BE VERIFIED AND SURVEYED BY A CALIF. LICENSED LAND SURVEYOR.
- 3. SEE DESIGNS AND DRAWINGS BY OTHERS FOR SITE UTILITIES, PAVING AND PATCHING.
- 4. FIELD VERIFY EXISTING CONDITIONS. ALL DIMENSIONS SHALL BE FIELD VERIFIED.

FIRE DEPARTMENT NOTES

- NOTHING IN THESE PLANS OR SPECIFICATIONS SHALL BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THE MOST STRINGENT OF APPLICABLE CODES. ALL WORK SHALL BE DONE IN ACCORDANCE WITH THE CALIFORNIA BUILDING CODE (CBC), CALIFORNIA FIRE CODE (CFC), AND ALL OTHER FEDERAL, STATE, COUNTY, AND CITY ORDINANCES.
- 2. COMBUSTIBLE OR FLAMMABLE WASTE MATERIAL OR RUBBISH OF ANY KIND SHALL NOT BE PERMITTED ON ANY YARD, VACANT LOT, OR OPEN SPACE. COMBUSTIBLE DEBRIS, RUBBISH, OR WASTE MATERIAL SHALL BE REMOVED AS OFTEN AS PRACTICAL. (CFC 3304)
- 3. FIRE EXTINGUISHERS PER CFC 906: PROVIDE PORTABLE FIRE EXTINGUISHERS, CLASS 2A:10B:C MINIMUM. ONE FOR EACH 3000 SQUARE FEET OR PORTION THEREOF OF FLOOR SPACE AND MAXIMUM TRAVEL DISTANCE FROM ANY POINT IN THE BUILDING TO AN EXTINGUISHER NOT TO EXCEED 75 FEET. WHEN POSSIBLE, THE FIRE EXTINGUISHERS SHOULD BE MOUNTED NEAR EXITS OR IN NORMAL EXIT PATHWAYS. IF NECESSARY, A SIGN SHALL BE POSTED TO CLEARLY INDICATE THE LOCATION OF THE EXTINGUISHER.
- 4. PLANS ARE NOT APPROVED FOR HIGH PILED COMBUSTIBLE STORAGE. STORAGE OF COMBUSTIBLE MATERIALS IN CLOSELY PACKED PILES OR COMBUSTIBLE MATERIALS ON PALLETS, IN RACKS, OR ON SHELVES WHERE THE TOP OF STORAGE IS GREATER THAN 12 FEET IN HEIGHT SHALL NOT BE ALLOWED.
- ADDRESS APPROVED NUMBERS OR ADDRESSES SHALL BE PLACED ON ALL NEW AND EXISTING BUILDINGS IN SUCH A POSITION AS TO BE PLAINLY VISIBLE AND LEGIBLE FROM THE STREET OR ROAD FRONTING THE PROPERTY. SAID NUMBERS SHALL BE AT LEAST 6" HIGH AND SHALL BE OF A COLOR TO CONTRAST WITH THEIR BACKGROUND. (CFC 505)
- ALL REQUIRED EXITS SHALL BE CLEAR OF OBSTRUCTIONS FOR THE DURATION OF THE CONSTRUCTION PROJECT.
- 7. DOOR HARDWARE- EGRESS DOORS SHALL BE READILY OPENABLE FROM THE EGRESS SIDE WITHOUT THE USE OF A KEY OR ANY SPECIAL KNOWLEDGE OR EFFORT. ALL HARDWARE SHALL COMPLY WITH CHAPTER IO OF THE CALIFORNIA BUILDING CODE (CBC).
- 8. MEANS OF EGRESS ILLUMINATION-. AT ANY TIME THE BUILDING IS OCCUPIED, THE MEANS OF EGRESS SHALL BE ILLUMINATED AT AN INTENSITY OF NOT LESS THAN I FOOT-CANDLE AT FLOOR LEVEL.
- EXIT SIGNS THE PATH OF TRAVEL TO AND WITHIN EXITS IN A BUILDING SHALL BE IDENTIFIED BY EXIT SIGNS CONFORMING TO THE REQUIREMENTS OF CBC CHAPTER IO. EXIT SIGNS SHALL BE READILY VISIBLE FROM THE DIRECTION OF APPROACH. EXIT SIGNS SHALL BE LOCATED AS NECESSARY TO INDICATE THE DIRECTION OF EGRESS TRAVEL. NO POINT SHALL BE MORE THAN 100 FEET FROM THE NEAREST VISIBLE SIGN.
- IO. AMOUNTS OF FLAMMABLE AND COMBUSTIBLE MATERIAL STORED IN THE BUILDING SHALL NOT EXCEED THE EXEMPT AMOUNTS QUANTIFIED IN CBC 307 AND CFC 5704.
- WHEN FIRE FACILITIES SUCH AS, BUT NOT LIMITED TO, FIRE HYDRANTS AND ACCESS ROADS ARE TO BE INSTALLED BY THE DEVELOPER, THEY SHALL BE INSTALLED AND MADE SERVICEABLE PRIOR TO AND DURING THE TIME OF CONSTRUCTION. (CFC 901)
- 12. PROVIDE NEW AUTOMATIC FIRE SPRINKLER SYSTEM AT ALL NEW AND/OR REMODELED STRUCTURES AND ADDITIONS. GENERAL CONTRACTOR SHALL INCLUDE IN BID THE PRICE FOR APPROVED PLANS, ENGINEERING, MATERIALS AND INSTALLATION OF NEW FIRE SPRINKLER SYSTEM INCLUDING ANY NEW RISERS AND TIE-IN TO EXISTING FIRE SPRINKLER AND ALARM SYSTEM WHICH MAY BE REQUIRED.
- 13. FIRE SPRINKLER CONTRACTOR SHALL SUBMIT PLANS TO AND OBTAIN PERMIT FROM THE JURISDICTION FIRE DEPARTMENT FOR ALL REQUIRED NEW INSTALLATIONS AND/OR MODIFICATIONS AND ADDITIONS TO EXISTING FIRE SPRINKLER SYSTEM. DESIGNATE ON SPRINKLER SUBMITTAL THE COMMODITY CLASS AND STORAGE HEIGHT.
- 14. ALL WORK SHALL COMPLY WITH NFPA STANDARDS, CBC AND CFC.

15. SUBMIT PLANS TO AND OBTAIN PERMITS FROM THE JURISDICTION FIRE

- DEPARTMENT FOR ALL FIRE ALARM INSTALLATIONS AND/OR MODIFICATIONS.
- 16. A SET OF PLANS SHOWING THE WORK TO BE DONE SHALL ALSO BE FORWARDED TO THE JURISDICTION BUILDING DEPARTMENT FOR REVIEW AND APPROVAL.
- 17. FINAL APPROVAL IS SUBJECT TO ACCEPTANCE AFTER A FIELD INSPECTION.
- 18. A KNOX BOX LOCK SYSTEM IS REQUIRED FOR THE BUILDING. APPLICATION IS AVAILABLE AT THE BUILDING DEPARTMENT. RETURN THE COMPLETED APPLICATION, ALONG WITH YOUR CHECK MADE PAYABLE TO "THE KNOX COMPANY" TO THE BUILDING DEPARTMENT FOR SIGN OFF AND MAILING PRIOR TO FINAL INSPECTION FOR OCCUPANCY. (CFC 902)
- 19. ANY FENCE GATE ACROSS THE ENTRY TO THE PROPERTY SHALL REQUIRE A KNOX BOX FOR FIRE DEPARTMENT ACCESS.





GOVERNING AGENCY AND CODES

CITY OF VISALIA

CALIFORNIA BUILDING STANDARDS CODE (CCR TITLE 24)

2019 CALIFORNIA BUILDING CODE 2019 CALIFORNIA PLUMBING CODE

2019 CALIFORNIA MECHANICAL CODE 2019 CALIFORNIA ENERGY CODE 2019 CALIFORNIA GREEN BUILDING STANDARDS CODE

2019 CALIFORNIA FIRE CODE 2019 CALIFORNIA ELECTRICAL CODE NFPA 13, 2019 EDITION NFPA 24, 2019 EDITION

ADA ACCESSIBLE GUIDELINES (ADAAG)

PROJECT INFO.

SITE PLAN REVIEW NO.: tbd

OWNER: DAYE FRANEY 121 N ENCINA STREET

VISALIA, CA 93291 559-804-4100 LOCATION: 312, 314 AND 316 W MAIN STREET

VISALIA, CA 93291 APN: 094-322-004

SITE AREA: 8,406 SF ZONING: DMU

USE: RESTAURANT **OCCUPANCY:** A-2

FLOOD ZONE: XL

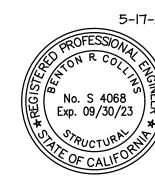
NUMBER OF STORIES: TYPE OF CONSTRUCTION: V-B (SPRINKLERED)

FLOOR AREA: 8,406 SF

ALLOWABLE FLOOR AREA: 24,000 SF (BASIC FOR OCC. A-2, TYPE V-B-SI)

F = 72' P = 377' W = 30

> If = (72/377 - 0.25) x 30/30 = 0.00 Aa = 24,000 SF



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5/17/22 22-1475 PROJECT NO:

PROJECT INFO AND SITE KEY

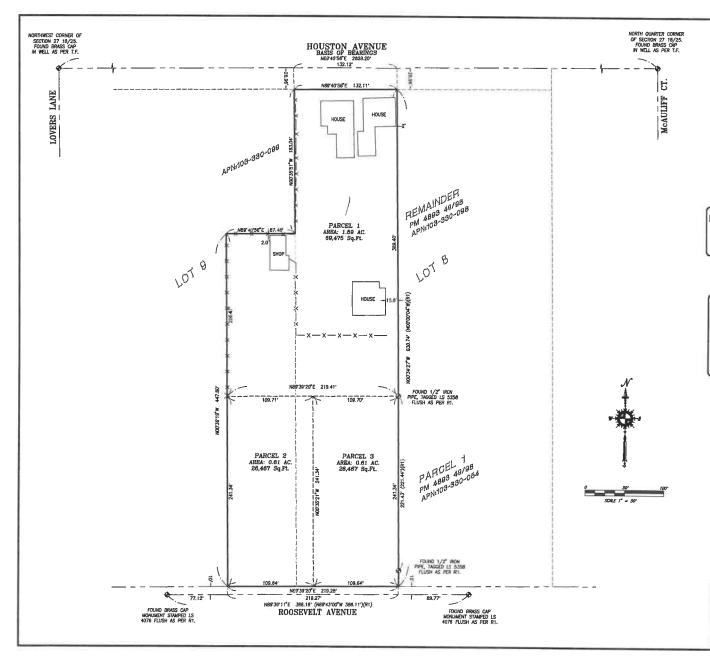
- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -- Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting -Project/Business Name: Project Description: GENERAL PROJECT INFORMATION Site Plan Review Resubmittal: If Resubmittal, Previous Site Plan Review Number: Property Owner: Applicant(s) Name: E. HOUSTON AVE Project Address/Location: Assessor Parcel Number: Parcel Size (Acreage or Square Feet): Building or Suite Square Footage: Are There Any Proposed Building Modifications: --- THIS AREA FOR CITY STAFF USE ONLY ---Yes (No () Date Received: 05/18/2022 Estimated Cost of Modifications to Building: SPR Agenda: 05/25/2022 Item No. _____ Describe All Proposed Building Modifications: Zone: R-1-5 SPR No. 22-086 Historic District: Yes No X X X AE XAE Flood Zone: -- A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS --Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: OPERATIONS & TRAFFIC INFORMATION Days of Week In Operation (Circle): Su M T W Th F Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existing Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees (Provide Separate Attachment if Necessary): Describe Any Special Events Planned for the Facility: Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS |
|------------------------|---|
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies |
| ENTS | not accepted). |
| SITE PLAN REQUIREMENTS | Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. |
| E | ⇒ Site plan shall provide for and indicate all of the following: |
| N R | - North arrow - Existing & proposed structures - Loading/unloading areas |
| PL | All existing & proposed site features Site dimensions, including building Refuse enclosures & containers Accessible path of travel from right of way Accessible path of travel from ADA stall |
| SIT | Site dimensions, including building Existing and proposed fencing at site Valley oak trees (show drip line) Accessible path of travel from ADA stall Location and width of drive approaches to site |
| | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| | Applicant Information (Final comments will be mailed to the name and address provided below) |
| R. | Name: Larry & tenny Op 8 Lar Signature of Owner or Authorized Agent |
| NAT | Address: 3318 5 0040/as Cent (14/a + 1enny Ussla, 5/10/22 |
| SIG | City, State, Zip 1/152/10 CA 93292 Owner |
| REQUIRED SIGNATURE | Phone: 559-696 5600 Email: Larryn penny & O Lyahoo. Com Authorized Agent Byerry (559) Date 790-5844 |
| REGL | Email: Larry n penny & Cyahoo. Com Kichard Buerto (559) Date 798-5844 |
| | * If signed by an authorized agent , the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | AGENCY AUTHORIZATION |
| | OWNER: |
| | |
| | !, declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): |
| | pared number (A) N). |
| | |
| | AGENT: |
| - | I designate to act as my duly authorized agent for all purposes necessary to file |
| IZATION FORM | an application for, and obtain a permit to |
| ONF | relative to the property mentioned herein. |
| ZATI | I declare under penalty of perjury the foregoing is true and correct. |
| 10R | Executed this day of, 20 |
| AGENCY AUTHOR | |
| NC | OWNER Signatures AGENT |
| AGE | |
| | Signature of Owner Skynature of Apart |
| | Signature of Owner Signature of Agent |
| | Owner Mailing Address Agent Mailing Address |
| | |
| | Owner Phone Number Agent Phone Number |
| | Owner Phone Number Agent Phone Number |
| 5 | |
| | |



SITE PLAN

CITY OF VISALIA - COUNTY OF TULARE STATE OF CALIFORNIA

LOTS 8 AND 9 OF THE OAKS AS PER MAP RECORDED IN BOOK 7 AT PAGE 50 OF MAPS, TULARE COUNTY RECORDS. EXCEPTING THE EAST 3 ACRES OF LOT 8 AND EXCEPTING THE WEST 242 FEET AND THE NORTH 210 FEET OF LOT 9. BEING LOCATED IN THE NORTHWEST QUARTER OF SECTION 27, TOWNSHIP 18 SOUTH, RANGE 25 EAST, MOUNT DIABLO BASE AND MERIDIAN (CONSISTING 60 OKS SHEET)

BASIS OF BEARINGS:

THE NORTH LINE OF THE NORTHWEST QUARTER OF SECTION 17, TOWNSHIP 18 SOUTH, RANGE 23 EAST, MOUNT DABLO BASE & MERIDIAN, TAKEN TO BE NOW $40^{\circ}50^{\circ}$ E AS PER GNSS OBSERVATION.

LEGEND:

- A MONIMENTS POLING AND ACCEPTED LINESS OTHERWISE NOTED
- (R1) RECORD DATA PER PARCEL MAP No. 4893 RECORDED IN BOOK 46 AT PAGE 88 OF PARCEL MAPS, TULARE COUNTY RECORDS.
- THE ON FILE WITH THE TULARE COUNTY SURVEYOR.
- INDICATES SUBJECT PARCEL BOUNDARY.

 DISTANCES NOT MONUMENTED ARE CALCULATED.

FEMA FLOOD ZONE: SHADED ZONE X

ADDITIONAL NOTES:

NO NEW PROPOSED ROADS OR EASEMENTS - ACCESS TO PARCEL 2 AND 3 WILL BE OFF OF ROOSEVELT AVENUE.

PROPOSED METHOD OF SOLID WASTE WITH BE THE CITY OF VISALIA.

THERE ARE NO PROPOSED PUBLIC BUS STOPS OR TURNOUTS.



M & L LAND SURVEYING 3949 N. CONDOR CT. SANGER, CA 93657

SANGER, CA 93657

Tel. (559) 531-9673

Email:

MLWEYANTOICLOUD.COM

| DATE OF SURVEY | 00/00/21 |
|----------------|-------------|
| JOB No. | 21XX |
| DRAWN BY | M.R. WEYANT |
| DRAWING NAME | 21XX |
| REVISION DATE | |

- Additional information and assistance in filling out this application can be found at the City of Visalia website (www.visalia.city) or by calling (559) 713-4440-



This application MUST be filled out in its entirety and submitted with an acceptable site plan (see site plan minimum requirements & submittal details on Page 2). Failure to provide all requested information may result in rejection of your application and exclusion from the Site Plan Review agenda.

- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -

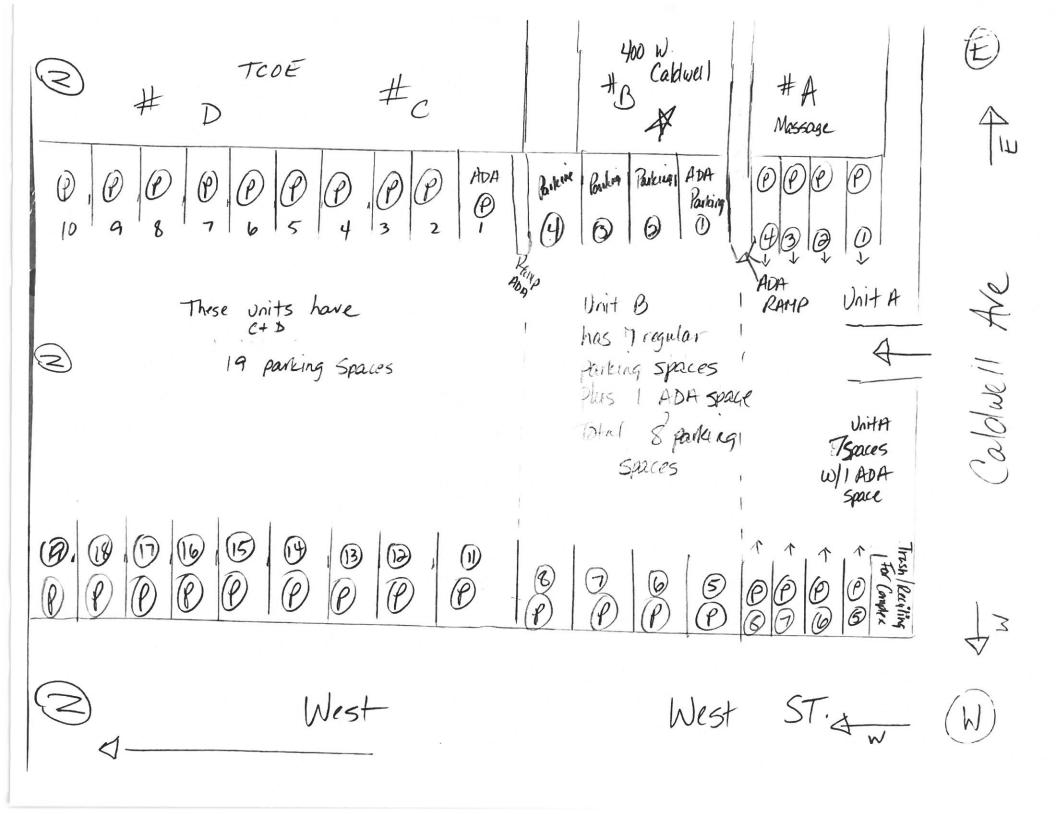
| - 1 | - Application submittal deadline is 4pm on Thursdays to be scheduled for | are next exercise meaning . |
|---|--|--|
| 1 | Project/Business Name: Facial X pressions Skin Care | Salon Date: 5-16-22 |
| 1. | Project Description: Skin Care Salon and retail | |
| 3 | -facials- stin care services and reta | il of slan products |
| 120 | Site Plan Review Resubmittal: Yes No No If Resubmittal, Previous Site Plan | |
| NE. | Property Owner. <u>Catherine</u> Doe | |
| | Applicant(s) Name: Norma A. Pena | |
| GENERAL PROJECT INCORAGATION | Project Address/Location: 400 W. Caldwell Ave # | B |
| NERA | Assessor Parcel Number: 123-240-024 | |
| 19 | Parcel Size (Acreage or Square Feet): Building or Suite Square Feet): | uare Footage: 1271 59. f4. |
| | Are There Any Proposed Building Modifications: Yes O No | THIS AREA FOR CITY STAFF USE ONLY |
| ı | Estimated Cost of Modifications to Building: S N A | Date Received: 05/16/2022 |
| | Describe All Proposed Building Modifications: Point to the Interior | SPR Agenda: 05/25/2022 Item No |
| | of the building, no building projects | Zone: <u>O-PA</u> SPR No . <u>22-087</u> |
| | needed. | Historic District: Yes No 🛇 |
| | | Flood Zone: X AE X/AE |
| A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS | | |
| | | ENDED FOR ALL SUBMITTALS |
| | | ^ |
| | | Campesina |
| | Existing/Prior Building Use: Radio Station - Radio La | Campesina |
| NION | Existing/Prior Building Use: Radio Station - Radio La Proposed Building Use: Skin Care Salon | Campesina |
| DRMATION | Proposed Hours of Operation: Radio Station - Radio La Radio Station - Radio La Skin Care Salo A Proposed Hours of Operation: By Appointment Only 3-0 | Campesina. |
| INFORMATION | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT W Th F Sa | Campesina 2-3 |
| AFFIC INFORMATION | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su M T W Th F Sa Number of Employees Per Day: Existing Proposed Proposed Number of Customers Per Day (Estimated): Existing 5-7 Proposed | Campesina 2-3 |
| & TRAFFIC INFORMATION | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su M T W Th F Sa Number of Employees Per Day: Existing Proposed Proposed Number of Customers Per Day (Estimated): Existing 5-7 Proposed | 2-3 7-10 |
| | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT WTh F Sa Number of Employees Per Day: Number of Customers Per Day (Estimated): Existing Proposed Proposed Predicted Peak Operating Hour: | 2-3 7-10 |
| | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT WTh F Sa Number of Employees Per Day: Number of Customers Per Day (Estimated): Existing Proposed Proposed Predicted Peak Operating Hour: | Campesina 2-3 1-10 recause T work by appointment only. |
| | Existing/Prior Building Use: Proposed Building Use: Skin Care Salon Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT W Th F Sa Number of Employees Per Day: Existing Proposed Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Number of Customers Per Day (Estimated): Proposed P | Campesina 2-3 1-10 Recause T work by appointment only. |
| | Existing/Prior Building Use: Proposed Building Use: Skin Care Salon Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT WTh F Sa Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existing Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations And Accommodations For Operations Accommodations For Operations And Accommodations For Operations Accommodations Accommodations For Operations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommoda | Campesina 2-3 1-10 Recause T work by appointment only. |
| OPERATIONS & TRAFFIC INFORMATION | Existing/Prior Building Use: Proposed Building Use: Skin Care Salon Proposed Hours of Operation: By Appointment Only 3-0 Days of Week In Operation (Circle): Su MT WTh F Sa Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existing Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations And Accommodations For Operations Accommodations For Operations And Accommodations For Operations Accommodations Accommodations For Operations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommodations Accommoda | Campesina 2-3 1-10 Recause T work by appointment only. |
| | Existing/Prior Building Use: Proposed Building Use: Proposed Hours of Operation: By Amountment Only 3-0 Days of Week In Operation (Circle): Su MT WTh F Sa Number of Employees Per Day: Existing Proposed Number of Customers Per Day (Estimated): Existing Proposed Proposed Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operating Separate Attachment if Necessary): Describe Separate Attachment if Necessary): Describe Separate Attachment if Necessary): Proposed Pr | Campesina 2-3 1-10 recause I war by appintment only. perations, Customers, or Employees s needed me be was ADA Compline to |

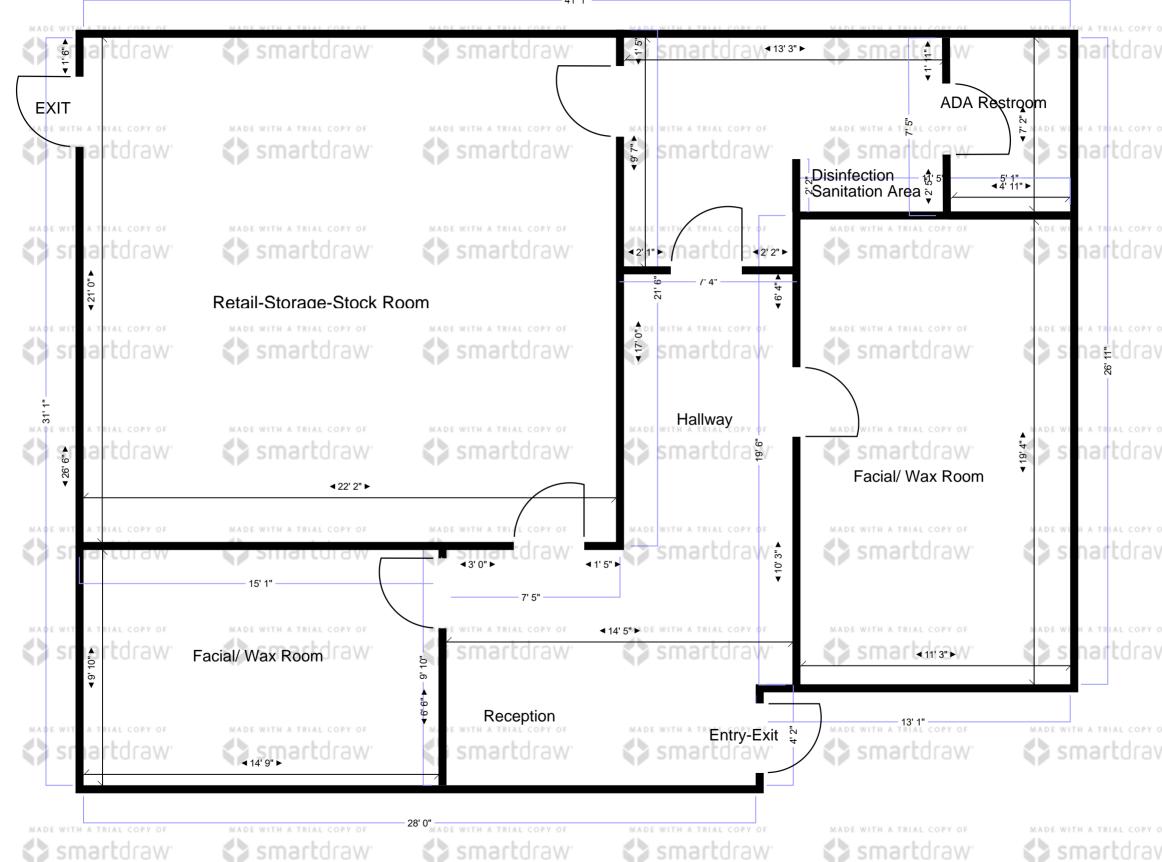
Page 1 of 2 - Application continues on back of this page

| | OFF BUAN AND AND AND AND AND AND AND AND AND A |
|------------------------|--|
| SITE PLAN REQUIREMENTS | SITE PLAN MINIMUM REQUIREMENTS Submit a digital copy of the site plan(s) and completed emplication on a flesh driver. |
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies not accepted). |
| | |
| | and on a layout sized appropriately to convey all necessary project information. |
| E G | Site plan shall provide for and indicate all of the following: - North arrow - Pristing & proposed attachange. |
| Ž | All origins 2 - Loading/unloading areas |
| 1 | - Site dimensions, including building - Refuse enclosures & containers - Accessible path of travel from ADA stall |
| " | - Existing and proposed rending at site - Valley oak trees (show drip line) - Location and width of drive approaches to site |
| | - Public improvements (curbs, sidewalks, - Existing & proposed landscaping - Tentative maps shall adhere to requirements utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| | Applicant Information (Final comments will be mailed to the name and address provided below) |
| # | 1 - 1 - |
| ATO | |
| SIGN | City, State, Zip Visalia CA 93277 Owner Owner Date |
| æ | Phone: 559-967-7687 |
| REQUIRED SIGNATURE | Email: facial x Are 451 on 500 spea spal Authorized Agent Date |
| œ | The state of the s |
| | " If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | AGENCY AUTHORIZATION |
| | OWNER: |
| | I, <u>Catherine</u> Doe declare as follows; I am the owner of certain real property bearing assessor's |
| | parcel number (APN): |
| | 123-240-124-000 |
| | AGENT: |
| | \mathcal{V}_{α} |
| Σ | I designate |
| FORM | relative to the property mentioned herein. |
| OF. | I declare under penalty of perjury the foregoing is true and correct. |
| AGENCY AUTHORIZATION | 1, 4, 111. |
| | Executed this |
| | Signatures Signatures |
| | OWNER AGENT |
| | Contract Doe |
| | Signature of Owner Signature of Owner |
| | 4.0. Box 325 3524 5. Hentage St. |
| | Owner Mailing Address Agent Mailing Address VISALIA, CA 93277 |
| | |
| | |
| | 93235 Owner Phone Number Agent Phone Number |
| | 93235 559-967-7687 |

Page 2 of 2







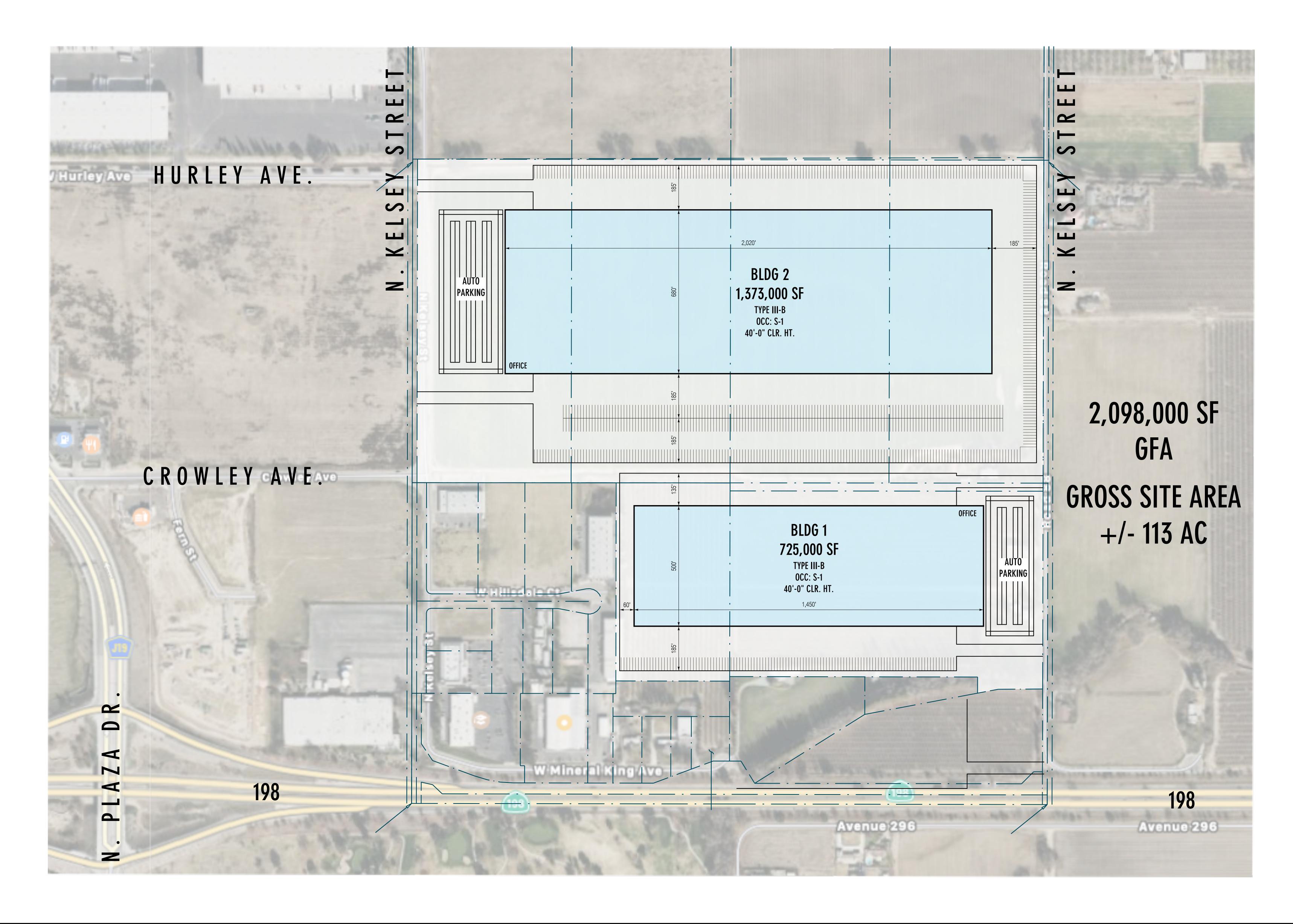
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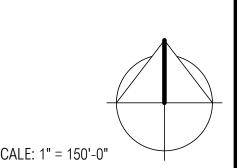


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- Site Plan Review meetings are held on Wednesdays at 9am at City Hall East - 315 E Acequia Ave - Applicant(s) or Representative(s) must be present -- Application submittal deadline is 4pm on Thursdays to be scheduled for the next available meeting -Visalia/ Kelsey St. Industrial Project/Business Name: unstruction of two (2) warehouse/distribution Project Description: GENERAL PROJECT INFORMATION 2,398 000 Saft If Resubmittal, Previous Site Plan Review Number: Site Plan Review Resubmittal: SE LAND, LLC Property Owner: Greenlaw Partners Applicant(s) Name: 29811 Road 88, Visalia, CA Project Address/Location: Assessor Parcel Number: 081-040-001; Ptn of 081-071-020; 081-071-013 Building or Suite Square Footage: 1,373,000 & 725,000 111 436 Parcel Size (Acreage or Square Feet): --- THIS AREA FOR CITY STAFF USE ONLY ---Yes No No Are There Any Proposed Building Modifications: Date Received: 05/18/2022 Estimated Cost of Modifications to Building: SPR Agenda: <u>05/25/2022</u> Item No. ___ Describe All Proposed Building Modifications: Zone: X SPR No. 22-088 Yes () No (X) Historic District: AE (X) Flood Zone: -- A SEPARATE, DETAILED OPERATIONAL STATEMENT IS HIGHLY RECOMMENDED FOR ALL SUBMITTALS --Agricultural land Existing/Prior Building Use: Industrial Warehouse & Distribution Facility Proposed Building Use: Operational Hours will be determined by future tenant. Proposed Hours of Operation: OPERATIONS & TRAFFIC INFORMATION W Th F Days of Week In Operation (Circle): Su M T TBD Number of Employees Per Day: Existina None Proposed TBD None Number of Customers Per Day (Estimated): Existing Proposed Operational Hours will be determined by the future tenant. Predicted Peak Operating Hour: Describe Any Truck Delivery Schedule & Operations: Truck/Trailer trips associated with the facility will consist of shipping, receiving, and other industrial-related activities. The number, type, and frequency of truck/vans for service and delivery will be decided by future tenants. Please Identify Any Unique or Specific Traffic Patterns That Will Require Accommodations For Operations, Customers, or Employees Operations would include office and industrial uses, such as warehousing and distribution. Detailed (Provide Separate Attachment if Necessary): operations, equipment, supplies and materials will be determined by the future tenants of the site There are no special events currently planned for the facility. Future events at the facility will Describe Any Special Events Planned for the Facility: be determined by the future tenant. Page 1 of 2 - Application continues on back of this page

| | SITE PLAN MINIMUM REQUIREMENTS |
|------------------------|--|
| | Submit a digital copy of the site plan(s) and completed application on a flash drive or equivalent (PDF format preferred, hard paper copies |
| ξ | not accepted). |
| SITE PLAN REQUIREMENTS | Digital copies must be clear, legible, and on a layout sized appropriately to convey all necessary project information. |
| 9 | ⇒ Site plan shall provide for and indicate all of the following: |
| Z | - North arrow - Existing & proposed structures - Loading/unloading areas |
| Z | - All existing & proposed site features - Adjacent street names - Accessible path of travel from right of way |
| SITE | Site dimensions, including building Refuse enclosures & containers Accessible path of travel from ADA stall Existing and proposed fencing at site Valley oak trees (show drip line) Location and width of drive approaches to site |
| | Existing and proposed fencing at site Valley oak trees (show drip line) Location and width of drive approaches to site Public improvements (curbs, sidewalks, Existing & proposed landscaping Tentative maps shall adhere to requirements |
| | utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) of Visalia Municipal Code Section 16 |
| | Applicant Information (Final comments will be mailed to the name and address provided below) |
| REQUIRED SIGNATURE | Name: Derek Meddings Signature of Owner or Authorized Agent* |
| GNA | Address: 1820) Von Karmon Avc Owner Date |
| ED SI | City, State, Zip Irvine, CA 92612 |
| Z | Phone: (949) 331 - 1332 Authorized Ageht Date |
| REC | Email: derek (a) greenlaw partners, com |
| | * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | AGENCY AUTHORIZATION |
| | OWNER: |
| | A comment |
| | I, SE Land, UC declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): |
| | 081-040-001 (081-071-013 Am of 081-071-020 |
| I | 001-040-001 001-013 rtm at 001-011-000 |
| | AGENT: |
| | I designate Voycot & Irichard to act as my duly authorized agent for all purposes necessary to file |
| ORM | an application for, and obtain a permit to |
| ATION FORM | |
| ZATI | I declare under penalty of perjury the foregoing is true and correct. |
| AGENCY AUTHORIZ | Executed this |
| AU. | |
| NC | OWNER Signatures AGENT |
| AGE | 20-50 |
| | Signature of Owner Signature of Agent |
| | PC Box 964 18301 Van Karman Ave |
| | Owner Mailing Address Agent Mailing Address |
| | Visalia, CA 93279 Irvine, CA 92612 |
| | 661-387-0200 (947) 331-1332 |
| | Owner Phone Number Agent Phone Number |
| | |
| | Page 2 of 2 |





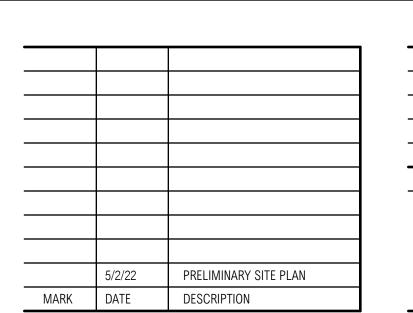




WEST VISALIA INDUSTRIAL DEVELOPMENT

KELSEY ST. / HWY 198 - VISALIA / TULARE CTY, CA

SCHEMATIC SITE PLAN





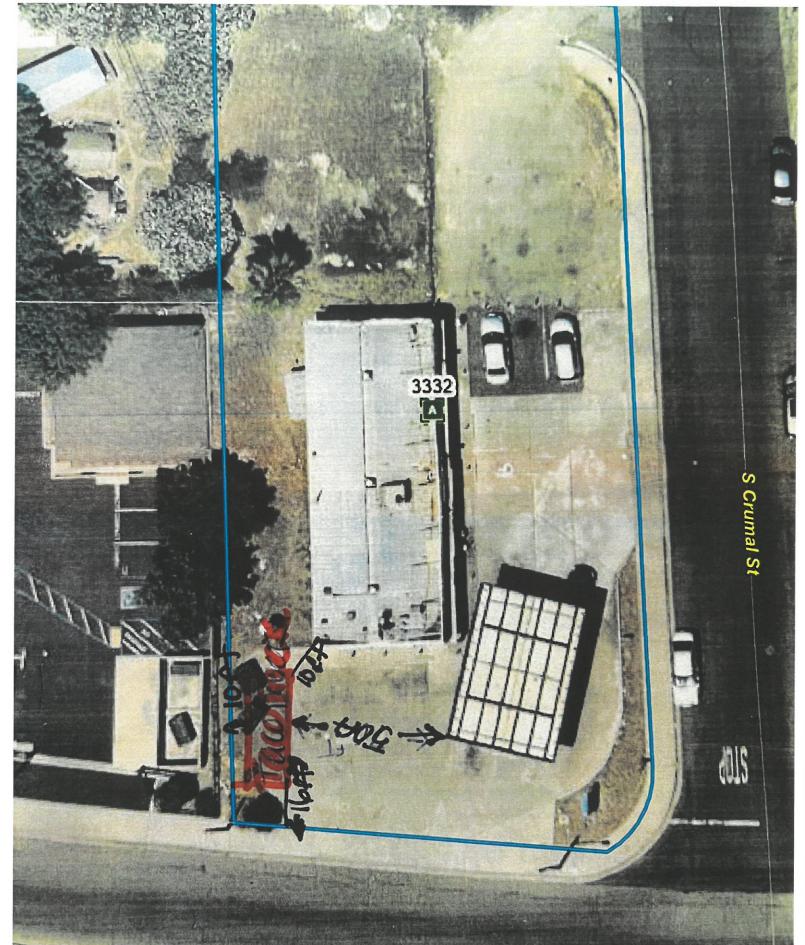
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| 33 | SITE PLAN MINIMUM REQUIREMENTS |
|---------------------|--|
| | Plan(s) must be clear, legible, and on a sheet size appropriate to easily convey all necessary project information. Suggested minimum |
| 2 | sheet size for site plans is 11"x17" (Excludes tentative parcel and final maps) |
| ME | ⇒ Site plan shall provide for and indicate all of the following: |
| SI IE PLAIN NEGUINE | - North arrow - Existing & proposed structures - Loading/unloading areas - All existing & proposed site features - Adjacent street names - Accessible path of travel from right of way - Site dimensions, including building - Refuse enclosures & containers - Accessible path of travel from ADA stall - Existing and proposed fencing at site - Valley oak trees (show drip line) - Location and width of drive approaches to site - Public improvements (curbs, sidewalks, utility poles, hydrants, street lights, etc.) - Parking stalls (include ADA) - Tentative maps shall adhere to requirements of Visalia Municipal Code Section 16 |
| | Submit 20 copies of the site plan with this application, folded to a legal size of 9" x 12" with the print on the outside (no rolled plans) |
| REQUIRED SIGNALORE | Applicant Information (Final comments will be mailed to the name and address provided below) Name: Susana Campo Signiture of Owner or Authorized Agent* Address: 3437 t. Suamore Ave Substitute of Owner or Authorized Agent* City, State, Zip MSNUG OA, 93292 Owner Phone: 559-786 3221 Email: Susana Campo 99 Q ya kw w Authorized Agent* Date |
| - | * If signed by an authorized agent, the "Agency Authorization" information below must be completed for this application to be considered acceptable. |
| | |
| | AGENCY AUTHORIZATION |
| を | OWNER: I, SUCHA SINGH declare as follows; I am the owner of certain real property bearing assessor's parcel number (APN): |
| | 193 152 010 |
| IN FURIN | AGENT: I designate, to act as my duly authorized agent for all purposes necessary to file an application for, and obtain a permit to relative to the property mentioned herein. |
| | I declare under penalty of perjury the foregoing is true and correct. |
| THO WE | Executed this 17 day of Nay 20 22 |
| 1 | OWNER Signatures AGENT |
| 1 | Signature of Agent Signature of Agent |
| | 3332 E. Mineral Fing Ave |
| 1 | Owner Malling Address VI Salia, CA 93292 |
| | (559) 303 - 1608 Agent Phone Number |
| | Owner Phone Number |
| | |
| | Page 2 of 2 |



ElMineral King Ave

E Mineral King Ave